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WIND-TUNNEL MEASUREMENTS OF THE CHORDWISE PRESSURE DISTRIBUTION AND PROFILE DRAG OF A RESEARCH AIRPLANE MODEL INCORPORATING A 17-PERCENT-THICK SUPERCRITICAL WING

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by James C. Ferris

Langley Research Center
Hampton, Va. 23365

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Pressure coefficients for four wing semispan stations and wing-section normal-force and pitching-moment coefficients for two semispan stations are presented in tabular form over the Mach number range from 0.30 to 0.80. In addition, plotted chordwise pressure distributions and wake profiles are presented for a selected range of section normal-force coefficients over the same Mach number range.

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WIND-TUNNEL MEASUREMENTS OF THE CHORDWISE PRESSURE DISTRIBUTION AND PROFILE DRAG OF A RESEARCH AIRPLANE MODEL INCORPORATING A 17-PERCENT-THICK SUPERCRITICAL WING*

By James C. Ferris
Langley Research Center

SUMMARY

An investigation has been conducted in the Langley 8-foot transonic pressure tunnel to determine the chordwise pressure distribution for a 0.09-scale model of a research airplane incorporating a 17-percent-thick supercritical wing. Airfoil profile drag was determined from wake pressure measurements at the 42-percent-semispan wing station. The investigation was conducted at Mach numbers from 0.30 to 0.80 over an angle-of-attack range sufficient to include buffet onset.

Pressure coefficients for four wing semispan stations and wing-section normal-force and pitching-moment coefficients for two semispan stations are presented in tabular form over the Mach number range from 0.30 to 0.80. In addition, plotted chordwise pressure distributions and wake profiles are presented for a selected range of section normal-force coefficients c_n over the same Mach number range.

The results of the investigation indicate that the 17-percent-thick supercritical airfoil has relatively high force drag-divergence Mach number (Mach number ≈ 0.74) at normal-force coefficients corresponding to cruise conditions. Section normal-force coefficients of 1.5 were achieved at a Mach number of 0.30 at an angle of attack of 17°. An examination of section wake profiles indicated that shock-induced separation did not occur until normal-force coefficients of 0.65 were achieved at the design Mach number of 0.73.

INTRODUCTION

Over the last several years research on supercritical airfoils at the Langley Research Center has been directed toward improving performance by increasing the drag-divergence Mach number and therefore the cruising speeds of airplanes that employ wings with this airfoil section. These airfoils accomplish this improvement by delaying the onset of shock-induced flow separation over the airfoil and, as a result, also delay buffet

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onset of the wing. (See refs. 1 to 4.) As part of this effort, wind-tunnel models with advanced design features such as variable-sweep wings and area-rule modifications have been investigated with supercritical wings. (See refs. 5 to 7.) The results from these investigations indicate the supercritical wing can be incorporated in the design of airplane configurations in conjunction with other advanced design features to obtain the additive performance improvements of each concept. Wind-tunnel test results given in references 8 to 10 and the full-scale flight tests of a research airplane configuration provide an excellent example of the application of the supercritical wing and the area rule to demonstrate the aerodynamic feasibility of near-sonic commercial jet transports.

Other unpublished data indicate that supercritical airfoil sections with substantial increases in thickness ratio can obtain drag-divergence Mach numbers equal to those of approximately 40-percent thinnner conventional sections. As a result, the advantages of more volume for fuel or boundary-layer-control high-lift devices, increased aspect ratio, and lower structural weight may be achieved by use of supercritical airfoil sections with high thickness ratios. A second flight research program was initiated to demonstrate these properties of the supercritical airfoil. This program utilized a modified T-2C trainer airplane incorporating a 17-percent-thick supercritical airfoil. Wind-tunnel and flight data for this configuration are presented in references 11 to 13.

The purpose of this paper is to present wing pressure distributions and profile drag data obtained from a wind-tunnel investigation of a 0.09-scale model of a U.S. Navy trainer airplane (T-2C) employing a supercritical airfoil section with a thickness-chord ratio of 0.17.

The investigation was conducted in the Langley 8-foot transonic pressure tunnel at Mach numbers from 0.30 to 0.80. At the lowest Mach number the angle of attack was varied sufficiently to determine maximum lift coefficient $(C_L)_{max}$ and the stall characteristics. At the higher Mach numbers the angle of attack was generally terminated at the buffet lift coefficient $(C_L)_B$ to avoid excessive dynamic loads due to buffeting on the instrumentation mounted within the model.

SYMBOLS

Values are given in SI Units; however, measurements and calculations were made in U.S. Customary Units. Wing-section pitching-moment coefficients are referenced to the 0.25 chord line of the basic wing panel. Most of the pressure data presented herein were machine tabulated and the limitations of type faces necessitated some differences between the notation of these tables and conventional symbols. The symbols in the following list are given in the conventional form with the machine notation included in parentheses after the conventional symbol.

[redacted]

b reference wing span, 98.618 centimeters

C_L lift coefficient, $\frac{\text{Lift}}{qS}$

C_{L_α} lift-curve slope, $\frac{\partial C_L}{\partial \alpha}$

C_p pressure coefficient

c local streamwise chord, centimeters

$\bar{c}$ reference mean geometric chord, 20.318 centimeters

c_d wing section drag coefficient, $\sum c_d' \frac{\Delta z}{c}$

c_d' point drag coefficient (ref. 14)

c_m (CM) wing-section pitching-moment coefficient about 0.25c, $\int_{L.E.}^{T.E.} \left(C_{p,l} - C_{p,u}\right)\left(0.25 - \frac{x}{c}\right)d\left(\frac{x}{c}\right)$

$c_{m_{c_n}}$ rate of change of wing-section pitching-moment coefficient about 0.25c with wing-section normal-force coefficient, $\frac{\partial c_m}{\partial c_n}$

$c_{m,o}$ wing-section pitching-moment coefficient about 0.25c at zero normal force

c_n (CN) wing-section normal-force coefficient, $\int_{L.E.}^{T.E.} \left(C_{p,l} - C_{p,u}\right)d\left(\frac{x}{c}\right)$

c_{n_α} rate of change of wing-section normal-force coefficient with angle of attack, $\frac{\partial c_n}{\partial \alpha}$, per degree

i_h horizontal-tail incidence angle, referred to fuselage reference line (positive when trailing edge is down), degrees

M free-stream Mach number

p_t free-stream total pressure, newtons/meter^2

q (Q) free-stream dynamic pressure, newtons/meter^2

$R_{\bar{c}}$ Reynolds number based on $\bar{c}$

[redacted]

S	reference wing area, 0.192 meter^2
x	longitudinal distance, centimeters
x'	ordinate along airfoil reference line measured from airfoil leading edge, centimeters
y	spanwise distance from plane of symmetry, centimeters
z	vertical distance in wake profile measured from lower surface of trailing edge of wing, centimeters
z'	ordinate normal to airfoil reference line, centimeters
α	angle of attack, degrees
δ_a	aileron deflection angle, referred to wing-chord plane (positive when trailing edge is down), degrees
δ_e	elevator deflection angle, referred to horizontal-tail plane (positive when trailing edge is down), degrees
η	wing semispan station, 2y/b

Subscripts:

B	buffet
L	left
l	lower
ler	leading-edge radius
max	maximum
R	right
sonic	sonic conditions
u	upper

APPARATUS AND PROCEDURES

Model Description

A three-view drawing of the sting-supported 0.09-scale model used for the present investigation is shown in figure 1(a) and a drawing of the 17-percent-thick supercritical airfoil is presented as figure 1(b). The geometric characteristics of the model are presented in table I and coordinates of the supercritical airfoil are given in table II. These coordinates do not include the small extension (0.0075c) at the trailing edge from the aileron inboard to the wing-fuselage juncture as shown in figures 1(a) and 1(b). This extension was used to form a step for configuration 1 and a 0.0075c thick (blunt) trailing edge for configuration 2.

The locations of the pressure orifices on the left wing are shown in figure 1(c). Most of the orifices were located at the 0.4245- and 0.7325-semispan stations to minimize fuselage and wing-tip fuel-tank interference on the data and to determine the effects of aileron deflection on the pressures over the aileron and wing. Some orifices were also located at inboard and outboard semispan stations of 0.1592 and 0.9025, respectively. These orifices, however, were not of a sufficient number to compute the section normal force and pitching moment of these semispan stations.

Photographs of the model and profile drag rake are presented in figures 2(a) and 2(b), respectively. The total-pressure probes on the rake were arranged in two vertical columns spaced at a horizontal distance of 0.508 centimeter and vertical distances between the probes in each row of 0.152 centimeter. The rows were staggered so that total-pressure measurements at 0.0772 centimeter vertical increments would be measured by alternating from one row to the other.

Tunnel Description

The investigation was conducted in the Langley 8-foot transonic pressure tunnel, which is a single-return tunnel having a rectangular, slotted test section to permit continuous operation through the transonic speed range. This facility has the capability of independent variation of Mach number, density, temperature, and humidity. The stagnation temperature and dewpoint were maintained at values sufficient to avoid significant condensation effects. (See, for example, ref. 10.) The characteristics of the tunnel can be found in reference 15.

Test Conditions

The model was investigated at Mach numbers from 0.30 to 0.80 through a lift coefficient range sufficient to determine buffet onset. The Reynolds number based on the mean geometric chord varied from 2×10^6 at $M = 0.30$ to 3.33×10^6 at $M = 0.65$ and was

maintained at a constant value of 3.86×10^6 at $M = 0.70$ to $M = 0.80$. Table III presents the tunnel conditions for which the data were obtained.

Boundary-Layer Transition

All the investigations were made with transition fixed on the model. Boundary-layer trips were applied to the upper and lower surfaces of the wing by using the technique described in references 16 and 17 to simulate the full-scale Reynolds number boundary-layer-displacement thickness characteristics at the wing trailing edge. In order to maintain laminar flow ahead of the trips, as required by this technique, the model surfaces were maintained in an extremely smooth condition.

The location and the size of the carborundum grains used for the boundary-layer trips are given in the following table:

Surface	Type of transition strip	Location
Fuselage	No. 150 carborundum grains	3.1 cm aft of nose apex
Wing upper surface	No. 120 carborundum grains	27 percent of local streamwise chord
Wing lower surface	No. 120 carborundum grains	37 percent of local streamwise chord
Wing-tip-mounted fuel tanks	No. 150 carborundum grains	3.3 cm aft of nose apex
Horizontal and vertical tails	No. 180 carborundum grains	10 percent of local streamwise chord

Measurements

Streamwise static pressures were measured at four wing semispan stations ($\eta = 0.1592$, 0.4245, 0.7325, and 0.9025). Wing section normal-force and pitching-moment coefficients for $\eta = 0.4245$ and $\eta = 0.7325$ were obtained by numerical integration (based on the trapezoidal method) of the local pressure coefficients measured at each orifice multiplied by an appropriate weighting factor (incremental area). Profile drag was computed from the wake survey rake measurements made at $\eta = 0.4245$ by using the method of reference 14.

Corrections

Corrections have been made to the angle of attack for model support-sting and balance deflections, which occur as a result of aerodynamic loads on the model. Further corrections to the measured angle of attack have been made for tunnel airflow angularity and for the first-order boundary corrections calculated by the method used in reference 18.

PRESENTATION OF RESULTS

Wing upper and lower surface tabulated pressure coefficients for $\eta = 0.1592$, 0.4245, 0.7325, and 0.9025 are presented in tables IV to VIII. Section normal-force and pitching-moment coefficients for $\eta = 0.4245$ and $\eta = 0.7325$ are also presented in these tables. Lift coefficients and angles of attack for the complete model, determined from force measurements, are included in the tabulations for reference and identification purposes. An index (p. 18) summarizes the contents of the tables and lists the pertinent test conditions.

Representative chordwise pressure distributions and corresponding wake profiles are presented in figure 3 for $\eta = 0.4245$. These data generally cover a normal-force coefficient range from 0.30 to 0.70 over the Mach number range from 0.30 to 0.76. Additional data are presented at $M = 0.76$ (somewhat higher than the design Mach number) to illustrate the shock loss pattern in the wake as the normal force is varied from near zero to a value sufficient to cause shock-induced separation.

Chordwise pressure distributions for an extended angle-of-attack range to include $c_{n,max}$ and the stall at $M = 0.30$ are presented in figure 4(a). The data presented in figure 4(b) at a Mach number more representative of cruise ($M = 0.73$) include negative values of normal-force coefficient and a range of positive values to those associated with shock-induced separation at this Mach number. Representative chordwise pressure distributions at $\eta = 0.7325$ are presented in figure 5 for various aileron deflection angles and the effect of sealing the aileron ends and hinge line on the chordwise pressure distribution is presented in figure 6.

The wing section data for $\eta = 0.4245$ are presented in figure 7 and summary data for this wing station are presented in figure 8.

DISCUSSION

Chordwise Pressure Distributions

Chordwise pressure distributions with corresponding wake profiles.- Most of the pressure data were obtained simultaneously with the force data presented in reference 11. For these data the configuration was complete with the horizontal tail on and with the incidence and elevator deflection angles at 0°. However, it was desirable to determine the airfoil profile drag over a Mach number and normal-force range compatible with the capability of the research airplane; consequently, a profile drag rake was mounted 6 percent aft of the trailing edge of the wing at $\eta = 0.4245$. A limited amount of data was obtained with the profile drag rake installed and for these tests it was necessary to remove the horizontal tail. (See fig. 2(c).) Since the pressure leads from the rake were routed down

the model support sting, some interference on the balance measurements resulted and the absolute values of the force and moment data from this part of the investigation were considered to be invalid.

Selected chordwise pressure distributions at $\eta = 0.4245$ with the corresponding wake profiles (which will be discussed later) are presented in figure 3. These pressure distributions are not directly comparable with the data obtained for the model with the horizontal tail on, because of the influence of the horizontal tail on the wing flow at some Mach numbers. The pressure distributions at subsonic Mach numbers from 0.30 to 0.65 (figs. 3(a) to 3(d)) indicate a peak near the leading edge typical of airfoils with large leading-edge radii and exhibit the general aft loading characteristic of supercritical airfoils. At Mach numbers of 0.60 and 0.65, supersonic flow is developed on the upper surface in the first 25 percent of the airfoil; however, at these Mach numbers the pressure distribution still indicates a peak near the leading edge.

As Mach number is increased to 0.70 (fig. 3(e)), the peak near the leading edge is reduced and much of the lift is developed by the rearward movement of the shock wave position. This rearward movement of the shock wave also improves the pressure recovery near the trailing edge at this Mach number and near the design conditions, $M = 0.73$, $c_n = 0.50$ (fig. 3(f)) where the pressure distribution assumes a shape typical of that for supercritical airfoils. (See refs. 2 to 4.) A plateau, evident in most of these data, aft of the shock wave on the upper surface, helps to stabilize the boundary layer ahead of the larger adverse pressure gradient over the last half of the airfoil.

As the Mach number is increased to 0.75 (fig. 3(g)), supersonic flow is observed on the lower surface for all the data presented. The supersonic flow on the lower surface for $c_n = 0.3201$ appears to disturb the flow in the cusp so that the upper surface recovery near the trailing edge (0.99c) is less than that for $c_n = 0.4772$. As c_n is increased to 0.5577, the flow on the upper surface appears to have deteriorated as the shock position has not moved rearward with this increase in c_n, the plateau aft of the shock wave is no longer evident, and there is more separation near the trailing edge.

The data at $M = 0.76$ are presented over a c_n range from near zero to values associated with separation of the flow on the upper surface near the trailing edge of the airfoil. (See fig. 3(h).) This Mach number and angle-of-attack range was chosen to illustrate the shock losses in the wake which will be discussed later. It is noted from the pressure distributions that substantial supersonic flow is developed on both the upper and lower surfaces of the airfoil and that at the low normal-force coefficients, the load is carried on the aft half of the airfoil, as would be expected for these negative angle-of-attack conditions. As c_n is increased to 0.4352, the upper surface shock wave moves rearward and further increases in c_n result in separated flow over the aft part of the airfoil with a corresponding forward movement of the shock wave and a reduction in the trailing-edge pressure recovery. As Mach number is increased to 0.80 (fig. 3(i)), super-

sonic flow is evident on both the upper and lower surface over most of the first 60 percent of the airfoil where shock-induced separation is indicated for all normal-force coefficients presented.

Extended angle-of-attack range.- The data presented in references 11 and 12 indicate considerable improvement in the low-speed lift capability of the modified T-2C research airplane. The chordwise pressure distributions for $\eta = 0.4245$ at the higher angles of attack are presented in figure 4(a) for $M = 0.30$, the lowest Mach number of the investigation. These data show a large pressure peak developed near the leading edge (typical of airfoils with large leading-edge radii at low speeds) which generally increases with increasing angle of attack up to the stall point and results in a higher stall angle than airfoils with small leading-edge radii. Additional low-speed two-dimensional section data for this airfoil are presented in reference 19.

Results for an extended angle-of-attack range near the cruise Mach number ($M = 0.73$) are presented in figure 4(b). The trends of the chordwise pressure distribution for these data are similar to the data presented in figure 3(h) at $M = 0.76$; however, the flow on the lower surface is subsonic at cruise values of c_n and considerably higher values of c_n are obtained $\left(c_n \approx 0.65\right)$ before separation of the flow near the trailing edge occurs.

Chordwise pressure distribution over the aileron.- The effect of aileron deflection angle on the chordwise pressure distribution at $\eta = 0.7325$ is presented in figure 5. The aileron deflection influences the pressure distribution over the entire chord of the wing at this station. There is noticeable separation near the trailing edge of the aileron at both Mach numbers for some δ_a -values for which data are presented. This separation was also evident in the fluorescent oil flow studies of this region of the wing presented in reference 11 and appears to be due to the spanwise flow caused by the flow around the ends of the aileron and flow through the hinge line.

The effects of sealing the hinge line and ends of the aileron are presented in figure 6. These results indicate that sealing the aileron improves the chordwise pressure distribution somewhat at both semispan stations.

Wake Profiles at $\eta = 0.4245$

The profile drag rake was located at approximately 6 percent of the local chord aft of the trailing edge of the wing at $\eta = 0.4245$ (the same as for the research airplane, see fig. 2(c)). The wake is turbulent and thin near the trailing edge of a wing and caution should be used in comparing these irregular wake profiles with profiles measured in the wake of a wing at one or more chord lengths aft of the trailing edge, since in the latter case the wake would have more time to stabilize. The rake was located aft of the right wing to eliminate interference of the rake on the chordwise pressure measurements. The

z/c scale for the wake profiles is expanded considerably to accommodate the close spacing of the probes near the center of the rake and therefore should not be compared directly with the x/c scale of the chordwise pressure distributions.

The results of figure 3 indicate that at lower Mach numbers (figs. 3(a) and 3(b)), the wake is smooth with no indication of separation. Although there are small regions of supersonic flow indicated on the upper surface by the pressure distributions at $M = 0.60$ and $M = 0.65$ (figs. 3(c) and 3(d)) for all angles of attack, the profiles indicate a shock loss occurring only at the highest angle of attack ($\alpha \approx 2.7^{\circ}$) for the data presented at $M = 0.65$. At Mach numbers of 0.70 and 0.73 (cruise Mach numbers, see figs. 3(e) and 3(f)) where substantial regions of supersonic flow are evident in the pressure distributions on the upper surface, the shock losses in the wake profile increase with increasing angle of attack. Although these shock losses cause small increases in the profile drag coefficient as c_n is increased, there is no indication of shock-induced separation for the data presented. With further increase in Mach number to 0.75, there is some separation indicated in the wake profile at the higher angle of attack (fig. 3(g), $\alpha = 1.31^{\circ}$) as the thickness of the wake aft of the upper surface is increased significantly.

The data at $M = 0.76$ (fig. 3(h)) are presented over a c_n range from near zero to values associated with separation of the flow on the upper surface near the trailing edge of the airfoil. At the lowest angle of attack there is some supersonic flow on the upper surface indicated in the pressure distribution, but no shock loss indicated in the wake profile at this angle of attack. The lower surface, however, does indicate a shock loss in the wake profile and a significantly large adverse pressure gradient is indicated on the lower surface in the pressure distribution. As angle of attack is increased, however, larger losses are observed in the wake aft of the upper surface and the losses are reduced on the lower surface. Separation on the upper surface is evident at positive angles of attack; however, it should be noted that a range of normal-force coefficients from 0 to approximately 0.35 exists where the shock losses are minimized even at Mach numbers greater than the design cruise Mach number.

Wing Section Characteristics

Profile drag.- The wing-section profile drag coefficient c_d, the angle of attack α, and the wing-section pitching-moment coefficient c_m for wing semispan station 0.4245 are presented as functions of the wing-section normal-force coefficient c_n in figure 7. At low subsonic Mach numbers (0.30 to 0.60), the profile drag is of the same order of magnitude as would be expected of a wing of this thickness ratio and camber. At the higher Mach numbers and normal-force coefficients where extensive supersonic flow exists on the upper surface, the wake rake was not sufficiently large to measure all the shock losses. This part of the normal-force range is indicated by a dashed line; however,

these data appear to be reasonably accurate up to normal-force coefficients associated with separation of the flow near the trailing edge ($c_n \approx 0.80$ at $M = 0.70$ and $c_n \approx 0.40$ at $M = 0.76$). The data at Mach numbers from 0.30 to 0.65 suggest the presence of a small laminar bucket which is not observed at the higher Mach numbers. This condition may be a possible result of the transition trip being sized and located for the cruise conditions; as a result, the trip was undersized for these lower Mach numbers. At the highest Mach number of the investigation ($M = 0.80$), the flow is separated over much of the airfoil and the profile drag is increased significantly.

Wing-section summary data are presented as a function of Mach number in figure 8. The dashed part of the curves from $M = 0.30$ to $M = 0.60$ are from the low Reynolds number data. The trends for c_d at the various values of c_n are similar to the data for the complete configuration presented in reference 11 and indicate a drag divergence Mach number on the order of 0.74 at $c_n = 0.40$.

Normal-force coefficient.- The curves of c_n as a function of α (fig. 7(b)) are nonlinear and have an increase in the slope at the higher Mach numbers at c_n values near cruise. This increase in slope is probably a result of the rapid rearward movement of the shock-wave location as the angle of attack is increased in this range of normal-force coefficients. A maximum value of 1.5 in normal-force coefficient was achieved at a Mach number of 0.30 and an angle of attack of 17°. The derivative c_{n_α} is presented as a function of Mach number in figure 8. As would be expected, the trend is similar to C_{L_α} for the complete configuration presented in reference 11. The large increase in c_{n_α} from $M = 0.65$ to $M = 0.74$ is a probable result of the increase in the extent of supersonic flow on the upper surface.

Pitching-moment coefficient.- The pitching-moment coefficients c_m referenced to the 25-percent chord (see fig. 7(c)) indicate relatively large negative values because of the aft loading characteristic of the supercritical section. This aft loading is caused by the camber in the rear 50 percent of the airfoil. The variation of c_m with Mach number was approximately 0.08 over a range of c_n values from 0 to 1.20 and a Mach number range from 0.30 to 0.75. The trends of $c_{m_{c_n}}$ and $c_{m,o}$ are presented as a function of Mach number in figure 8.

CONCLUSIONS

Results of wind-tunnel measurements of the chordwise pressure distribution and profile drag of a 17-percent-thick supercritical wing indicate the following conclusions:

1. The variation of section profile drag characteristics with Mach number for normal-force coefficients corresponding to those of airfoil cruise indicated relatively high drag divergence Mach numbers ($M \approx 0.74$) for this 17-percent-thick airfoil.

2. Maximum wing section normal-force coefficients on the order of 1.5 were achieved at a Mach number of 0.30 at an angle of attack of 17°.

3. An examination of section wake profiles indicated that at moderate normal-force coefficients at the higher Mach numbers (although some shock losses were noted), significant regions of local supersonic flow existed with little or no indication of shock-induced separation.

4. Trailing-edge separation is evident on the upper surface at normal-force coefficients above 0.65 and 0.44 at Mach numbers of 0.73 and 0.76, respectively, and shock-induced separation is indicated at all normal-force coefficients presented for a Mach number of 0.80.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., March 16, 1973.

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TABLE I.- MODEL GEOMETRIC CHARACTERISTICS

Wing:	
Total area, m^2	0.192
Aileron area (one aileron), m^2	0.007
Span (theoretical), cm	98.618
Aspect ratio	5.07
Taper ratio	0.496
Dihedral angle, deg	3.323
Incidence at root, deg	2.5
Incidence at tip, deg	1
Airfoil at root and tip	See table II
Mean aerodynamic chord, cm	20.318
Horizontal distance to center line of airplane, cm	21.735
Vertical distance to fuselage reference line at 25 percent chord, cm	1.084
Incidence, deg	2
Horizontal tail:	
Total area, m^2	0.054
Elevator area (total aft of hinge line), m^2	0.016
Span, cm	49.131
Aspect ratio	4.47
Taper ratio	0.508
Dihedral angle, deg	0
Airfoil at root and tip	NACA 65_1A012
Mean geometric chord, cm	11.533
Horizontal distance to center of airplane, cm	10.923
Vertical distance to fuselage reference line at 25 percent chord, cm	13.076
Vertical tail:	
Total area (exposed), m^2	0.027
Rudder area, m^2	0.007
Span (theoretical; exposed), cm	22.055
Aspect ratio (exposed)	1.800
Taper ratio (exposed)	0.375
Airfoil at root and tip, cm	NACA 63_1A012
Mean aerodynamic chord, cm	13.385
Vertical distance to fuselage reference line, cm	16.848

TABLE II.- WING AIRFOIL COORDINATES ALONG STREAMWISE CHORDS

[Leading-edge radius/Chord = 0.0428; $(x'/c)_{ler}$ = 0.0428; $(z'/c)_{ler}$ = 0.00]

x'/c	z'/c		x'/c	z'/c	
	Upper	Lower		Upper	Lower
0.0	0.000	0.000	0.575	0.08423	-0.0652
.0125	.0304	-.030	.600	.08248	-.0607
.0250	.0401	-.0408	.625	.08043	-.0554
.0375	.0469	-.048	.650	.07811	-.0495
.0500	.0519	-.0533	.675	.07541	-.0431
.075	.0593	-.0611	.700	.07233	-.0366
.100	.0652	-.0664	.725	.06881	-.0301
.125	.06963	-.0704	.750	.06476	-.0240
.150	.07325	-.0735	.775	.0595	-.0184
.175	.07625	-.0760	.800	.0553	-.0134
.200	.07890	-.0779	.825	.0499	-.0093
.250	.0832	-.0807	.850	.0440	-.0060
.300	.0863	-.0819	.875	.0376	-.0036
.350	.08825	-.0820	.900	.0308	-.0021
.400	.0891	-.0810	.925	.0236	-.0017
.450	.08893	-.0786	.950	.0160	-.0025
.500	.08783	-.0748	.975	.0081	-.0044
.550	.08568	-.0690	1.000	.00	-.0080

TABLE III.- WIND-TUNNEL OPERATING CONDITIONS

Mach number	p_t, N/m^2	q, N/m^2	$R_{\bar{c}}$
0.30	171 699	10 103	2.00×10^6
.50	146 609	21 690	2.67
.60	159 872	31 649	3.33
.65	151 541	33 756	3.33
.70	167 820	41 464	3.86
.73	163 655	42 853	3.86
.75	161 165	43 619	3.86
.76	159 920	44 098	3.86
.80	155 850	45 774	3.86

INDEX TO TABLES IV TO VIII

Mach number	Aileron deflection angle, δ_a, deg	Angle of attack, α, deg	Lift coefficient range
Table IV; configuration 1; horizontal tail on; wake rake off; aileron unsealed			
0.30	-6	-4.15 to 4.49	-0.103 to 0.672
.30	-3	-4.13 to 4.50	-.081 to .692
.30	0	-4.10 to 13.05	-.059 to 1.364
.30	3	-4.08 to 4.58	-.040 to .723
.30	6	-4.09 to 4.55	-.036 to .726
.50	0	-4.16 to 8.81	-.092 to 1.040
.60	-6	-4.51 to 5.06	-.194 to .781
.60	-3	-4.40 to 3.73	-.163 to .663
.60	0	-4.30 to 3.84	-.134 to .684
.60	3	-4.41 to 3.84	-.128 to .705
.60	6	-4.28 to 3.89	-.111 to .720
.65	0	-4.45 to 6.05	-.185 to .934
.70	-6	-4.80 to 4.86	-.256 to .815
.70	-3	-4.87 to 4.76	-.247 to .804
.70	0	-4.70 to 4.09	-.221 to .802
.70	3	-4.64 to 3.84	-.205 to .804
.70	6	-4.59 to 5.41	-.186 to .895
.73	-6	-4.89 to 2.83	-.291 to .640
.73	-3	-4.87 to 2.62	-.264 to .648
.73	0	-4.91 to 2.67	-.262 to .649
.73	3	-4.81 to 2.40	-.241 to .651
.73	6	-4.76 to 2.49	-.221 to .678
.75	0	-4.88 to 5.38	-.259 to .707
.76	-6	-4.78 to 4.09	-.254 to .597
.76	-3	-4.73 to 4.12	-.236 to .619
.76	0	-4.79 to 5.13	-.246 to .664
.76	3	-4.73 to 3.89	-.257 to .662
.76	6	-4.74 to 3.13	-.236 to .590
.80	0	-4.50 to 5.33	-.206 to .533
Table V; configuration 1; horizontal tail off; wake rake on; aileron unsealed			
0.30	0	-4.14 to 10.90	-0.011 to 1.176
.50	0	-4.27 to 5.39	-.023 to .799
.60	0	-4.49 to 3.79	-.072 to .698
.65	0	-4.63 to 5.54	-.112 to .905
.70	0	-4.98 to 3.83	-.150 to .824
.73	0	-5.13 to 1.42	-.185 to .581
.75	0	-5.06 to 1.31	-.186 to .547
.76	0	-4.39 to 1.08	-.133 to .476
.80	0	-4.15 to .02	-.109 to .155
Table VI; configuration 2; horizontal tail off; wake rake on; aileron unsealed			
0.70	0	-4.97 to 3.78	-0.149 to 0.819
.75	0	-5.06 to 1.34	-.183 to .555
Table VII; configuration 2; horizontal tail on; wake rake off; aileron sealed			
0.70	0	-4.64 to 3.81	-0.192 to 0.812
.73	0	-4.68 to 2.36	-.216 to .657
.75	0	-4.70 to 2.01	-.237 to .553
Table VIII; configuration 2; horizontal tail on; wake rake off; aileron unsealed; high angle-of-attack range			
0.30	0	2.40 to 18.77	0.518 to 1.448

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED

(a) M = 0.30

$\delta_a = -6^o$; $\alpha = -4.15^o$; $C_L = -0.103$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.385	.916	0.000	.963	.956	0.000	.051	.942	.050	-.225	.925
.150	-.413	.914	.012	.344	.959	.012	.305	.957	.150	-.301	.921
.300	-.407	.915	.025	.004	.939	.025	.075	.943	.300	-.343	.918
.450	-.378	.916	.050	-.305	.920	.050	-.205	.927	.450	-.319	.920
.600	-.422	.914	.100	-.360	.917	.100	-.279	.922	.600	-.317	.920
.800	-.391	.915	.150	-.381	.916	.150	-.278	.922	.800	-.177	.928
.990	.046	.942	.200	-.401	.915	.200	-.330	.919			
			.300	-.403	.915	.300	-.354	.918			
			.350	-.397	.915	.350	-.337	.919			
			.400	-.404	.915	.400	-.339	.919			
			.450	-.386	.916	.450	-.350	.918			
			.500	-.445	.912	.500	-.371	.917			
			.550	-.456	.912	.550	-.365	.917			
			.600	-.427	.913	.600	-.361	.917			
			.650	-.456	.912	.700	-.239	.925			
			.700	-.449	.912	.800	-.181	.928			
			.800	-.336	.919	.900	-.057	.935			
			.900	-.116	.932	.950	.034	.941			
			.950	.007	.939	.990	.117	.946			
			.990	.086	.944						
					LOWER SURFACE						
.100	-.678	.898	.025	-.843	.888	.025	-.872	.887	.100	-.952	.882
.300	-.628	.901	.050	-1.008	.879	.050	-1.081	.874	.300	-.594	.903
.600	-.333	.919	.100	-.818	.890	.100	-.890	.886	.600	-.377	.916
.800	.146	.948	.200	-.709	.896	.200	-.724	.896	.800	.062	.943
			.300	-.656	.900	.300	-.665	.899			
			.400	-.596	.903	.400	-.636	.901			
			.500	-.551	.906	.500	-.541	.906			
			.600	-.283	.922	.600	-.384	.916			
			.700	.016	.940	.700	-.132	.931			
			.800	.156	.951	.800	.111	.945			
			.900	.270	.955	.900	.183	.950			
			.950	.270	.955	.950	.238	.953			
			1.000	.110	.945						
CN=				-.0131			-.1701				
CM=				-.0955			-.0544				

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = -3.09^o$; $C_L = -0.003$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.559	.905	0.000	1.008	.999	0.000	.061	.943	.050	-.359	.917
.150	-.483	.910	.012	.115	.946	.012	.154	.948	.150	-.363	.917
.300	-.446	.912	.025	-.256	.924	.025	-.106	.932	.300	-.370	.917
.450	-.405	.915	.050	-.430	.910	.050	-.417	.914	.450	-.344	.918
.600	-.449	.912	.100	-.443	.912	.100	-.405	.915	.600	-.332	.919
.800	-.397	.915	.150	-.459	.911	.150	-.369	.917	.800	-.175	.928
.990	.044	.941	.200	-.464	.911	.200	-.418	.914			
			.300	-.454	.912	.300	-.403	.915			
			.350	-.441	.913	.350	-.389	.916			
			.400	-.427	.913	.400	-.368	.917			
			.450	-.416	.914	.450	-.383	.916			
			.500	-.468	.911	.500	-.401	.915			
			.550	-.487	.910	.550	-.386	.916			
			.600	-.451	.912	.600	-.373	.917			
			.650	-.475	.910	.700	-.248	.924			
			.700	-.463	.911	.800	-.181	.928			
			.800	-.347	.918	.900	-.054	.936			
			.900	-.122	.932	.950	.034	.941			
			.950	.009	.939	.990	.113	.946			
			.990	.088	.944						
					LOWER SURFACE						
.100	-.570	.905	.025	-.602	.903	.025	-.601	.903	.100	-.828	.889
.300	-.560	.905	.050	-.861	.887	.050	-.917	.884	.300	-.563	.905
.600	-.307	.920	.100	-.753	.894	.100	-.796	.891	.600	-.375	.916
.800	.174	.949	.200	-.630	.901	.200	-.626	.901	.800	.086	.944
			.300	-.567	.903	.300	-.597	.903			
			.400	-.552	.906	.400	-.594	.903			
			.500	-.518	.908	.500	-.509	.908			
			.600	-.262	.923	.600	-.365	.917			
			.700	.027	.940	.700	-.119	.932			
			.800	.213	.952	.800	.131	.947			
			.900	.313	.958	.900	.213	.952			
			.950	.256	.957	.950	.270	.955			
			1.000	.106	.945						
CN=				.0729			-.0682				
CM=				-.0999			-.0540				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = -1.98^o$; $C_L = 0.103$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.678	.899	0.000	1.016	1.000	0.000	.061	.943	.050	-.560	.906
.150	-.580	.905	.012	-.136	.931	.012	-.119	.932	.150	-.474	.911
.300	-.506	.909	.025	-.474	.911	.025	-.347	.919	.300	-.428	.914
.450	-.450	.912	.050	-.623	.902	.050	-.604	.903	.450	-.374	.917
.600	-.464	.912	.100	-.609	.903	.100	-.523	.908	.600	-.351	.918
.800	-.397	.916	.150	-.556	.906	.150	-.468	.911	.800	-.187	.928
.950	.043	.942	.200	-.553	.906	.200	-.495	.910			
			.300	-.507	.909	.300	-.468	.911			
			.350	-.488	.910	.350	-.435	.913			
			.400	-.483	.910	.400	-.411	.915			
			.450	-.480	.912	.450	-.427	.914			
			.500	-.507	.909	.500	-.431	.914			
			.550	-.507	.909	.550	-.415	.915			
			.600	-.476	.911	.600	-.397	.916			
			.650	-.501	.909	.700	-.261	.924			
			.700	-.477	.911	.800	-.192	.928			
			.800	-.363	.918	.900	-.064	.935			
			.900	-.112	.933	.950	.026	.941			
			.950	.004	.939	.990	.103	.945			
			.990	.083	.944						
					LOWER SURFACE						
.100	-.515	.909	.025	-.418	.914	.025	-.367	.918	.100	-.714	.897
.300	-.504	.909	.050	-.629	.902	.050	-.721	.896	.300	-.520	.908
.600	-.296	.922	.100	-.595	.904	.100	-.630	.902	.600	-.368	.917
.800	.193	.951	.200	-.541	.907	.200	-.556	.906	.800	.108	.946
			.300	-.522	.908	.300	-.546	.907			
			.400	-.507	.909	.400	-.555	.906			
			.500	-.494	.910	.500	-.480	.911			
			.600	-.233	.925	.600	-.345	.919			
			.700	.041	.942	.700	-.114	.932			
			.800	.239	.953	.800	.141	.948			
			.900	.328	.959	.900	.227	.953			
			.950	.310	.958	.950	.283	.956			
			1.000	.105	.945						
CN=				.1812			.0386				
CM=				-.1010			-.0521				

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = -0.86^o$; $C_L = 0.209$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.941	.883	0.000	1.013	.959	0.000	.068	.943	.050	-.754	.894
.150	-.675	.899	.012	-.346	.919	.012	-.376	.917	.150	-.560	.906
.300	-.570	.905	.025	-.738	.895	.025	-.592	.904	.300	-.478	.911
.450	-.470	.911	.050	-.847	.889	.050	-.754	.894	.450	-.401	.915
.600	-.483	.911	.100	-.726	.896	.100	-.640	.901	.600	-.363	.918
.800	-.401	.915	.150	-.677	.899	.150	-.564	.906	.800	-.194	.928
.950	.048	.942	.200	-.626	.902	.200	-.578	.905			
			.300	-.568	.905	.300	-.518	.908			
			.350	-.538	.907	.350	-.477	.911			
			.400	-.542	.907	.400	-.456	.912			
			.450	-.492	.910	.450	-.464	.912			
			.500	-.532	.908	.500	-.462	.912			
			.550	-.532	.908	.550	-.441	.913			
			.600	-.494	.910	.600	-.422	.914			
			.650	-.521	.908	.700	-.279	.923			
			.700	-.497	.910	.800	-.206	.927			
			.800	-.358	.918	.900	-.079	.935			
			.900	-.123	.932	.950	.024	.941			
			.950	.001	.939	.990	.100	.945			
			.990	.075	.944						
					LOWER SURFACE						
.100	-.437	.913	.025	-.150	.930	.025	-.133	.931	.100	-.613	.903
.300	-.444	.913	.050	-.425	.914	.050	-.504	.909	.300	-.495	.910
.600	-.289	.922	.100	-.471	.911	.100	-.530	.908	.600	-.359	.918
.800	.216	.952	.200	-.455	.912	.200	-.495	.910	.800	.118	.946
			.300	-.467	.911	.300	-.496	.910			
			.400	-.451	.912	.400	-.509	.909			
			.500	-.451	.912	.500	-.456	.912			
			.600	-.225	.926	.600	-.333	.919			
			.700	.045	.942	.700	-.103	.933			
			.800	.257	.955	.800	.152	.948			
			.900	.343	.960	.900	.240	.953			
			.950	.322	.958	.950	.295	.957			
			1.000	.098	.945						
CN=				.2830			.1371				
CM=				-.1016			-.0513				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = 0.23^o$; $C_L = 0.306$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.176	.869	0.000	.995	.998	0.000	.067	.943	.050	-.540	.883
.150	-.743	.895	.012	-.638	.901	.012	-.651	.900	.150	-.634	.902
.300	-.598	.904	.025	-1.037	.878	.025	-.795	.892	.300	-.534	.907
.450	-.489	.910	.050	-1.121	.873	.050	-.961	.882	.450	-.431	.914
.600	-.488	.910	.100	-.838	.889	.100	-.770	.893	.600	-.383	.916
.800	-.384	.916	.150	-.749	.895	.150	-.666	.900	.800	-.199	.927
.990	.051	.942	.200	-.709	.897	.200	-.619	.901			
			.300	-.623	.902	.300	-.581	.905			
			.350	-.585	.904	.350	-.578	.908			
			.400	-.564	.906	.400	-.501	.909			
			.450	-.525	.908	.450	-.501	.909			
			.500	-.564	.906	.500	-.498	.910			
			.550	-.554	.906	.550	-.470	.911			
			.600	-.517	.908	.600	-.441	.913			
			.650	-.525	.908	.700	-.295	.922			
			.700	-.497	.910	.800	-.218	.926			
			.800	-.353	.918	.900	-.078	.935			
			.900	-.104	.933	.950	.016	.940			
			.950	.017	.940	.990	.091	.945			
			.990	.085	.944						
					LOWER SURFACE						
.100	-.316	.920	.025	.011	.940	.025	.037	.941	.100	-.481	.911
.300	-.491	.916	.050	-.297	.927	.050	-.358	.918	.300	-.451	.912
.600	-.760	.924	.100	-.324	.920	.100	-.398	.916	.600	-.352	.918
.800	.229	.953	.200	-.382	.916	.200	-.409	.915	.800	.123	.947
			.300	-.411	.915	.300	-.451	.912			
			.400	-.411	.915	.400	-.471	.911			
			.500	-.415	.915	.500	-.425	.914			
			.600	-.201	.927	.600	-.312	.921			
			.700	.067	.943	.700	-.095	.934			
			.800	.270	.955	.800	.154	.948			
			.900	.355	.960	.900	.239	.953			
			.950	.325	.959	.950	.294	.957			
			1.000	.096	.945						
CN=				.3787			.2341				
CM=				-.0568			-.0485				

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = 1.27^o$; $C_L = 0.396$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.325	.860	0.000	.927	.954	0.000	.070	.943	.050	-1.117	.873
.150	-.843	.889	.012	-.928	.884	.012	-.909	.885	.150	-.683	.899
.300	-.677	.899	.025	-1.254	.865	.025	-1.071	.876	.300	-.564	.906
.450	-.575	.908	.050	-1.262	.864	.050	-1.113	.873	.450	-.453	.912
.600	-.569	.908	.100	-.975	.881	.100	-.891	.886	.600	-.390	.916
.800	-.403	.915	.150	-.851	.889	.150	-.739	.895	.800	-.202	.927
.990	.038	.941	.200	-.795	.892	.200	-.716	.897			
			.300	-.690	.898	.300	-.635	.901			
			.350	-.643	.901	.350	-.572	.905			
			.400	-.625	.902	.400	-.533	.908			
			.450	-.574	.905	.450	-.527	.908			
			.500	-.598	.904	.500	-.518	.908			
			.550	-.597	.904	.550	-.492	.910			
			.600	-.548	.907	.600	-.459	.912			
			.650	-.558	.906	.700	-.302	.921			
			.700	-.521	.908	.800	-.219	.926			
			.800	-.361	.918	.900	-.076	.935			
			.900	-.117	.932	.950	.014	.940			
			.950	.000	.939	.990	.082	.944			
			.990	.061	.943						
					LOWER SURFACE						
.100	-.216	.926	.025	.122	.946	.025	.237	.953	.100	-.386	.916
.300	-.364	.918	.050	-.122	.932	.050	-.191	.928	.300	-.410	.915
.600	-.246	.925	.100	-.239	.925	.100	-.287	.922	.600	-.337	.919
.800	.238	.953	.200	-.320	.920	.200	-.355	.918	.800	.124	.947
			.300	-.369	.917	.300	-.400	.915			
			.400	-.377	.917	.400	-.437	.913			
			.500	-.399	.916	.500	-.404	.915			
			.600	-.189	.928	.600	-.296	.922			
			.700	.073	.944	.700	-.095	.934			
			.800	.270	.955	.800	.164	.949			
			.900	.345	.960	.900	.254	.954			
			.950	.321	.958	.950	.305	.957			
			1.000	.067	.943						
CN=				.4666			.3213				
CM=				-.0973			-.0451				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = 2.40^o$; $C_L = 0.494$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.510	.850	0.000	-.835	.889	0.000	-.069	.943	.050	-1.372	.858
.150	-.942	.883	.012	-1.322	.861	.012	-1.231	.866	.150	-.757	.894
.300	-.719	.897	.025	-1.674	.840	.025	-1.359	.859	.300	-.611	.903
.450	-.559	.906	.050	-1.508	.850	.050	-1.373	.858	.450	-.476	.911
.600	-.432	.913	.100	-1.132	.877	.100	-1.018	.879	.600	-.403	.915
.800	-.392	.916	.150	-.953	.883	.150	-.839	.890	.800	-.204	.927
.950	.038	.947	.200	-.870	.888	.200	-.781	.893			
			.300	-.742	.895	.300	-.685	.899			
			.350	-.690	.898	.350	-.621	.903			
			.400	-.656	.900	.400	-.585	.905			
			.450	-.596	.904	.450	-.557	.906			
			.500	-.629	.902	.500	-.555	.906			
			.550	-.612	.903	.550	-.518	.909			
			.600	-.563	.906	.600	-.488	.910			
			.650	-.571	.905	.700	-.316	.921			
			.700	-.526	.908	.800	-.227	.926			
			.800	-.362	.918	.900	-.076	.935			
			.900	-.093	.934	.950	.011	.940			
			.950	.001	.939	.990	.075	.944			
			.990	.050	.942						
					LOWER SURFACE						
.100	-.122	.932	.025	.302	.957	.025	.391	.963	.100	-.273	.923
.300	-.316	.921	.050	-.003	.939	.050	-.041	.937	.300	-.361	.918
.600	-.234	.925	.100	-.128	.932	.100	-.190	.928	.600	-.321	.920
.800	.242	.954	.200	-.236	.925	.200	-.263	.924	.800	.129	.947
			.300	-.305	.921	.300	-.345	.919			
			.400	-.329	.920	.400	-.399	.916			
			.500	-.363	.918	.500	-.364	.918			
			.600	-.168	.929	.600	-.281	.923			
			.700	.036	.944	.700	-.078	.935			
			.800	.275	.956	.800	.171	.949			
			.900	.361	.961	.900	.265	.955			
			.950	.332	.959	.950	.310	.958			
			1.000	.059	.943						
CN=				.5673			.4228				
CM=				-.0933			-.0429				

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = 3.39^o$; $C_L = 0.578$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.758	.835	0.000	-.734	.883	0.000	-.077	.944	.050	-1.572	.846
.150	-1.024	.879	.012	-1.576	.846	.012	-1.565	.847	.150	-.855	.889
.300	-.753	.895	.025	-1.905	.826	.025	-1.613	.844	.300	-.638	.902
.450	-.590	.904	.050	-1.703	.838	.050	-1.547	.848	.450	-.493	.910
.600	-.540	.907	.100	-1.228	.867	.100	-1.130	.872	.600	-.406	.915
.800	-.382	.917	.150	-1.051	.877	.150	-.914	.885	.800	-.195	.928
.950	.024	.941	.200	-.950	.883	.200	-.860	.888			
			.300	-.797	.892	.300	-.731	.896			
			.350	-.736	.896	.350	-.650	.901			
			.400	-.687	.899	.400	-.607	.903			
			.450	-.641	.901	.450	-.587	.905			
			.500	-.657	.900	.500	-.571	.905			
			.550	-.635	.902	.550	-.532	.908			
			.600	-.586	.905	.600	-.490	.910			
			.650	-.583	.904	.700	-.319	.921			
			.700	-.541	.907	.800	-.228	.926			
			.800	-.365	.918	.900	-.079	.935			
			.900	-.108	.933	.950	.014	.940			
			.950	-.002	.939	.990	.071	.944			
			.990	.050	.942						
					LOWER SURFACE						
.100	-.012	.939	.025	.401	.963	.025	.508	.969	.100	-.190	.928
.300	-.271	.923	.050	.143	.948	.050	.065	.943	.300	-.319	.920
.600	-.219	.926	.100	-.048	.936	.100	-.072	.935	.600	-.311	.921
.800	.249	.954	.200	-.191	.928	.200	-.227	.926	.800	.136	.947
			.300	-.241	.925	.300	-.294	.922			
			.400	-.292	.922	.400	-.332	.920			
			.500	-.349	.919	.500	-.346	.919			
			.600	-.155	.930	.600	-.263	.924			
			.700	.093	.945	.700	-.060	.936			
			.800	.290	.957	.800	.181	.950			
			.900	.364	.961	.900	.279	.956			
			.950	.329	.959	.950	.330	.959			
			1.000	.048	.942						
CN=				.6474			.5068				
CM=				-.0928			-.0413				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -6^o$; $\alpha = 4.49^o$; $C_L = 0.672$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.967	.823	0.000	.592	.574	0.000	.073	.944	.050	-1.756	.835
.150	-1.115	.873	.012	-1.973	.622	.012	-1.932	.825	.150	-.925	.884
.300	-.812	.891	.025	-2.251	.806	.025	-1.944	.824	.300	-.683	.899
.450	-.604	.904	.050	-1.952	.821	.050	-1.749	.836	.450	-.514	.909
.600	-.556	.906	.100	-1.372	.858	.100	-1.273	.864	.600	-.417	.915
.800	-.378	.917	.150	-1.167	.870	.150	-1.013	.879	.800	-.195	.928
.950	.023	.941	.200	-1.024	.879	.200	-.944	.883			
			.300	-.851	.889	.300	-.793	.892			
			.350	-.785	.893	.350	-.707	.897			
			.400	-.722	.897	.400	-.655	.901			
			.450	-.670	.900	.450	-.621	.902			
			.500	-.684	.899	.500	-.595	.904			
			.550	-.660	.900	.550	-.548	.907			
			.600	-.608	.903	.600	-.510	.909			
			.650	-.595	.904	.700	-.331	.920			
			.700	-.538	.907	.800	-.236	.925			
			.800	-.356	.918	.900	-.086	.934			
			.900	-.096	.934	.950	.002	.939			
			.950	-.009	.939	.990	.056	.943			
			.990	.030	.941						
					LOWER SURFACE						
.100	.082	.944	.025	.540	.871	.025	.640	.977	.100	-.086	.934
.300	-.220	.926	.050	.266	.855	.050	.179	.950	.300	-.284	.923
.600	-.198	.928	.100	.052	.842	.100	.010	.940	.600	-.301	.921
.800	.263	.955	.200	-.111	.833	.200	-.143	.931	.900	.132	.947
			.300	-.188	.828	.300	-.240	.925			
			.400	-.250	.925	.400	-.309	.921			
			.500	-.315	.821	.500	-.319	.920			
			.600	-.133	.831	.600	-.247	.925			
			.700	.108	.846	.700	-.059	.936			
			.800	.301	.857	.800	.181	.950			
			.900	.371	.861	.900	.274	.956			
			.950	.339	.859	.950	.323	.959			
			1.000	.043	.842						
CN=				.7451			.5997				
CM=				-.0891			-.0373				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = -4.13^o$; $C_L = -0.081$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.346	.920	0.000	.975	.997	0.000	.060	.943	.050	-.242	.926
.150	-.408	.916	.012	.341	.960	.012	.296	.957	.150	-.325	.921
.300	-.404	.916	.025	-.036	.938	.025	.025	.941	.300	-.360	.919
.450	-.376	.918	.050	-.328	.921	.050	-.273	.924	.450	-.348	.919
.600	-.428	.915	.100	-.355	.919	.100	-.313	.922	.600	-.365	.918
.800	-.384	.917	.150	-.396	.917	.150	-.305	.922	.800	-.251	.925
.950	.050	.943	.200	-.402	.916	.200	-.356	.919			
			.300	-.400	.916	.300	-.382	.918			
			.350	-.399	.917	.350	-.361	.919			
			.400	-.414	.916	.400	-.363	.919			
			.450	-.386	.917	.450	-.396	.917			
			.500	-.448	.914	.500	-.414	.916			
			.550	-.458	.913	.550	-.406	.916			
			.600	-.433	.915	.600	-.405	.916			
			.650	-.465	.913	.700	-.325	.921			
			.700	-.460	.913	.800	-.260	.925			
			.800	-.335	.920	.900	-.080	.935			
			.900	-.111	.933	.950	.029	.942			
			.950	.008	.940	.990	.101	.946			
			.990	.096	.946						
					LOWER SURFACE						
.100	-.707	.893	.025	-.306	.893	.025	-.835	.891	.100	-.945	.884
.300	-.607	.904	.050	-.993	.882	.050	-1.054	.878	.300	-.589	.905
.600	-.424	.921	.100	-.846	.890	.100	-.869	.889	.600	-.339	.920
.800	.163	.949	.200	-.575	.900	.200	-.696	.899	.800	.117	.947
			.300	-.620	.904	.300	-.635	.903			
			.400	-.568	.907	.400	-.604	.904			
			.500	-.535	.909	.500	-.501	.910			
			.600	-.267	.924	.600	-.329	.921			
			.700	.013	.941	.700	-.059	.936			
			.800	.235	.952	.800	.167	.950			
			.900	.280	.956	.900	.223	.953			
			.950	.234	.957	.950	.269	.956			
			1.000	.122	.947						
CN=				.0017			-.0873				
CM=				-.0991			-.0787				

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = -2.99^o$; $C_L = 0.030$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.610	.903	0.000	1.001	.999	0.000	.070	.944	.050	-.426	.914
.150	-.539	.909	.012	.080	.944	.012	.053	.943	.150	-.397	.916
.300	-.476	.911	.025	-.332	.920	.025	-.156	.930	.300	-.391	.916
.450	-.415	.915	.050	-.513	.909	.050	-.449	.913	.450	-.365	.918
.600	-.457	.913	.100	-.505	.910	.100	-.426	.914	.600	-.364	.918
.800	-.400	.916	.150	-.502	.910	.150	-.408	.915	.800	-.243	.925
.950	.042	.942	.200	-.501	.910	.200	-.432	.914			
			.300	-.470	.912	.300	-.431	.914			
			.350	-.459	.912	.350	-.407	.915			
			.400	-.460	.912	.400	-.394	.916			
			.450	-.437	.914	.450	-.412	.915			
			.500	-.489	.911	.500	-.427	.914			
			.550	-.491	.910	.550	-.425	.914			
			.600	-.451	.913	.600	-.431	.914			
			.650	-.492	.910	.700	-.327	.920			
			.700	-.480	.911	.800	-.260	.924			
			.800	-.358	.918	.900	-.069	.935			
			.900	-.116	.933	.950	.033	.941			
			.950	.000	.940	.990	.112	.946			
			.990	.087	.945						
					LOWER SURFACE						
.100	-.541	.904	.025	-.525	.909	.025	-.515	.909	.100	-.768	.894
.300	-.445	.907	.050	-.749	.895	.050	-.829	.891	.300	-.525	.909
.600	-.308	.921	.100	-.710	.898	.100	-.721	.897	.600	-.316	.921
.800	.174	.950	.200	-.606	.904	.200	-.602	.904	.900	.155	.949
			.300	-.583	.905	.300	-.562	.906			
			.400	-.531	.908	.400	-.542	.908			
			.500	-.504	.910	.500	-.455	.913			
			.600	-.247	.925	.600	-.299	.922			
			.700	.035	.942	.700	-.048	.937			
			.800	.232	.953	.800	.196	.951			
			.900	.301	.957	.900	.255	.955			
			.950	.291	.957	.950	.304	.957			
			1.000	.112	.948						
CN=				.1103			.0257				
CM=				-.1020			-.0774				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = -1.95^o$; $C_L = 0.130$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.778	.894	0.000	1.005	.999	0.000	.060	.943	.050	-.629	.902
.150	-.590	.905	.012	-.159	.930	.012	-.170	.930	.150	-.510	.910
.300	-.510	.910	.025	-.523	.909	.025	-.363	.918	.300	-.441	.914
.450	-.447	.913	.050	-.705	.898	.050	-.615	.903	.450	-.404	.916
.600	-.471	.912	.100	-.613	.903	.100	-.552	.907	.600	-.401	.916
.800	-.397	.916	.150	-.579	.905	.150	-.498	.910	.800	-.273	.923
.990	.046	.942	.200	-.565	.906	.200	-.509	.910			
			.300	-.513	.909	.300	-.494	.910			
			.350	-.499	.910	.350	-.468	.912			
			.400	-.485	.911	.400	-.451	.913			
			.450	-.469	.912	.450	-.467	.912			
			.500	-.515	.909	.500	-.473	.912			
			.550	-.517	.909	.550	-.472	.912			
			.600	-.478	.911	.600	-.464	.912			
			.650	-.515	.909	.700	-.356	.919			
			.700	-.493	.911	.800	-.280	.923			
			.800	-.363	.918	.900	-.086	.935			
			.900	-.112	.933	.950	.016	.941			
			.950	.003	.940	.990	.089	.945			
			.990	.086	.945						
					LOWER SURFACE						
.100	-.462	.912	.025	-.306	.922	.025	-.332	.920	.100	-.686	.899
.300	-.495	.910	.050	-.567	.904	.050	-.673	.900	.300	-.501	.910
.600	-.290	.923	.100	-.582	.905	.100	-.599	.904	.600	-.324	.921
.800	.204	.952	.200	-.532	.908	.200	-.533	.908	.800	.161	.949
			.300	-.515	.909	.300	-.528	.908			
			.400	-.478	.911	.400	-.521	.909			
			.500	-.473	.912	.500	-.440	.914			
			.600	-.226	.926	.600	-.294	.922			
			.700	.046	.942	.700	-.046	.937			
			.800	.250	.954	.800	.194	.951			
			.900	.325	.959	.900	.258	.955			
			.950	.307	.958	.950	.304	.958			
			1.000	.099	.945						
CN=				.2035			.1208				
CM=				-.1031			-.0771				

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = -0.90$; $C_L = 0.226$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.903	.886	0.000	1.001	.999	0.000	.064	.943	.050	-.751	.895
.150	-.705	.898	.012	-.339	.916	.012	-.448	.913	.150	-.586	.905
.300	-.565	.906	.025	-.805	.892	.025	-.589	.905	.300	-.503	.910
.450	-.480	.911	.050	-.917	.886	.050	-.793	.893	.450	-.433	.914
.600	-.493	.911	.100	-.767	.894	.100	-.669	.900	.600	-.416	.915
.800	-.400	.916	.150	-.682	.899	.150	-.600	.904	.800	-.276	.923
.950	.043	.942	.200	-.648	.901	.200	-.593	.905			
			.300	-.604	.904	.300	-.548	.907			
			.350	-.562	.907	.350	-.506	.910			
			.400	-.560	.907	.400	-.489	.911			
			.450	-.509	.910	.450	-.501	.910			
			.500	-.551	.907	.500	-.511	.910			
			.550	-.556	.907	.550	-.484	.911			
			.600	-.512	.909	.600	-.482	.911			
			.650	-.536	.908	.700	-.368	.918			
			.700	-.513	.909	.800	-.282	.923			
			.800	-.371	.918	.900	-.092	.934			
			.900	-.128	.932	.950	.012	.940			
			.950	-.011	.939	.990	.080	.944			
			.990	.071	.944						
					LOWER SURFACE						
.100	-.405	.916	.025	-.187	.929	.025	-.113	.933	.100	-.594	.905
.300	-.462	.912	.050	-.415	.915	.050	-.472	.912	.300	-.468	.912
.600	-.290	.923	.100	-.456	.913	.100	-.482	.911	.600	-.312	.921
.800	.220	.953	.200	-.471	.912	.200	-.467	.912	.800	.170	.950
			.300	-.456	.913	.300	-.468	.912			
			.400	-.453	.913	.400	-.491	.911			
			.500	-.461	.912	.500	-.408	.916			
			.600	-.222	.927	.600	-.278	.923			
			.700	.052	.943	.700	-.037	.937			
			.800	.246	.954	.800	.204	.952			
			.900	.321	.959	.900	.266	.955			
			.950	.306	.958	.950	.308	.958			
			1.000	.087	.945						
CN=				.3023			.2176				
CM=				-.1012			-.0739				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = 0.18^o$; $C_L = 0.321$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.109	.874	0.000	.970	.997	0.000	.067	.944	.050	-.951	.884
.150	-.762	.895	.012	-.686	.899	.012	-.697	.899	.150	-.657	.901
.300	-.614	.903	.025	-1.037	.878	.025	-.831	.891	.300	-.540	.908
.450	-.502	.910	.050	-1.101	.875	.050	-.987	.881	.450	-.457	.913
.600	-.501	.910	.100	-.882	.888	.100	-.784	.893	.600	-.429	.914
.800	-.396	.916	.150	-.764	.895	.150	-.668	.900	.800	-.281	.923
.950	.042	.942	.200	-.710	.897	.200	-.664	.900			
			.300	-.630	.902	.300	-.605	.904			
			.350	-.600	.904	.350	-.563	.906			
			.400	-.582	.905	.400	-.535	.908			
			.450	-.539	.908	.450	-.536	.908			
			.500	-.582	.905	.500	-.540	.908			
			.550	-.574	.906	.550	-.517	.909			
			.600	-.531	.908	.600	-.504	.910			
			.650	-.540	.908	.700	-.379	.917			
			.700	-.522	.909	.800	-.290	.923			
			.800	-.359	.918	.900	-.086	.935			
			.900	-.119	.933	.950	.005	.940			
			.950	-.000	.940	.990	.071	.944			
			.990	.070	.944						
					LOWER SURFACE						
.100	-.307	.921	.025	-.014	.939	.025	.075	.944	.100	-.478	.911
.300	-.400	.916	.050	-.269	.924	.050	-.325	.920	.300	-.428	.914
.600	-.262	.924	.100	-.355	.919	.100	-.397	.916	.600	-.301	.922
.800	.222	.953	.200	-.377	.917	.200	-.381	.917	.800	.174	.950
			.300	-.411	.915	.300	-.417	.915			
			.400	-.428	.914	.400	-.446	.913			
			.500	-.408	.916	.500	-.384	.917			
			.600	-.202	.928	.600	-.264	.924			
			.700	.068	.944	.700	-.026	.938			
			.800	.265	.955	.800	.204	.952			
			.900	.340	.960	.900	.267	.955			
			.950	.314	.958	.950	.310	.958			
			1.000	.080	.944						
CN=				.3868			.3092				
CM=				-.0595			-.0712				

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = 1.27^o$; $C_L = 0.417$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.337	.861	0.000	.908	.993	0.000	.069	.944	.050	-1.205	.869
.150	-.852	.890	.012	-1.021	.860	.012	-.977	.882	.150	-.732	.897
.300	-.671	.900	.025	-1.363	.859	.025	-1.129	.873	.300	-.588	.905
.450	-.538	.908	.050	-1.287	.864	.050	-1.202	.869	.450	-.485	.911
.600	-.523	.909	.100	-1.005	.881	.100	-.909	.886	.600	-.439	.914
.800	-.390	.917	.150	-.872	.888	.150	-.761	.895	.800	-.283	.923
.950	.038	.942	.200	-.802	.892	.200	-.744	.896			
			.300	-.698	.899	.300	-.661	.901			
			.350	-.659	.901	.350	-.602	.904			
			.400	-.629	.903	.400	-.567	.906			
			.450	-.573	.906	.450	-.562	.907			
			.500	-.615	.904	.500	-.553	.907			
			.550	-.598	.905	.550	-.536	.908			
			.600	-.553	.907	.600	-.512	.910			
			.650	-.566	.906	.700	-.379	.917			
			.700	-.530	.909	.800	-.284	.923			
			.800	-.368	.918	.900	-.085	.935			
			.900	-.112	.933	.950	.000	.940			
			.950	-.010	.939	.990	.059	.943			
			.990	.048	.943						
					LOWER SURFACE						
.100	-.213	.927	.025	.161	.949	.025	.264	.955	.100	-.345	.919
.300	-.354	.919	.050	-.088	.935	.050	-.187	.929	.300	-.397	.917
.600	-.247	.925	.100	-.245	.925	.100	-.257	.925	.600	-.285	.923
.800	.239	.954	.200	-.309	.921	.200	-.307	.922	.800	.185	.951
			.300	-.348	.919	.300	-.367	.918			
			.400	-.367	.918	.400	-.407	.916			
			.500	-.391	.917	.500	-.352	.919			
			.600	-.177	.929	.600	-.237	.926			
			.700	.082	.945	.700	-.017	.939			
			.800	.268	.956	.800	.218	.953			
			.900	.349	.960	.900	.281	.956			
			.950	.312	.958	.950	.319	.959			
			1.000	.072	.944						
CN=				.4852			.4043				
CM=				-.0586			-.0671				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = 2.34^o$; $C_L = 0.507$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.523	.850	0.000	.844	.990	0.000	.069	.944	.050	-1.409	.857
.150	-.947	.884	.012	-1.333	.861	.012	-1.277	.865	.150	-.788	.893
.300	-.711	.898	.025	-1.543	.849	.025	-1.340	.861	.300	-.624	.903
.450	-.566	.906	.050	-1.558	.848	.050	-1.381	.858	.450	-.502	.910
.600	-.529	.909	.100	-1.115	.874	.100	-1.031	.879	.600	-.454	.913
.800	-.386	.917	.150	-.963	.883	.150	-.858	.889	.800	-.278	.923
.990	.028	.941	.200	-.885	.888	.200	-.813	.892			
			.300	-.755	.895	.300	-.703	.898			
			.350	-.703	.898	.350	-.650	.902			
			.400	-.663	.901	.400	-.611	.904			
			.450	-.613	.904	.450	-.600	.904			
			.500	-.639	.902	.500	-.590	.905			
			.550	-.619	.903	.550	-.563	.907			
			.600	-.570	.906	.600	-.531	.909			
			.650	-.572	.906	.700	-.392	.917			
			.700	-.533	.908	.800	-.291	.923			
			.800	-.368	.918	.900	-.089	.935			
			.900	-.106	.934	.950	.002	.940			
			.950	-.006	.939	.990	.043	.942			
			.990	.053	.943						
					LOWER SURFACE						
.100	-.133	.932	.025	.288	.957	.025	.408	.964	.100	-.253	.925
.300	-.311	.922	.050	.021	.941	.050	-.032	.938	.300	-.347	.919
.600	-.230	.926	.100	-.145	.931	.100	-.166	.930	.600	-.278	.923
.800	.251	.955	.200	-.224	.927	.200	-.256	.925	.800	.182	.950
			.300	-.300	.922	.300	-.313	.921			
			.400	-.320	.921	.400	-.367	.918			
			.500	-.355	.919	.500	-.332	.920			
			.600	-.163	.930	.600	-.228	.926			
			.700	.087	.945	.700	-.010	.939			
			.800	.275	.956	.800	.220	.953			
			.900	.357	.961	.900	.282	.956			
			.950	.318	.959	.950	.311	.958			
			1.000	.069	.944						
CN=				.5737			.4895				
CM=				-.0954			-.0638				

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = 3.41^o$; $C_L = 0.598$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.786	.835	0.000	.704	.981	0.000	.071	.944	.050	-1.584	.846
.150	-1.033	.879	.012	-1.625	.844	.012	-1.600	.846	.150	-.892	.887
.300	-.765	.895	.025	-2.015	.821	.025	-1.662	.842	.300	-.673	.900
.450	-.594	.905	.050	-1.749	.837	.050	-1.613	.845	.450	-.525	.909
.600	-.548	.907	.100	-1.267	.865	.100	-1.165	.871	.600	-.460	.913
.800	-.394	.917	.150	-1.055	.878	.150	-.953	.884	.800	-.270	.924
.990	.029	.941	.200	-.962	.883	.200	-.898	.887			
			.300	-.804	.892	.300	-.759	.895			
			.350	-.742	.896	.350	-.691	.899			
			.400	-.700	.899	.400	-.648	.902			
			.450	-.640	.902	.450	-.631	.903			
			.500	-.660	.901	.500	-.613	.904			
			.550	-.634	.902	.550	-.578	.906			
			.600	-.588	.905	.600	-.542	.908			
			.650	-.582	.905	.700	-.402	.916			
			.700	-.533	.908	.800	-.292	.923			
			.800	-.375	.918	.900	-.092	.934			
			.900	-.107	.933	.950	-.013	.939			
			.950	-.006	.939	.990	.029	.941			
			.990	.027	.941						
					LOWER SURFACE						
.100	-.023	.938	.025	.414	.964	.025	.551	.972	.100	-.182	.929
.300	-.255	.925	.050	.147	.948	.050	.087	.945	.300	-.299	.922
.600	-.214	.927	.100	-.032	.938	.100	-.077	.935	.600	-.269	.924
.800	.258	.955	.200	-.166	.930	.200	-.204	.928	.800	.182	.950
			.300	-.249	.925	.300	-.271	.924			
			.400	-.279	.923	.400	-.321	.921			
			.500	-.323	.921	.500	-.304	.922			
			.600	-.147	.931	.600	-.212	.927			
			.700	.099	.946	.700	-.001	.940			
			.800	.289	.957	.800	.224	.953			
			.900	.358	.961	.900	.292	.957			
			.950	.324	.959	.950	.316	.958			
			1.000	.050	.943						
CN=				.6668			.5799				
CM=				-.0927			-.0605				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = -3^o$; $\alpha = 4.50^o$; $C_L = 0.692$

STATION .1532			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.004	.821	0.000	.565	.973	0.000	.073	.944	.050	-1.830	.831
.150	-1.115	.874	.012	-2.026	.820	.012	-1.977	.823	.150	-.973	.882
.300	-.810	.892	.025	-2.330	.802	.025	-1.938	.825	.300	-.716	.897
.450	-.618	.903	.050	-1.962	.824	.050	-1.873	.829	.450	-.549	.907
.600	-.556	.907	.100	-1.410	.856	.100	-1.278	.864	.600	-.467	.912
.800	-.374	.917	.150	-1.197	.869	.150	-1.063	.877	.800	-.265	.924
.950	.016	.941	.200	-1.056	.877	.200	-.970	.882			
			.300	-.859	.889	.300	-.817	.891			
			.350	-.795	.893	.350	-.732	.896			
			.400	-.747	.895	.400	-.683	.899			
			.450	-.680	.899	.450	-.664	.900			
			.500	-.704	.898	.500	-.640	.902			
			.550	-.655	.901	.550	-.602	.904			
			.600	-.610	.904	.600	-.561	.906			
			.650	-.594	.905	.700	-.403	.916			
			.700	-.552	.907	.800	-.286	.923			
			.800	-.356	.919	.900	-.091	.934			
			.900	-.102	.934	.950	-.022	.938			
			.950	-.012	.939	.990	.015	.940			
			.990	.023	.941						
					LOWER SURFACE						
.100	.083	.945	.025	.549	.972	.025	.661	.979	.100	-.064	.936
.300	-.214	.927	.050	.290	.956	.050	.237	.954	.300	-.267	.924
.600	-.194	.928	.100	.077	.944	.100	.025	.941	.600	-.254	.925
.800	.266	.955	.200	-.090	.934	.200	-.125	.932	.800	.179	.950
			.300	-.158	.928	.300	-.218	.927			
			.400	-.250	.925	.400	-.266	.924			
			.500	-.299	.922	.500	-.280	.923			
			.600	-.117	.933	.600	-.196	.928			
			.700	.102	.946	.700	.007	.940			
			.800	.298	.957	.800	.235	.953			
			.900	.362	.961	.900	.292	.957			
			.950	.329	.959	.950	.324	.959			
			1.000	.032	.941						
CN=				.7637			.6757				
CM=				-.0685			-.0570				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -4.10^o$; $C_L = -0.059$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.364	.918	0.000	.970	.997	0.000	.066	.944	.050	-.271	.924
.150	-.458	.913	.012	.279	.956	.012	.263	.955	.150	-.374	.918
.300	-.418	.915	.025	-.082	.935	.025	-.022	.938	.300	-.379	.917
.450	-.405	.916	.050	-.368	.918	.050	-.305	.922	.450	-.384	.917
.600	-.439	.914	.100	-.410	.916	.100	-.330	.920	.600	-.406	.916
.800	-.398	.916	.150	-.418	.915	.150	-.326	.921	.800	-.313	.921
.990	.042	.942	.200	-.442	.914	.200	-.384	.917			
			.300	-.424	.915	.300	-.407	.916			
			.350	-.415	.915	.350	-.381	.917			
			.400	-.426	.915	.400	-.387	.917			
			.450	-.432	.914	.450	-.416	.915			
			.500	-.472	.912	.500	-.444	.914			
			.550	-.468	.912	.550	-.454	.913			
			.600	-.454	.913	.600	-.452	.913			
			.650	-.482	.911	.700	-.415	.915			
			.700	-.471	.912	.800	-.326	.921			
			.800	-.356	.919	.900	-.078	.935			
			.900	-.111	.933	.950	.012	.940			
			.950	.000	.940	.990	.086	.945			
			.990	.092	.945						
					LOWER SURFACE						
.100	-.797	.893	.025	-.733	.897	.025	-.746	.896	.100	-.867	.885
.300	-.598	.904	.050	-.936	.885	.050	-.928	.885	.300	-.546	.908
.600	-.328	.920	.100	-.837	.890	.100	-.818	.891	.600	-.283	.923
.800	.150	.949	.200	-.666	.900	.200	-.649	.901	.800	.199	.951
			.300	-.623	.903	.300	-.605	.904			
			.400	-.566	.906	.400	-.539	.908			
			.500	-.522	.909	.500	-.446	.913			
			.600	-.260	.924	.600	-.261	.924			
			.700	.033	.942	.700	.005	.940			
			.800	.198	.951	.800	.242	.954			
			.900	.289	.957	.900	.258	.955			
			.950	.281	.956	.950	.300	.957			
			1.000	.104	.946						
CN=				.0287			.0070				
CM=				-.1020			-.1025				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -3.02^o$; $C_L = 0.043$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.564	.906	0.000	1.003	.999	0.000	.047	.942	.050	-.448	.913
.150	-.528	.908	.012	.083	.965	.012	.033	.942	.150	-.435	.914
.300	-.466	.912	.025	-.300	.922	.025	-.213	.927	.300	-.421	.915
.450	-.436	.914	.050	-.538	.908	.050	-.489	.911	.450	-.408	.916
.600	-.458	.913	.100	-.538	.908	.100	-.470	.912	.600	-.434	.914
.800	-.401	.916	.150	-.492	.911	.150	-.420	.915	.800	-.342	.919
.990	.038	.942	.200	-.511	.909	.200	-.463	.912			
			.300	-.472	.912	.300	-.473	.912			
			.350	-.457	.913	.350	-.438	.914			
			.400	-.458	.913	.400	-.435	.914			
			.450	-.450	.913	.450	-.460	.912			
			.500	-.484	.911	.500	-.481	.911			
			.550	-.498	.910	.550	-.486	.911			
			.600	-.478	.911	.600	-.487	.911			
			.650	-.504	.910	.700	-.437	.914			
			.700	-.482	.911	.800	-.342	.919			
			.800	-.368	.918	.900	-.088	.934			
			.900	-.119	.933	.950	.002	.940			
			.950	.001	.940	.990	.067	.944			
			.990	.085	.945						
					LOWER SURFACE						
.100	-.655	.901	.025	-.583	.905	.025	-.557	.907	.100	-.783	.893
.300	-.541	.908	.050	-.733	.896	.050	-.798	.893	.300	-.518	.909
.600	-.312	.921	.100	-.704	.898	.100	-.704	.898	.600	-.282	.923
.800	.195	.951	.200	-.604	.904	.200	-.573	.906	.800	.206	.952
			.300	-.564	.906	.300	-.559	.907			
			.400	-.514	.909	.400	-.520	.909			
			.500	-.492	.911	.500	-.432	.914			
			.600	-.244	.925	.600	-.256	.925			
			.700	.049	.943	.700	.010	.940			
			.800	.230	.953	.800	.246	.954			
			.900	.306	.958	.900	.269	.955			
			.950	.307	.958	.950	.308	.958			
			1.000	.111	.946						
CN=				.1238			.1025				
CM=				-.1050			-.1018				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -2.48^o$; $C_L = 0.098$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.529	.903	0.000	1.018	1.000	0.000	.056	.943	.050	-.551	.907
.150	-.599	.905	.012	-.032	.938	.012	-.113	.933	.150	-.459	.913
.300	-.437	.911	.025	-.490	.911	.025	-.315	.921	.300	-.445	.914
.450	-.441	.914	.050	-.671	.900	.050	-.562	.907	.450	-.418	.915
.600	-.465	.912	.100	-.592	.905	.100	-.503	.910	.600	-.462	.913
.800	-.409	.916	.150	-.544	.908	.150	-.480	.912	.800	-.350	.919
.990	.038	.942	.200	-.559	.907	.200	-.515	.910			
			.300	-.494	.911	.300	-.488	.911			
			.350	-.498	.911	.350	-.474	.912			
			.400	-.481	.912	.400	-.466	.912			
			.450	-.465	.913	.450	-.488	.911			
			.500	-.505	.910	.500	-.500	.910			
			.550	-.512	.910	.550	-.509	.910			
			.600	-.487	.911	.600	-.507	.910			
			.650	-.516	.910	.700	-.448	.914			
			.700	-.492	.911	.800	-.346	.920			
			.800	-.371	.918	.900	-.089	.935			
			.900	-.125	.932	.950	.005	.940			
			.950	.008	.940	.990	.064	.944			
			.990	.093	.945						
					LOWER SURFACE						
.100	-.591	.905	.025	-.441	.914	.025	-.334	.920	.100	-.740	.896
.300	-.510	.910	.050	-.683	.900	.050	-.756	.895	.300	-.491	.911
.600	-.312	.921	.100	-.631	.903	.100	-.632	.903	.600	-.284	.923
.800	.210	.952	.200	-.562	.907	.200	-.547	.908	.800	.221	.953
			.300	-.530	.909	.300	-.544	.908			
			.400	-.498	.911	.400	-.507	.910			
			.500	-.474	.912	.500	-.418	.915			
			.600	-.234	.926	.600	-.243	.926			
			.700	.047	.943	.700	.011	.940			
			.800	.240	.954	.800	.255	.955			
			.900	.319	.959	.900	.283	.956			
			.950	.306	.958	.950	.320	.959			
			1.000	.113	.946						
CN=				.1782			.1553				
CM=				-.1044			-.1015				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -1.94^o$; $C_L = 0.148$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.753	.895	0.000	1.009	.999	0.000	.074	.944	.050	-.607	.904
.150	-.619	.903	.012	-.157	.930	.012	-.198	.928	.150	-.528	.909
.300	-.622	.909	.025	-.521	.909	.025	-.433	.914	.300	-.458	.913
.450	-.455	.913	.050	-.757	.895	.050	-.661	.901	.450	-.427	.915
.600	-.471	.912	.100	-.683	.899	.100	-.563	.907	.600	-.440	.914
.800	-.405	.916	.150	-.606	.904	.150	-.506	.910	.800	-.356	.919
.990	.040	.942	.200	-.589	.905	.200	-.535	.908			
			.300	-.530	.908	.300	-.514	.909			
			.350	-.510	.910	.350	-.466	.912			
			.400	-.506	.910	.400	-.480	.911			
			.450	-.486	.911	.450	-.484	.911			
			.500	-.527	.909	.500	-.510	.910			
			.550	-.531	.908	.550	-.510	.910			
			.600	-.502	.910	.600	-.503	.910			
			.650	-.525	.909	.700	-.447	.913			
			.700	-.503	.910	.800	-.340	.920			
			.800	-.373	.918	.900	-.085	.935			
			.900	-.116	.933	.950	.003	.940			
			.950	.004	.940	.990	.063	.943			
			.990	.092	.945						
					LOWER SURFACE						
.100	-.535	.909	.025	-.345	.919	.025	-.262	.924	.100	-.688	.899
.300	-.491	.911	.050	-.552	.907	.050	-.613	.904	.300	-.464	.912
.600	-.299	.923	.100	-.566	.906	.100	-.573	.906	.600	-.262	.924
.800	.220	.953	.200	-.511	.910	.200	-.490	.911	.800	.233	.953
			.300	-.506	.910	.300	-.481	.911			
			.400	-.469	.912	.400	-.480	.911			
			.500	-.461	.913	.500	-.390	.917			
			.600	-.222	.927	.600	-.239	.926			
			.700	.060	.943	.700	.034	.942			
			.800	.258	.955	.800	.260	.955			
			.900	.320	.959	.900	.301	.957			
			.950	.308	.958	.950	.326	.959			
			1.000	.109	.946						
CN=				.2292			.2040				
CM=				-.1049			-.0958				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -1.37^o$; $C_L = 0.199$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.834	.891	0.000	1.017	1.000	0.000	.058	.943	.050	-.726	.897
.150	-.671	.900	.012	-.308	.922	.012	-.338	.920	.150	-.562	.907
.300	-.546	.908	.025	-.668	.900	.025	-.524	.909	.300	-.468	.912
.450	-.482	.911	.050	-.823	.891	.050	-.762	.895	.450	-.452	.913
.600	-.436	.911	.100	-.719	.897	.100	-.655	.901	.600	-.456	.913
.800	-.401	.916	.150	-.654	.901	.150	-.556	.907	.800	-.352	.919
.990	.037	.942	.200	-.628	.903	.200	-.571	.906			
			.300	-.558	.907	.300	-.549	.907			
			.350	-.536	.908	.350	-.487	.910			
			.400	-.524	.909	.400	-.508	.910			
			.450	-.504	.910	.450	-.508	.910			
			.500	-.541	.908	.500	-.523	.909			
			.550	-.546	.908	.550	-.527	.909			
			.600	-.513	.910	.600	-.522	.909			
			.650	-.538	.908	.700	-.456	.913			
			.700	-.515	.909	.800	-.342	.920			
			.800	-.373	.918	.900	-.090	.934			
			.900	-.131	.932	.950	-.002	.940			
			.950	.000	.940	.990	.057	.943			
			.990	.083	.945						
					LOWER SURFACE						
.100	-.490	.911	.025	-.237	.926	.025	-.183	.929	.100	-.562	.905
.300	-.470	.912	.050	-.466	.912	.050	-.550	.907	.300	-.466	.912
.600	-.284	.923	.100	-.499	.910	.100	-.521	.909	.600	-.271	.926
.800	.224	.953	.200	-.466	.912	.200	-.466	.912	.800	.229	.953
			.300	-.496	.911	.300	-.456	.913			
			.400	-.454	.913	.400	-.470	.912			
			.500	-.444	.914	.500	-.376	.918			
			.600	-.217	.927	.600	-.232	.926			
			.700	.064	.944	.700	.044	.942			
			.800	.247	.954	.800	.258	.955			
			.900	.331	.959	.900	.301	.957			
			.950	.316	.958	.950	.319	.959			
			1.000	.106	.946						
CN=				.2759			.2508				
CM=				-.1050			-.0985				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -0.85^o$; $C_L = 0.247$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.956	.884	0.000	1.004	.999	0.000	.073	.944	.050	-.813	.892
.150	-.707	.899	.012	-.424	.915	.012	-.457	.913	.150	-.619	.903
.300	-.576	.906	.025	-.817	.892	.025	-.646	.902	.300	-.518	.909
.450	-.497	.911	.050	-.961	.883	.050	-.940	.890	.450	-.455	.913
.600	-.497	.911	.100	-.804	.893	.100	-.698	.899	.600	-.460	.913
.800	-.411	.916	.150	-.725	.897	.150	-.614	.904	.800	-.347	.919
.990	.034	.942	.200	-.665	.901	.200	-.603	.904			
			.300	-.595	.905	.300	-.563	.907			
			.350	-.558	.907	.350	-.522	.909			
			.400	-.557	.907	.400	-.518	.909			
			.450	-.521	.909	.450	-.521	.909			
			.500	-.561	.907	.500	-.539	.908			
			.550	-.559	.907	.550	-.535	.908			
			.600	-.522	.909	.600	-.522	.909			
			.650	-.547	.908	.700	-.466	.912			
			.700	-.533	.908	.800	-.346	.919			
			.800	-.384	.917	.900	-.097	.934			
			.900	-.130	.932	.950	.001	.940			
			.950	-.007	.939	.990	.043	.942			
			.990	.091	.945						
					LOWER SURFACE						
.100	-.444	.914	.025	-.152	.931	.025	-.067	.936	.100	-.561	.907
.300	-.431	.914	.050	-.420	.915	.050	-.470	.912	.300	-.438	.914
.600	-.278	.923	.100	-.436	.914	.100	-.444	.914	.600	-.253	.925
.800	.229	.953	.200	-.448	.913	.200	-.431	.914	.800	.239	.954
			.300	-.457	.913	.300	-.448	.913			
			.400	-.429	.915	.400	-.443	.914			
			.500	-.437	.914	.500	-.362	.919			
			.600	-.206	.928	.600	-.223	.927			
			.700	.060	.943	.700	.047	.943			
			.800	.258	.955	.800	.263	.955			
			.900	.334	.959	.900	.305	.958			
			.950	.313	.958	.950	.328	.959			
			1.000	.095	.945						
CN=				.3279			.2969				
CM=				-.1047			-.0977				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = -0.31^o$; $C_L = 0.297$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.090	.891	0.000	1.001	.999	0.000	.073	.944	.050	-.921	.886
.150	-.730	.897	.012	-.612	.904	.012	-.681	.901	.150	-.651	.901
.300	-.538	.905	.025	-.941	.884	.025	-.771	.894	.300	-.549	.907
.450	-.507	.910	.050	-1.024	.879	.050	-.926	.885	.450	-.467	.912
.600	-.499	.910	.100	-.817	.892	.100	-.751	.896	.600	-.474	.912
.800	-.401	.916	.150	-.760	.895	.150	-.652	.901	.800	-.361	.919
.990	.033	.942	.200	-.699	.899	.200	-.639	.902			
			.300	-.617	.903	.300	-.592	.905			
			.350	-.584	.905	.350	-.565	.908			
			.400	-.569	.906	.400	-.541	.908			
			.450	-.561	.908	.450	-.541	.908			
			.500	-.579	.906	.500	-.560	.907			
			.550	-.570	.906	.550	-.549	.907			
			.600	-.537	.908	.600	-.541	.908			
			.650	-.551	.907	.700	-.462	.913			
			.700	-.527	.909	.800	-.344	.920			
			.800	-.370	.918	.900	-.083	.935			
			.900	-.125	.932	.950	-.004	.940			
			.950	.000	.940	.990	.050	.943			
			.990	.091	.945						
					LOWER SURFACE						
.100	-.370	.918	.025	-.091	.935	.025	.036	.942	.100	-.496	.911
.300	-.422	.915	.050	-.330	.920	.050	-.395	.916	.300	-.424	.915
.600	-.255	.924	.100	-.402	.916	.100	-.391	.917	.600	-.242	.926
.800	.236	.954	.200	-.390	.917	.200	-.373	.918	.800	.241	.954
			.300	-.410	.916	.300	-.410	.916			
			.400	-.415	.915	.400	-.419	.915			
			.500	-.419	.915	.500	-.369	.919			
			.600	-.197	.928	.600	-.212	.927			
			.700	.068	.944	.700	.057	.943			
			.800	.247	.955	.800	.265	.955			
			.900	.338	.960	.900	.307	.958			
			.950	.310	.958	.950	.332	.959			
			1.000	.088	.945						
CN=				.3665			.3472				
CM=				-.1032			-.0954				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 0.23^o$; $C_L = 0.343$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.102	.875	0.000	.969	.997	0.000	.074	.944	.050	-.962	.883
.150	-.754	.895	.012	-.781	.894	.012	-.801	.892	.150	-.688	.899
.300	-.632	.902	.025	-1.079	.876	.025	-.941	.884	.300	-.565	.906
.450	-.521	.909	.050	-1.108	.874	.050	-.978	.882	.450	-.472	.912
.600	-.508	.910	.100	-.887	.887	.100	-.820	.891	.600	-.485	.911
.800	-.407	.916	.150	-.773	.893	.150	-.701	.898	.800	-.347	.919
.990	.037	.942	.200	-.739	.896	.200	-.686	.899			
			.300	-.652	.901	.300	-.621	.903			
			.350	-.611	.904	.350	-.575	.906			
			.400	-.592	.905	.400	-.545	.908			
			.450	-.557	.907	.450	-.564	.906			
			.500	-.594	.905	.500	-.564	.906			
			.550	-.586	.905	.550	-.565	.906			
			.600	-.553	.907	.600	-.533	.908			
			.650	-.561	.907	.700	-.469	.912			
			.700	-.521	.908	.800	-.328	.920			
			.800	-.380	.917	.900	-.087	.935			
			.900	-.115	.933	.950	-.001	.940			
			.950	-.000	.940	.990	.019	.941			
			.990	.073	.944						
					LOWER SURFACE						
.100	-.293	.922	.025	-.020	.939	.025	.122	.947	.100	-.432	.914
.300	-.332	.917	.050	-.263	.924	.050	-.318	.921	.300	-.402	.916
.600	-.250	.924	.100	-.331	.920	.100	-.330	.920	.600	-.225	.926
.800	.236	.954	.200	-.359	.919	.200	-.357	.919	.800	.240	.954
			.300	-.392	.917	.300	-.382	.917			
			.400	-.399	.916	.400	-.411	.915			
			.500	-.407	.916	.500	-.334	.920			
			.600	-.193	.929	.600	-.207	.928			
			.700	.075	.944	.700	.047	.943			
			.800	.266	.955	.800	.274	.956			
			.900	.334	.959	.900	.305	.958			
			.950	.318	.958	.950	.339	.960			
			1.000	.083	.945						
CN=				.4139			.3890				
CM=				-.1021			-.0931				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 1.31^o$; $C_L = 0.435$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.343	.861	0.000	.914	.994	0.000	.062	.943	.050	-1.226	.868
.150	-.857	.889	.012	-1.023	.880	.012	-1.017	.880	.150	-.732	.897
.300	-.652	.901	.025	-1.362	.860	.025	-1.194	.869	.300	-.614	.904
.450	-.552	.907	.050	-1.334	.861	.050	-1.223	.868	.450	-.520	.909
.600	-.516	.909	.100	-1.026	.879	.100	-.970	.883	.600	-.493	.911
.800	-.397	.916	.150	-.872	.888	.150	-.785	.894	.800	-.363	.918
.990	.037	.942	.200	-.814	.892	.200	-.757	.895			
			.300	-.706	.898	.300	-.686	.899			
			.350	-.672	.900	.350	-.637	.902			
			.400	-.628	.903	.400	-.603	.904			
			.450	-.534	.905	.450	-.608	.904			
			.500	-.626	.903	.500	-.610	.904			
			.550	-.611	.904	.550	-.593	.905			
			.600	-.554	.907	.600	-.560	.907			
			.650	-.568	.906	.700	-.469	.912			
			.700	-.528	.909	.800	-.338	.920			
			.800	-.376	.918	.900	-.084	.935			
			.900	-.116	.933	.950	-.029	.938			
			.550	.001	.940	.990	-.005	.940			
			.950	.061	.943						
					LOWER SURFACE						
.100	-.217	.927	.025	.170	.950	.025	.279	.956	.100	-.332	.920
.300	-.351	.919	.050	-.095	.934	.050	-.178	.929	.300	-.356	.919
.600	-.242	.926	.100	-.272	.927	.100	-.230	.926	.600	-.262	.925
.800	.239	.954	.200	-.291	.923	.200	-.282	.923	.800	.235	.954
			.300	-.336	.920	.300	-.365	.918			
			.400	-.362	.918	.400	-.376	.918			
			.500	-.376	.918	.500	-.323	.921			
			.600	-.168	.930	.600	-.133	.928			
			.700	.094	.945	.700	.043	.942			
			.800	.279	.956	.800	.272	.956			
			.900	.344	.960	.900	.296	.957			
			.950	.324	.959	.950	.324	.959			
			1.000	.058	.944						
CN=				.5036			.4775				
CM=				-.0999			-.0884				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 2.38^o$; $C_L = 0.524$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.591	.851	0.000	.826	.988	0.000	.077	.944	.050	-1.441	.855
.150	-.932	.885	.012	-1.365	.859	.012	-1.405	.857	.150	-.770	.894
.300	-.717	.898	.025	-1.636	.843	.025	-1.409	.857	.300	-.645	.902
.450	-.573	.906	.050	-1.528	.850	.050	-1.410	.857	.450	-.526	.909
.600	-.537	.908	.100	-1.147	.872	.100	-1.063	.877	.600	-.504	.910
.800	-.399	.916	.150	-.974	.882	.150	-.879	.888	.800	-.342	.920
.990	.033	.942	.200	-.898	.887	.200	-.839	.890			
			.300	-.760	.895	.300	-.732	.897			
			.350	-.716	.898	.350	-.666	.901			
			.400	-.654	.901	.400	-.638	.902			
			.450	-.631	.903	.450	-.624	.903			
			.500	-.640	.902	.500	-.626	.903			
			.550	-.628	.903	.550	-.599	.905			
			.600	-.596	.905	.600	-.579	.906			
			.650	-.585	.905	.700	-.472	.912			
			.700	-.543	.908	.800	-.325	.921			
			.800	-.371	.918	.900	-.081	.935			
			.900	-.100	.933	.950	-.040	.937			
			.950	-.000	.940	.990	-.022	.938			
			.990	.042	.942						
					LOWER SURFACE						
.100	-.091	.934	.025	.324	.959	.025	.428	.965	.100	-.228	.926
.300	-.235	.922	.050	.037	.942	.050	-.024	.938	.300	-.325	.921
.600	-.224	.927	.100	-.119	.933	.100	-.165	.930	.600	-.234	.926
.800	.250	.954	.200	-.229	.926	.200	-.235	.926	.800	.240	.954
			.300	-.290	.923	.300	-.287	.923			
			.400	-.312	.921	.400	-.296	.922			
			.500	-.346	.919	.500	-.310	.922			
			.600	-.155	.931	.600	-.179	.929			
			.700	.033	.945	.700	.067	.944			
			.800	.295	.957	.800	.278	.956			
			.900	.356	.961	.900	.315	.958			
			.950	.328	.959	.950	.330	.959			
			1.000	.059	.943						
CN=				.5913			.5640				
CM=				-.0975			-.0853				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 3.47^o$; $C_L = 0.619$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.780	.935	0.000	.694	.981	0.000	.065	.944	.050	-1.651	.943
.150	-1.046	.978	.012	-1.728	.838	.012	-1.719	.839	.150	-.912	.886
.300	-.747	.985	.025	-1.994	.823	.025	-1.763	.836	.300	-.696	.899
.450	-.604	.904	.050	-1.798	.835	.050	-1.677	.841	.450	-.555	.907
.600	-.549	.903	.100	-1.291	.864	.100	-1.214	.868	.600	-.509	.910
.800	-.337	.917	.150	-1.098	.875	.150	-.582	.882	.800	-.317	.921
.990	.027	.941	.200	-.966	.883	.200	-.932	.885			
			.300	-.812	.892	.300	-.792	.893			
			.350	-.765	.895	.350	-.716	.898			
			.400	-.716	.898	.400	-.681	.900			
			.450	-.662	.901	.450	-.658	.901			
			.500	-.678	.900	.500	-.649	.902			
			.550	-.650	.902	.550	-.615	.904			
			.600	-.605	.904	.600	-.577	.906			
			.650	-.594	.905	.700	-.474	.912			
			.700	-.547	.908	.800	-.315	.921			
			.800	-.371	.918	.900	-.096	.934			
			.900	-.106	.934	.950	-.059	.936			
			.950	-.010	.939	.990	-.063	.937			
			.990	.034	.942						
					LOWER SURFACE						
.100	.006	.940	.025	.441	.966	.025	.580	.974	.100	-.129	.932
.300	-.258	.925	.050	.172	.950	.050	.113	.946	.300	-.278	.923
.600	-.208	.928	.100	-.006	.939	.100	-.040	.937	.600	-.223	.926
.800	.253	.955	.200	-.155	.931	.200	-.178	.929	.800	.236	.954
			.300	-.239	.926	.300	-.247	.925			
			.400	-.272	.924	.400	-.266	.924			
			.500	-.321	.921	.500	-.286	.923			
			.600	-.139	.932	.600	-.166	.930			
			.700	.106	.946	.700	.063	.944			
			.800	.294	.957	.800	.280	.956			
			.900	.366	.961	.900	.304	.958			
			.950	.330	.959	.950	.334	.959			
			1.000	.037	.942						
CN=				.6904			.6580				
CM=				-.0946			-.0797				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 4.53^o$; $C_L = 0.705$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.347	.923	0.000	.548	.972	0.000	.057	.943	.050	-1.922	.927
.150	-1.135	.973	.012	-2.084	.817	.012	-2.135	.814	.150	-.968	.883
.300	-.820	.892	.025	-2.340	.801	.025	-2.074	.818	.300	-.732	.897
.450	-.632	.903	.050	-2.041	.820	.050	-1.898	.828	.450	-.572	.906
.600	-.551	.907	.100	-1.339	.857	.100	-1.283	.864	.600	-.512	.910
.800	-.379	.918	.150	-1.177	.870	.150	-1.073	.877	.800	-.297	.922
.990	.021	.941	.200	-1.049	.878	.200	-.990	.882			
			.300	-.866	.889	.300	-.829	.891			
			.350	-.798	.893	.350	-.746	.896			
			.400	-.746	.896	.400	-.694	.899			
			.450	-.694	.899	.450	-.680	.900			
			.500	-.700	.899	.500	-.662	.901			
			.550	-.667	.901	.550	-.648	.902			
			.600	-.616	.904	.600	-.593	.905			
			.650	-.604	.904	.700	-.476	.912			
			.700	-.546	.908	.800	-.297	.922			
			.800	-.353	.919	.900	-.106	.934			
			.900	-.101	.934	.950	-.062	.936			
			.950	-.009	.939	.990	-.067	.936			
			.990	.023	.941						
					LOWER SURFACE						
.100	.090	.945	.025	.570	.973	.025	.658	.981	.100	-.039	.938
.300	-.211	.927	.050	.306	.958	.050	.241	.954	.300	-.246	.925
.600	-.194	.929	.100	.077	.944	.100	.029	.942	.600	-.207	.928
.800	.274	.956	.200	-.092	.934	.200	-.109	.933	.800	.231	.953
			.300	-.194	.929	.300	-.182	.929			
			.400	-.235	.926	.400	-.239	.926			
			.500	-.294	.923	.500	-.253	.925			
			.600	-.117	.933	.600	-.151	.931			
			.700	.111	.946	.700	.084	.945			
			.800	.293	.957	.800	.286	.957			
			.900	.366	.961	.900	.318	.959			
			.950	.335	.960	.950	.330	.959			
			1.000	.030	.942						
CN=				.7726			.7390				
CM=				-.0894			-.0753				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 6.68^o$; $C_L = 0.881$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.532	.791	0.000	.173	.950	0.000	.066	.944	.050	-2.388	.799
.150	-1.294	.864	.012	-2.917	.768	.012	-2.991	.769	.150	-1.174	.871
.300	-.892	.887	.025	-3.069	.759	.025	-2.665	.783	.300	-.808	.892
.450	-.668	.900	.050	-2.543	.790	.050	-2.357	.801	.450	-.612	.904
.600	-.575	.906	.100	-1.640	.842	.100	-1.570	.847	.600	-.506	.910
.800	-.346	.919	.150	-1.375	.859	.150	-1.266	.865	.800	-.326	.921
.990	.002	.940	.200	-1.220	.869	.200	-1.140	.873			
			.300	-.958	.883	.300	-.922	.885			
			.350	-.868	.889	.350	-.840	.890			
			.400	-.811	.892	.400	-.775	.894			
			.450	-.747	.896	.450	-.736	.896			
			.500	-.743	.896	.500	-.713	.898			
			.550	-.699	.899	.550	-.667	.900			
			.600	-.643	.902	.600	-.620	.903			
			.650	-.611	.904	.700	-.460	.913			
			.700	-.534	.908	.800	-.290	.923			
			.800	-.351	.919	.900	-.115	.933			
			.900	-.087	.935	.950	-.115	.933			
			.950	-.027	.938	.990	-.106	.934			
			.990	-.007	.939						
					LOWER SURFACE						
.100	.229	.953	.025	.745	.984	.025	.843	.989	.100	.099	.966
.300	-.117	.933	.050	.530	.971	.050	.447	.966	.300	-.168	.930
.600	-.149	.931	.100	.242	.954	.100	.199	.952	.600	-.196	.928
.800	.235	.957	.200	.042	.942	.200	.017	.941	.800	.242	.954
			.300	-.074	.935	.300	-.096	.934			
			.400	-.152	.931	.400	-.171	.930			
			.500	-.236	.926	.500	-.203	.928			
			.600	-.073	.935	.600	-.112	.933			
			.700	.131	.947	.700	.084	.945			
			.800	.314	.958	.800	.286	.957			
			.900	.383	.962	.900	.311	.958			
			.950	.332	.959	.950	.319	.959			
			1.000	.004	.940						
CN=				.9451			.9045				
CM=				-.0812			-.0658				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 8.82^o$; $C_L = 1.052$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.703	.781	0.000	-.320	.921	0.000	.085	.945	.050	-3.044	.761
.150	-1.456	.854	.012	-3.760	.719	.012	-3.810	.714	.150	-1.291	.844
.300	-.965	.883	.025	-3.815	.716	.025	-3.308	.745	.300	-.842	.889
.450	-.710	.898	.050	-3.013	.763	.050	-2.856	.772	.450	-.626	.903
.600	-.583	.906	.100	-1.935	.826	.100	-1.827	.832	.600	-.529	.909
.800	-.338	.922	.150	-1.576	.847	.150	-1.429	.856	.800	-.341	.920
.990	-.018	.939	.200	-1.352	.860	.200	-1.272	.865			
			.300	-1.046	.878	.300	-.989	.882			
			.350	-.953	.884	.350	-.893	.887			
			.400	-.849	.889	.400	-.813	.892			
			.450	-.801	.893	.450	-.776	.894			
			.500	-.775	.894	.500	-.729	.897			
			.550	-.726	.897	.550	-.674	.900			
			.600	-.651	.902	.600	-.600	.905			
			.650	-.607	.904	.700	-.439	.914			
			.700	-.519	.909	.800	-.241	.926			
			.800	-.310	.922	.900	-.134	.932			
			.900	-.097	.934	.950	-.131	.932			
			.950	-.055	.937	.990	-.134	.932			
			.990	-.055	.937						
					LOWER SURFACE						
.100	.399	.963	.025	.876	.991	.025	.972	.997	.100	.302	.958
.300	-.024	.938	.050	.669	.979	.050	.623	.977	.300	-.082	.935
.600	-.119	.933	.100	.411	.964	.100	.374	.962	.600	-.149	.931
.800	.232	.957	.200	.154	.949	.200	.127	.947	.800	.244	.954
			.300	.028	.942	.300	.000	.940			
			.400	-.079	.935	.400	-.095	.934			
			.500	-.167	.930	.500	-.129	.932			
			.600	-.039	.938	.600	-.065	.936			
			.700	.154	.949	.700	.116	.947			
			.800	.327	.959	.800	.301	.958			
			.900	.383	.962	.900	.320	.959			
			.950	.326	.959	.950	.326	.959			
			1.000	-.031	.938						
CN=				1.1153			1.0615				
CM=				-.0710			-.0546				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 10.93^o$; $C_L = 1.213$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.138	.755	0.000	-.974	.888	0.000	.076	.945	.050	-3.761	.719
.150	-1.619	.845	.012	-4.323	.650	.012	-4.697	.664	.150	-1.423	.856
.300	-1.043	.879	.025	-4.664	.666	.025	-4.151	.696	.300	-.928	.885
.450	-.734	.897	.050	-3.471	.736	.050	-3.295	.746	.450	-.688	.899
.600	-.583	.906	.100	-2.282	.810	.100	-2.117	.815	.600	-.589	.905
.800	-.357	.924	.150	-1.759	.836	.150	-1.633	.844	.800	-.387	.917
.990	-.046	.937	.200	-1.488	.852	.200	-1.405	.857			
			.300	-1.140	.873	.300	-1.091	.876			
			.350	-1.011	.880	.350	-.966	.883			
			.400	-.925	.886	.400	-.884	.888			
			.450	-.864	.890	.450	-.822	.892			
			.500	-.792	.893	.500	-.765	.895			
			.550	-.734	.897	.550	-.698	.899			
			.600	-.665	.902	.600	-.619	.903			
			.650	-.597	.905	.700	-.408	.916			
			.700	-.512	.910	.800	-.239	.926			
			.800	-.252	.925	.900	-.166	.930			
			.900	-.117	.933	.950	-.160	.930			
			.950	-.087	.935	.990	-.158	.931			
			.990	-.076	.935						
					LOWER SURFACE						
.100	.551	.972	.025	.952	.996	.025	.994	.998	.100	.416	.984
.300	.060	.943	.050	.789	.986	.050	.761	.985	.300	-.026	.938
.600	-.018	.935	.100	.535	.971	.100	.498	.969	.600	-.126	.932
.800	.311	.958	.200	.256	.955	.200	.256	.955	.800	.262	.955
			.300	.126	.947	.300	.071	.944			
			.400	-.011	.939	.400	-.015	.939			
			.500	-.113	.933	.500	-.090	.935			
			.600	.004	.940	.600	-.042	.937			
			.700	.175	.950	.700	.130	.948			
			.800	.338	.960	.800	.305	.958			
			.900	.392	.963	.900	.316	.958			
			.950	.331	.959	.950	.321	.959			
			1.000	-.070	.936						
CN=				1.2744			1.2190				
CM=				-.0589			-.0453				

(a) M = 0.30. Continued.

$\delta_a = 0^o$; $\alpha = 13.05^o$; $C_L = 1.364$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.573	.730	0.000	-1.520	.851	0.000	.071	.944	.050	-4.387	.682
.150	-1.763	.837	.012	-5.748	.600	.012	-5.847	.596	.150	-1.543	.849
.300	-1.044	.876	.025	-5.409	.622	.025	-4.941	.649	.300	-.946	.886
.450	-.731	.897	.050	-3.934	.709	.050	-3.779	.718	.450	-.772	.896
.600	-.543	.908	.100	-2.443	.795	.100	-2.360	.801	.600	-.625	.903
.800	-.336	.923	.150	-1.919	.827	.150	-1.823	.833	.800	-.415	.915
.990	-.043	.936	.200	-1.614	.845	.200	-1.528	.850			
			.300	-1.203	.869	.300	-1.163	.872			
			.350	-1.058	.878	.350	-1.023	.880			
			.400	-.966	.883	.400	-.922	.886			
			.450	-.856	.890	.450	-.836	.891			
			.500	-.806	.893	.500	-.772	.894			
			.550	-.715	.898	.550	-.696	.899			
			.600	-.675	.903	.600	-.618	.904			
			.650	-.542	.908	.700	-.387	.917			
			.700	-.451	.913	.800	-.264	.925			
			.800	-.214	.927	.900	-.185	.929			
			.900	-.176	.933	.950	-.201	.928			
			.950	-.115	.933	.990	-.198	.928			
			.990	-.130	.932						
					LOWER SURFACE						
.100	.652	.978	.025	.967	.997	.025	.993	.998	.100	.526	.971
.300	.176	.947	.050	.886	.992	.050	.880	.992	.300	.072	.944
.600	-.053	.937	.100	.659	.979	.100	.616	.976	.600	-.109	.933
.800	.322	.959	.200	.358	.962	.200	.335	.960	.800	.269	.956
			.300	.199	.952	.300	.174	.950			
			.400	.059	.944	.400	.042	.942			
			.500	-.047	.937	.500	-.034	.938			
			.600	.039	.942	.600	-.015	.939			
			.700	.193	.951	.700	.159	.949			
			.800	.345	.960	.800	.314	.958			
			.900	.334	.963	.900	.328	.959			
			.950	.320	.959	.950	.318	.959			
			1.000	-.097	.934						
CN=				1.4109			1.3683				
CM=				-.0449			-.0369				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = -4.08^o$; $C_L = -0.040$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.445	.913	0.000	.975	.997	0.000	.055	.943	.050	-.325	.920
.150	-.460	.912	.012	.225	.953	.012	.225	.953	.150	-.381	.917
.300	-.423	.915	.025	-.110	.933	.025	-.038	.937	.300	-.399	.916
.450	-.402	.916	.050	-.384	.917	.050	-.312	.921	.450	-.401	.916
.600	-.437	.914	.100	-.391	.917	.100	-.358	.919	.600	-.456	.913
.800	-.318	.916	.150	-.427	.914	.150	-.357	.919	.800	-.397	.916
.990	.041	.942	.200	-.447	.913	.200	-.392	.917			
			.300	-.423	.915	.300	-.425	.915			
			.350	-.425	.915	.350	-.415	.915			
			.400	-.422	.915	.400	-.415	.915			
			.450	-.418	.915	.450	-.440	.914			
			.500	-.471	.912	.500	-.477	.911			
			.550	-.480	.911	.550	-.487	.911			
			.600	-.449	.913	.600	-.503	.910			
			.650	-.489	.911	.700	-.472	.912			
			.700	-.477	.912	.800	-.364	.918			
			.800	-.362	.918	.900	-.084	.935			
			.900	-.178	.932	.950	-.008	.939			
			.950	-.001	.940	.990	.027	.941			
			.990	.087	.945						
					LOWER SURFACE						
.100	-.769	.894	.025	-.749	.895	.025	-.751	.895	.100	-.855	.889
.300	-.589	.905	.050	-.936	.884	.050	-.990	.881	.300	-.563	.908
.600	-.330	.920	.100	-.811	.892	.100	-.797	.893	.600	-.269	.925
.800	.149	.948	.200	-.669	.900	.200	-.646	.902	.800	.223	.953
			.300	-.607	.904	.300	-.571	.906			
			.400	-.558	.907	.400	-.532	.908			
			.500	-.517	.909	.500	-.425	.915			
			.600	-.256	.925	.600	-.229	.926			
			.700	.034	.942	.700	.051	.943			
			.800	.208	.952	.800	.243	.955			
			.900	.208	.957	.900	.275	.956			
			.950	.290	.957	.950	.295	.957			
			1.000	.110	.946						
CN=				.0442			.0537				
CM=				-.1050			-.1174				

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = -3.01^o$; $C_L = 0.063$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.538	.905	0.000	1.014	.999	0.000	.054	.943	.050	-.496	.910
.150	-.538	.909	.012	.083	.944	.012	.001	.940	.150	-.466	.912
.300	-.432	.911	.025	-.323	.920	.025	-.233	.926	.300	-.443	.913
.450	-.429	.914	.050	-.544	.907	.050	-.511	.909	.450	-.431	.914
.600	-.456	.913	.100	-.536	.908	.100	-.491	.910	.600	-.477	.912
.800	-.401	.916	.150	-.520	.909	.150	-.452	.913	.800	-.413	.915
.990	.043	.942	.200	-.515	.909	.200	-.489	.911			
			.300	-.479	.911	.300	-.486	.911			
			.350	-.473	.912	.350	-.463	.912			
			.400	-.461	.912	.400	-.458	.912			
			.450	-.449	.913	.450	-.447	.911			
			.500	-.437	.910	.500	-.510	.909			
			.550	-.515	.909	.550	-.512	.909			
			.600	-.477	.911	.600	-.528	.908			
			.650	-.506	.910	.700	-.486	.911			
			.700	-.487	.911	.800	-.372	.918			
			.800	-.359	.918	.900	-.061	.934			
			.900	-.123	.932	.950	-.022	.938			
			.950	.004	.940	.990	.005	.940			
			.990	.081	.944						
					LOWER SURFACE						
.100	-.648	.901	.025	-.514	.909	.025	-.488	.911	.100	-.761	.895
.300	-.545	.907	.050	-.744	.896	.050	-.795	.892	.300	-.497	.910
.600	-.299	.922	.100	-.662	.900	.100	-.661	.900	.600	-.242	.925
.800	.198	.951	.200	-.580	.905	.200	-.569	.906	.800	.243	.954
			.300	-.551	.907	.300	-.530	.908			
			.400	-.504	.910	.400	-.495	.910			
			.500	-.483	.911	.500	-.395	.916			
			.600	-.241	.925	.600	-.220	.927			
			.700	.041	.942	.700	.058	.943			
			.800	.238	.954	.800	.281	.956			
			.900	.314	.958	.900	.290	.957			
			.950	.307	.958	.950	.314	.958			
			1.000	.105	.946						
CN=				.1426			.1594				
CM=				-.1053			-.1163				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = -1.91^o$; $C_L = 0.164$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.781	.891	0.000	1.015	1.000	0.000	.061	.543	.050	-.646	.901
.150	-.622	.903	.012	-.216	.527	.012	-.227	.926	.150	-.541	.908
.300	-.530	.909	.025	-.593	.905	.025	-.478	.911	.300	-.495	.910
.450	-.463	.912	.050	-.746	.895	.050	-.694	.899	.450	-.452	.913
.600	-.479	.911	.100	-.642	.902	.100	-.618	.903	.600	-.487	.911
.800	-.393	.916	.150	-.590	.905	.150	-.554	.907	.800	-.416	.915
.990	.035	.942	.200	-.582	.905	.200	-.557	.907			
			.300	-.552	.907	.300	-.538	.908			
			.350	-.527	.908	.350	-.512	.909			
			.400	-.525	.909	.400	-.500	.910			
			.450	-.499	.910	.450	-.513	.909			
			.500	-.547	.907	.500	-.543	.908			
			.550	-.539	.908	.550	-.543	.908			
			.600	-.505	.910	.600	-.550	.907			
			.650	-.528	.908	.700	-.499	.910			
			.700	-.507	.910	.800	-.367	.918			
			.800	-.375	.917	.900	-.094	.934			
			.900	-.177	.932	.950	-.033	.938			
			.950	-.006	.939	.990	-.017	.939			
			.990	.081	.944						
					LOWER SURFACE						
.100	-.531	.908	.025	-.325	.920	.025	-.246	.925	.100	-.647	.901
.300	-.493	.910	.050	-.565	.906	.050	-.586	.905	.300	-.468	.912
.600	-.294	.927	.100	-.546	.907	.100	-.542	.908	.600	-.235	.926
.800	.202	.951	.200	-.511	.909	.200	-.475	.911	.800	.264	.955
			.300	-.499	.910	.300	-.473	.912			
			.400	-.475	.912	.400	-.461	.912			
			.500	-.454	.913	.500	-.373	.918			
			.600	-.222	.926	.600	-.202	.928			
			.700	.052	.943	.700	.073	.944			
			.800	.236	.954	.800	.291	.957			
			.900	.320	.959	.900	.298	.957			
			.950	.312	.958	.950	.315	.958			
			1.000	.097	.945						
CN=				.2379			.2598				
CM=				-.1056			-.1131				

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = -0.85^o$; $C_L = 0.266$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.954	.883	0.000	.995	.898	0.000	.066	.944	.050	-.844	.890
.150	-.836	.899	.012	-.446	.813	.012	-.502	.910	.150	-.636	.903
.300	-.734	.905	.025	-.807	.892	.025	-.663	.901	.300	-.547	.907
.450	-.636	.911	.050	-.915	.886	.050	-.841	.890	.450	-.482	.911
.600	-.693	.910	.100	-.782	.894	.100	-.737	.896	.600	-.503	.910
.800	-.612	.915	.150	-.707	.898	.150	-.637	.902	.800	-.406	.916
.990	.033	.942	.200	-.663	.901	.200	-.627	.903			
			.300	-.607	.904	.300	-.584	.905			
			.350	-.583	.905	.350	-.550	.907			
			.400	-.569	.906	.400	-.530	.908			
			.450	-.570	.905	.450	-.552	.907			
			.500	-.579	.906	.500	-.563	.906			
			.550	-.568	.906	.550	-.557	.907			
			.600	-.532	.908	.600	-.557	.907			
			.650	-.550	.907	.700	-.498	.910			
			.700	-.523	.909	.800	-.354	.919			
			.800	-.383	.917	.900	-.091	.934			
			.900	-.174	.932	.950	-.046	.937			
			.950	-.004	.939	.990	-.033	.938			
			.990	.075	.944						
					LOWER SURFACE						
.100	-.426	.915	.025	-.120	.933	.025	-.027	.938	.100	-.526	.909
.300	-.445	.913	.050	-.380	.917	.050	-.441	.914	.300	-.425	.915
.600	-.237	.933	.100	-.422	.915	.100	-.444	.913	.600	-.217	.927
.800	.211	.952	.200	-.439	.914	.200	-.416	.915	.800	.275	.956
			.300	-.440	.914	.300	-.426	.915			
			.400	-.427	.915	.400	-.437	.914			
			.500	-.430	.914	.500	-.340	.920			
			.600	-.206	.928	.600	-.185	.929			
			.700	.043	.943	.700	.088	.945			
			.800	.254	.955	.800	.302	.958			
			.900	.336	.959	.900	.307	.958			
			.950	.314	.958	.950	.321	.959			
			1.000	.076	.944						
CN=				.3341			.3427				
CM=				-.1055			-.1056				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = 0.25^o$; $C_L = 0.356$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.133	.873	0.000	.964	.897	0.000	.063	.943	.050	-1.025	.879
.150	-.789	.893	.012	-.713	.898	.012	-.764	.895	.150	-.714	.898
.300	-.631	.903	.025	-1.063	.877	.025	-.919	.886	.300	-.587	.905
.450	-.525	.909	.050	-1.135	.873	.050	-1.065	.877	.450	-.510	.910
.600	-.527	.909	.100	-.887	.887	.100	-.871	.888	.600	-.514	.909
.800	-.404	.916	.150	-.805	.892	.150	-.721	.897	.800	-.401	.916
.990	.035	.942	.200	-.757	.895	.200	-.703	.898			
			.300	-.664	.901	.300	-.652	.901			
			.350	-.631	.903	.350	-.598	.904			
			.400	-.607	.904	.400	-.580	.906			
			.450	-.570	.906	.450	-.582	.905			
			.500	-.596	.905	.500	-.591	.905			
			.550	-.589	.905	.550	-.581	.905			
			.600	-.549	.907	.600	-.575	.906			
			.650	-.558	.907	.700	-.500	.910			
			.700	-.521	.909	.800	-.341	.920			
			.800	-.372	.918	.900	-.106	.933			
			.900	-.122	.933	.950	-.075	.935			
			.950	-.005	.939	.990	-.074	.935			
			.990	.061	.943						
					LOWER SURFACE						
.100	-.313	.921	.025	.033	.942	.025	.141	.948	.100	-.424	.915
.300	-.331	.917	.050	-.226	.926	.050	-.251	.925	.300	-.392	.917
.600	-.254	.924	.100	-.317	.921	.100	-.324	.921	.600	-.213	.927
.800	.223	.953	.200	-.355	.919	.200	-.342	.920	.800	.272	.956
			.300	-.388	.917	.300	-.374	.918			
			.400	-.391	.917	.400	-.389	.917			
			.500	-.401	.916	.500	-.317	.921			
			.600	-.183	.929	.600	-.174	.929			
			.700	.073	.944	.700	.091	.945			
			.800	.272	.956	.800	.305	.958			
			.900	.347	.960	.900	.305	.958			
			.950	.316	.958	.950	.316	.958			
			1.000	.089	.945						
CN=				.4236			.4387				
CM=				-.1032			-.1055				

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = 1.32^o$; $C_L = 0.450$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.371	.859	0.000	.901	.893	0.000	.070	.944	.050	-1.231	.867
.150	-.872	.888	.012	-1.005	.880	.012	-1.030	.879	.150	-.757	.895
.300	-.692	.899	.025	-1.383	.858	.025	-1.193	.869	.300	-.627	.903
.450	-.536	.909	.050	-1.354	.860	.050	-1.259	.865	.450	-.531	.908
.600	-.528	.909	.100	-1.009	.880	.100	-.984	.881	.600	-.519	.909
.800	-.404	.916	.150	-.899	.887	.150	-.798	.893	.800	-.397	.916
.990	.030	.941	.200	-.835	.890	.200	-.777	.894			
			.300	-.723	.897	.300	-.701	.898			
			.350	-.668	.900	.350	-.639	.902			
			.400	-.641	.902	.400	-.615	.903			
			.450	-.603	.904	.450	-.610	.904			
			.500	-.676	.903	.500	-.615	.903			
			.550	-.614	.903	.550	-.599	.904			
			.600	-.572	.906	.600	-.595	.904			
			.650	-.576	.906	.700	-.496	.910			
			.700	-.535	.908	.800	-.322	.921			
			.800	-.388	.917	.900	-.110	.933			
			.900	-.117	.933	.950	-.091	.934			
			.950	-.008	.939	.990	-.089	.934			
			.990	.059	.943						
					LOWER SURFACE						
.100	-.297	.927	.025	.158	.949	.025	.293	.957	.100	-.231	.920
.300	-.338	.920	.050	-.069	.936	.050	-.135	.932	.300	-.338	.920
.600	-.241	.925	.100	-.233	.926	.100	-.211	.927	.600	-.201	.928
.800	.244	.954	.200	-.286	.923	.200	-.280	.923	.800	.278	.956
			.300	-.334	.920	.300	-.321	.921			
			.400	-.350	.919	.400	-.349	.919			
			.500	-.370	.918	.500	-.287	.923			
			.600	-.171	.930	.600	-.160	.930			
			.700	.091	.945	.700	.099	.945			
			.800	.284	.956	.800	.310	.958			
			.900	.353	.960	.900	.311	.958			
			.950	.323	.959	.950	.320	.959			
			1.000	.067	.944						
CN=				.5140			.5232				
CM=				-.1028			-.1016				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) $M = 0.30$. *Continued.*

$\delta_a = 3^o$; $\alpha = 2.43^o$; $C_L = 0.540$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.534	.947	0.000	.771	.585	0.000	.073	.544	.050	-1.514	.850
.150	-.937	.883	.012	-1.336	.857	.012	-1.415	.856	.150	-.816	.892
.300	-.727	.907	.025	-1.735	.837	.025	-1.462	.853	.300	-.653	.901
.450	-.575	.906	.050	-1.592	.846	.050	-1.526	.850	.450	-.565	.908
.600	-.539	.908	.100	-1.162	.871	.100	-1.092	.875	.600	-.522	.909
.800	-.407	.916	.150	-.997	.881	.150	-.896	.887	.800	-.374	.918
.990	.034	.942	.200	-.907	.886	.200	-.848	.890			
			.300	-.771	.894	.300	-.744	.896			
			.350	-.709	.898	.350	-.681	.900			
			.400	-.675	.900	.400	-.647	.901			
			.450	-.629	.903	.450	-.636	.902			
			.500	-.650	.901	.500	-.642	.902			
			.550	-.633	.902	.550	-.614	.903			
			.600	-.595	.905	.600	-.587	.904			
			.650	-.530	.909	.700	-.490	.911			
			.700	-.553	.907	.800	-.307	.922			
			.800	-.379	.917	.900	-.119	.933			
			.900	-.116	.933	.950	-.102	.934			
			.950	-.000	.940	.990	-.105	.934			
			.990	.042	.942						
					LOWER SURFACE						
.100	-.036	.934	.025	.355	.961	.025	.443	.966	.100	-.212	.927
.300	-.239	.922	.050	.038	.942	.050	.015	.941	.300	-.304	.922
.600	-.232	.927	.100	-.129	.932	.100	-.116	.933	.600	-.188	.929
.800	.247	.956	.200	-.274	.926	.200	-.210	.927	.800	.278	.956
			.300	-.296	.923	.300	-.266	.924			
			.400	-.305	.922	.400	-.291	.923			
			.500	-.336	.920	.500	-.260	.924			
			.600	-.150	.931	.600	-.136	.932			
			.700	.092	.945	.700	.108	.946			
			.800	.287	.957	.800	.320	.959			
			.900	.354	.961	.900	.305	.958			
			.950	.320	.959	.950	.322	.959			
			1.000	.056	.943						
CN=				.6043			.6152				
CM=				-.0983			-.0968				

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = 3.47^o$; $C_L = 0.628$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.739	.934	0.000	.652	.579	0.000	.071	.944	.050	-1.680	.841
.150	-1.045	.878	.012	-1.725	.838	.012	-1.730	.838	.150	-.917	.886
.300	-.758	.894	.025	-2.032	.821	.025	-1.758	.836	.300	-.703	.898
.450	-.603	.904	.050	-1.761	.836	.050	-1.719	.838	.450	-.572	.906
.600	-.554	.907	.100	-1.295	.863	.100	-1.201	.869	.600	-.528	.909
.800	-.336	.916	.150	-1.083	.875	.150	-.994	.881	.800	-.358	.919
.990	.034	.941	.200	-.986	.882	.200	-.932	.885			
			.300	-.819	.891	.300	-.796	.893			
			.350	-.763	.895	.350	-.720	.897			
			.400	-.727	.897	.400	-.682	.900			
			.450	-.674	.900	.450	-.670	.900			
			.500	-.693	.899	.500	-.659	.901			
			.550	-.652	.901	.550	-.633	.902			
			.600	-.614	.903	.600	-.609	.904			
			.650	-.597	.905	.700	-.494	.911			
			.700	-.550	.907	.800	-.292	.923			
			.800	-.372	.918	.900	-.135	.932			
			.900	-.193	.934	.950	-.129	.932			
			.950	-.012	.939	.990	-.129	.932			
			.990	.036	.942						
					LOWER SURFACE						
.100	-.015	.940	.025	.432	.965	.025	.574	.974	.100	-.131	.932
.300	-.259	.924	.050	.191	.951	.050	.157	.949	.300	-.272	.924
.600	-.239	.927	.100	-.022	.938	.100	-.021	.938	.600	-.182	.929
.800	.259	.955	.200	-.155	.931	.200	-.150	.931	.800	.275	.956
			.300	-.231	.926	.300	-.226	.926			
			.400	-.274	.924	.400	-.249	.925			
			.500	-.312	.921	.500	-.250	.925			
			.600	-.133	.932	.600	-.129	.932			
			.700	.103	.946	.700	.120	.947			
			.800	.299	.957	.800	.322	.959			
			.900	.358	.961	.900	.322	.959			
			.950	.326	.959	.950	.325	.959			
			1.000	.038	.942						
CN=				.6908			.6999				
CM=				-.0943			-.0932				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 3^o$; $\alpha = 4.58^o$; $C_L = 0.723$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.035	.922	C.000	.502	.969	C.000	.077	.944	.050	-1.891	.928
.150	-1.156	.872	.012	-2.109	.916	.012	-2.139	.814	.150	-1.025	.879
.300	-.831	.891	.025	-2.355	.801	.025	-2.048	.819	.300	-.756	.855
.450	-.629	.903	.050	-2.081	.817	.050	-1.930	.826	.450	-.590	.905
.600	-.569	.906	.100	-1.436	.855	.100	-1.340	.861	.600	-.544	.928
.800	-.333	.917	.150	-1.184	.870	.150	-1.092	.875	.800	-.356	.919
.990	.013	.941	.200	-1.074	.877	.200	-1.016	.880			
			.300	-.881	.888	.300	-.842	.890			
			.350	-.818	.892	.350	-.766	.895			
			.400	-.758	.895	.400	-.718	.897			
			.450	-.701	.898	.450	-.699	.899			
			.500	-.709	.898	.500	-.695	.899			
			.550	-.690	.900	.550	-.648	.902			
			.600	-.628	.903	.600	-.616	.904			
			.650	-.607	.904	.700	-.484	.911			
			.700	-.555	.907	.800	-.276	.924			
			.800	-.371	.918	.900	-.143	.931			
			.900	-.111	.933	.950	-.138	.932			
			.950	-.019	.939	.990	-.144	.931			
			.990	.016	.941						
					LOWER SURFACE						
.100	.043	.945	.025	.556	.973	.025	.693	.981	.100	-.033	.938
.300	-.206	.928	.050	.306	.958	.050	.244	.954	.300	-.225	.927
.600	-.137	.928	.100	.087	.945	.100	.062	.943	.600	-.171	.930
.800	.261	.955	.200	-.084	.935	.200	-.057	.934	.800	.275	.956
			.300	-.173	.930	.300	-.175	.929			
			.400	-.228	.926	.400	-.197	.928			
			.500	-.287	.923	.500	-.224	.927			
			.600	-.117	.933	.600	-.117	.933			
			.700	.112	.946	.700	.130	.947			
			.800	.292	.957	.800	.323	.959			
			.900	.367	.961	.900	.324	.959			
			.950	.316	.958	.950	.329	.959			
			1.000	.024	.941						
CN=				.7901			.7842				
CM=				-.0904			-.0881				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = -4.09^o$; $C_L = -0.036$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.443	.913	0.000	.581	.598	0.000	.061	.943	.050	-.379	.917
.150	-.444	.913	.012	.262	.555	.012	.205	.951	.150	-.386	.916
.300	-.432	.914	.025	-.147	.530	.025	-.075	.935	.300	-.407	.915
.450	-.404	.915	.050	-.363	.518	.050	-.330	.919	.450	-.419	.914
.600	-.442	.913	.100	-.416	.514	.100	-.379	.917	.600	-.442	.910
.800	-.498	.915	.150	-.430	.513	.150	-.366	.917	.800	-.447	.912
.950	.040	.941	.200	-.435	.513	.200	-.419	.914			
			.300	-.423	.514	.300	-.430	.913			
			.350	-.420	.514	.350	-.439	.913			
			.400	-.433	.913	.400	-.432	.914			
			.450	-.419	.914	.450	-.457	.912			
			.500	-.487	.910	.500	-.488	.910			
			.550	-.490	.911	.550	-.498	.909			
			.600	-.457	.912	.600	-.524	.903			
			.650	-.489	.910	.700	-.501	.909			
			.700	-.480	.911	.800	-.333	.919			
			.800	-.363	.918	.900	-.108	.933			
			.900	-.122	.932	.950	-.086	.934			
			.950	.005	.939	.990	-.087	.934			
			.990	.091	.945						
					LOWER SURFACE						
.100	-.767	.893	.025	-.721	.856	.025	-.695	.898	.100	-.849	.889
.300	-.585	.904	.050	-.832	.886	.050	-.749	.883	.300	-.507	.909
.600	-.428	.920	.100	-.812	.891	.100	-.789	.892	.600	-.200	.927
.800	.171	.949	.200	-.669	.899	.200	-.604	.903	.800	.264	.955
			.300	-.612	.903	.300	-.557	.906			
			.400	-.545	.907	.400	-.507	.909			
			.500	-.515	.908	.500	-.489	.916			
			.600	-.246	.924	.600	-.184	.928			
			.700	.032	.941	.700	.104	.945			
			.800	.211	.952	.800	.295	.957			
			.900	.295	.957	.900	.285	.956			
			.950	.291	.957	.950	.295	.957			
			1.000	.112	.946						
CN=				.0472			.1029				
CM=				-.1057			-.1301				

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = -3.01^o$; $C_L = 0.069$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.454	.911	0.000	1.606	.559	0.000	.065	.943	.050	-.516	.909
.150	-.524	.904	.012	-.013	.534	.012	.010	.943	.150	-.493	.910
.300	-.471	.911	.025	-.316	.521	.025	-.277	.923	.300	-.459	.912
.450	-.426	.913	.050	-.581	.506	.050	-.515	.909	.450	-.449	.913
.600	-.458	.912	.100	-.536	.508	.100	-.473	.910	.600	-.513	.909
.800	-.402	.916	.150	-.516	.509	.150	-.474	.911	.800	-.459	.912
.950	.044	.942	.200	-.505	.510	.200	-.500	.910			
			.300	-.493	.510	.300	-.494	.910			
			.350	-.494	.511	.350	-.473	.911			
			.400	-.474	.911	.400	-.471	.912			
			.450	-.492	.512	.450	-.494	.910			
			.500	-.513	.909	.500	-.517	.909			
			.550	-.512	.909	.550	-.531	.908			
			.600	-.491	.911	.600	-.543	.907			
			.650	-.514	.909	.700	-.516	.909			
			.700	-.487	.910	.800	-.337	.919			
			.800	-.378	.917	.900	-.124	.932			
			.900	-.125	.932	.950	-.114	.933			
			.950	.001	.939	.990	-.116	.933			
			.990	.086	.945						
					LOWER SURFACE						
.100	-.629	.902	.025	-.515	.909	.025	-.400	.916	.100	-.712	.897
.300	-.543	.907	.050	-.697	.898	.050	-.733	.895	.300	-.477	.911
.600	-.305	.921	.100	-.659	.900	.100	-.645	.901	.600	-.198	.928
.800	.196	.951	.200	-.574	.905	.200	-.539	.907	.800	.236	.946
			.300	-.552	.907	.300	-.513	.909			
			.400	-.467	.913	.400	-.474	.911			
			.500	-.479	.911	.500	-.360	.918			
			.600	-.233	.926	.600	-.174	.929			
			.700	.043	.942	.700	.119	.945			
			.800	.247	.954	.800	.304	.958			
			.900	.321	.959	.900	.296	.957			
			.950	.304	.957	.950	.295	.957			
			1.000	.108	.949						
CN=				.1559			.2063				
CM=				-.1086			-.1284				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = -1.92^o$; $C_L = 0.171$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.416	.891	0.000	1.014	.959	0.000	.061	.944	.050	-.716	.897
.150	-.631	.902	.012	-.193	.929	.012	-.244	.924	.150	-.556	.906
.300	-.545	.904	.025	-.541	.905	.025	-.501	.918	.300	-.503	.910
.450	-.660	.912	.050	-.777	.893	.050	-.714	.897	.450	-.472	.911
.600	-.477	.911	.100	-.655	.900	.100	-.606	.903	.600	-.525	.909
.800	-.405	.915	.150	-.624	.902	.150	-.568	.907	.800	-.454	.912
.950	.033	.941	.200	-.631	.904	.200	-.573	.905			
			.300	-.615	.904	.300	-.549	.907			
			.350	-.529	.908	.350	-.521	.909			
			.400	-.524	.909	.400	-.512	.907			
			.450	-.503	.910	.450	-.532	.908			
			.500	-.519	.907	.500	-.552	.907			
			.550	-.554	.907	.550	-.554	.907			
			.600	-.537	.909	.600	-.569	.906			
			.650	-.539	.907	.700	-.523	.908			
			.700	-.515	.909	.800	-.324	.920			
			.800	-.336	.916	.900	-.137	.931			
			.900	-.132	.932	.950	-.129	.932			
			.950	-.006	.939	.990	-.131	.932			
			.990	.075	.944						
					LOWER SURFACE						
.100	-.514	.903	.025	-.320	.920	.025	-.174	.928	.100	-.604	.906
.300	-.492	.910	.050	-.523	.908	.050	-.548	.907	.300	-.447	.913
.600	-.293	.922	.100	-.552	.907	.100	-.519	.909	.600	-.193	.928
.800	.223	.954	.200	-.504	.909	.200	-.470	.912	.900	.305	.957
			.300	-.491	.910	.300	-.448	.913			
			.400	-.495	.912	.400	-.438	.913			
			.500	-.446	.913	.500	-.336	.919			
			.600	-.220	.926	.600	-.155	.930			
			.700	.059	.943	.700	.130	.947			
			.800	.244	.954	.800	.332	.959			
			.900	.326	.959	.900	.317	.959			
			.950	.414	.958	.950	.305	.957			
			1.000	.059	.945						
CN=				.2454			.3058				
CM=				-.1065			-.1271				

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = -0.82^o$; $C_L = 0.269$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.394	.891	0.000	.932	.958	0.000	.067	.943	.050	-.989	.897
.150	-.626	.903	.012	-.431	.910	.012	-.515	.909	.150	-.630	.902
.300	-.597	.904	.025	-.329	.891	.025	-.731	.896	.300	-.555	.906
.450	-.631	.910	.050	-.535	.884	.050	-.990	.887	.450	-.500	.910
.600	-.500	.910	.100	-.736	.896	.100	-.733	.896	.600	-.532	.908
.800	-.411	.915	.150	-.653	.898	.150	-.629	.902	.800	-.444	.913
.950	.044	.942	.200	-.686	.899	.200	-.648	.901			
			.300	-.605	.903	.300	-.609	.903			
			.350	-.534	.905	.350	-.568	.905			
			.400	-.537	.904	.400	-.551	.907			
			.450	-.530	.904	.450	-.559	.906			
			.500	-.517	.905	.500	-.574	.905			
			.550	-.576	.905	.550	-.575	.905			
			.600	-.533	.907	.600	-.591	.905			
			.650	-.563	.906	.700	-.521	.908			
			.700	-.533	.908	.800	-.303	.921			
			.800	-.333	.916	.900	-.150	.930			
			.900	-.133	.931	.950	-.144	.931			
			.950	-.006	.939	.990	-.149	.931			
			.990	.070	.943						
					LOWER SURFACE						
.100	-.442	.917	.025	-.136	.931	.025	.006	.943	.100	-.491	.910
.300	-.437	.914	.050	-.340	.917	.050	-.402	.915	.300	-.404	.915
.600	-.273	.923	.100	-.422	.914	.100	-.424	.914	.600	-.174	.929
.800	.230	.954	.200	-.427	.914	.200	-.390	.916	.900	.323	.959
			.300	-.410	.914	.300	-.390	.916			
			.400	-.420	.914	.400	-.393	.916			
			.500	-.414	.915	.500	-.304	.921			
			.600	-.185	.928	.600	-.137	.931			
			.700	.071	.944	.700	.142	.943			
			.800	.268	.955	.800	.344	.960			
			.900	.336	.957	.900	.321	.954			
			.950	.212	.958	.950	.312	.954			
			1.000	.071	.945						
CN=				.3563			.3973				
CM=				-.1089			-.1245				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = 0.25^o$; $C_L = 0.362$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.180	.863	0.000	.963	.957	0.000	.066	.943	.050	-1.093	.874
.150	-.784	.893	.012	-.823	.850	.012	-.769	.894	.150	-.723	.896
.300	-.633	.902	.025	-1.093	.874	.025	-.966	.882	.300	-.605	.903
.450	-.518	.909	.050	-1.123	.873	.050	-1.082	.875	.450	-.529	.908
.600	-.513	.910	.100	-.921	.885	.100	-.850	.889	.600	-.548	.907
.800	-.404	.915	.150	-.800	.892	.150	-.724	.896	.800	-.437	.913
.950	.034	.942	.200	-.706	.896	.200	-.711	.897			
			.300	-.655	.900	.300	-.654	.900			
			.350	-.629	.902	.350	-.606	.903			
			.400	-.606	.903	.400	-.581	.905			
			.450	-.591	.906	.450	-.590	.904			
			.500	-.602	.904	.500	-.601	.904			
			.550	-.594	.904	.550	-.591	.904			
			.600	-.593	.906	.600	-.587	.904			
			.650	-.598	.906	.700	-.513	.909			
			.700	-.538	.907	.800	-.276	.923			
			.800	-.395	.917	.900	-.168	.929			
			.900	-.124	.932	.950	-.167	.929			
			.950	-.004	.939	.990	-.170	.929			
			.990	.066	.943						
					LOWER SURFACE						
.100	-.291	.922	.025	.092	.942	.025	.158	.949	.100	-.390	.916
.300	-.390	.916	.050	-.227	.926	.050	-.244	.925	.300	-.367	.918
.600	-.260	.924	.100	-.313	.921	.100	-.311	.921	.600	-.170	.929
.800	.238	.953	.200	-.333	.919	.200	-.331	.920	.800	.317	.958
			.300	-.373	.917	.300	-.357	.918			
			.400	-.373	.917	.400	-.362	.918			
			.500	-.401	.916	.500	-.289	.922			
			.600	-.174	.929	.600	-.130	.932			
			.700	.077	.944	.700	.150	.949			
			.800	.274	.956	.800	.340	.960			
			.900	.343	.960	.900	.316	.958			
			.950	.324	.959	.950	.309	.958			
			1.000	.074	.944						
CN=				.4375			.4738				
CM=				-.1049			-.1182				

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = 1.32^o$; $C_L = 0.452$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.370	.854	0.000	.887	.952	0.000	.074	.944	.050	-1.245	.866
.150	-.862	.884	.012	-1.074	.876	.012	-1.084	.875	.150	-.753	.895
.300	-.690	.894	.025	-1.330	.858	.025	-1.221	.867	.300	-.632	.902
.450	-.554	.903	.050	-1.338	.857	.050	-1.300	.862	.450	-.542	.907
.600	-.530	.904	.100	-1.041	.878	.100	-.960	.883	.600	-.547	.907
.800	-.401	.914	.150	-.859	.886	.150	-.807	.892	.300	-.415	.915
.950	.031	.941	.200	-.835	.890	.200	-.782	.893			
			.300	-.725	.896	.300	-.704	.898			
			.350	-.691	.899	.350	-.648	.901			
			.400	-.660	.901	.400	-.610	.903			
			.450	-.606	.904	.450	-.610	.903			
			.500	-.634	.902	.500	-.616	.903			
			.550	-.622	.903	.550	-.600	.904			
			.600	-.598	.906	.600	-.589	.905			
			.650	-.577	.905	.700	-.492	.910			
			.700	-.537	.908	.800	-.252	.924			
			.800	-.386	.916	.900	-.171	.929			
			.900	-.121	.932	.950	-.175	.929			
			.950	-.007	.939	.990	-.176	.929			
			.990	.051	.942						
					LOWER SURFACE						
.100	-.189	.924	.025	.135	.951	.025	.337	.959	.100	-.308	.921
.300	-.335	.920	.050	-.030	.935	.050	-.093	.934	.300	-.212	.921
.600	-.247	.925	.100	-.216	.927	.100	-.205	.927	.600	-.154	.930
.800	.242	.954	.200	-.276	.923	.200	-.264	.924	.800	.329	.959
			.300	-.333	.920	.300	-.300	.922			
			.400	-.342	.919	.400	-.324	.920			
			.500	-.371	.917	.500	-.251	.925			
			.600	-.158	.930	.600	-.110	.933			
			.700	.083	.944	.700	.161	.949			
			.800	.280	.956	.800	.354	.960			
			.900	.353	.960	.900	.323	.959			
			.950	.324	.959	.950	.318	.958			
			1.000	.059	.943						
CN=				.5251			.5600				
CM=				-.1027			-.1126				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = 2.41^o$; $C_L = 0.543$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.527	.849	0.000	.300	.987	0.000	.071	.944	.050	-1.528	.849
.150	-.974	.882	.012	-1.407	.856	.012	-1.447	.854	.150	-.841	.860
.300	-.722	.897	.025	-1.630	.843	.025	-1.492	.851	.300	-.689	.899
.450	-.573	.905	.050	-1.566	.847	.050	-1.505	.850	.450	-.578	.905
.600	-.537	.908	.100	-1.164	.870	.100	-1.099	.874	.600	-.561	.906
.800	-.383	.917	.150	-1.001	.880	.150	-.929	.884	.800	-.404	.915
.990	.031	.941	.200	-.839	.886	.200	-.878	.887			
			.300	-.778	.893	.300	-.756	.895			
			.350	-.715	.897	.350	-.702	.899			
			.400	-.676	.899	.400	-.650	.900			
			.450	-.629	.902	.450	-.651	.901			
			.500	-.649	.901	.500	-.648	.901			
			.550	-.633	.902	.550	-.625	.902			
			.600	-.586	.905	.600	-.607	.903			
			.650	-.582	.905	.700	-.496	.910			
			.700	-.547	.907	.800	-.246	.925			
			.800	-.383	.917	.900	-.185	.928			
			.900	-.111	.933	.950	-.188	.928			
			.950	.002	.940	.990	-.193	.928			
			.990	.049	.942						
					LOWER SURFACE						
.100	-.079	.935	.025	.343	.960	.025	.474	.967	.100	-.201	.928
.300	-.289	.922	.050	.057	.943	.050	.017	.940	.300	-.238	.922
.600	-.223	.926	.100	-.098	.934	.100	-.108	.933	.600	-.150	.931
.800	.257	.955	.200	-.194	.928	.200	-.201	.927	.800	.320	.958
			.300	-.230	.923	.300	-.255	.924			
			.400	-.296	.922	.400	-.282	.924			
			.500	-.326	.920	.500	-.241	.925			
			.600	-.142	.931	.600	-.096	.934			
			.700	.103	.945	.700	.166	.949			
			.800	.239	.957	.800	.356	.961			
			.900	.356	.961	.900	.324	.959			
			.950	.337	.959	.950	.322	.958			
			1.000	.065	.943						
CN=				.6147			.6523				
CM=				-.0996			-.1091				

(a) M = 0.30. Continued.

$\delta_a = 6^o$; $\alpha = 3.47^o$; $C_L = 0.632$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.742	.836	0.000	.675	.980	0.000	.072	.944	.050	-1.721	.838
.150	-1.056	.877	.012	-1.732	.837	.012	-1.781	.834	.150	-.948	.883
.300	-.768	.894	.025	-2.033	.819	.025	-1.771	.835	.300	-.718	.897
.450	-.606	.904	.050	-1.808	.832	.050	-1.727	.837	.450	-.583	.905
.600	-.555	.907	.100	-1.246	.865	.100	-1.246	.866	.600	-.562	.906
.800	-.337	.917	.150	-1.101	.874	.150	-.999	.880	.800	-.391	.917
.990	.027	.941	.200	-.933	.881	.200	-.931	.884			
			.300	-.822	.891	.300	-.802	.892			
			.350	-.766	.894	.350	-.732	.896			
			.400	-.720	.897	.400	-.683	.899			
			.450	-.670	.900	.450	-.675	.900			
			.500	-.656	.899	.500	-.664	.900			
			.550	-.657	.901	.550	-.633	.902			
			.600	-.611	.903	.600	-.611	.903			
			.650	-.594	.904	.700	-.483	.911			
			.700	-.551	.907	.800	-.250	.925			
			.800	-.359	.919	.900	-.192	.928			
			.900	-.114	.933	.950	-.195	.928			
			.950	-.016	.939	.990	-.206	.927			
			.990	.032	.941						
					LOWER SURFACE						
.100	.022	.941	.025	.456	.967	.025	.585	.974	.100	-.115	.933
.300	-.257	.924	.050	.121	.951	.050	.167	.949	.300	-.251	.925
.600	-.207	.927	.100	-.019	.938	.100	-.009	.934	.600	-.154	.930
.800	.263	.955	.200	-.146	.931	.200	-.153	.930	.800	.322	.959
			.300	-.220	.926	.300	-.211	.927			
			.400	-.268	.924	.400	-.222	.926			
			.500	-.303	.922	.500	-.224	.926			
			.600	-.130	.932	.600	-.085	.934			
			.700	.108	.945	.700	.175	.950			
			.800	.293	.957	.800	.364	.961			
			.900	.357	.961	.900	.333	.959			
			.950	.330	.959	.950	.329	.959			
			1.000	.043	.942						
CN=				.6990			.7344				
CM=				-.0963			-.1049				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(a) M = 0.30. Concluded.

$\delta_a = 6^o$; $\alpha = 4.55^o$; $C_L = 0.726$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.006	.820	0.000	.518	.570	0.000	.375	.944	.050	-1.964	.823
.150	-1.152	.871	.012	-2.151	.812	.012	-2.124	.813	.150	-1.045	.877
.300	-.421	.491	.025	-2.330	.754	.025	-2.120	.814	.300	-.774	.893
.450	-.627	.902	.050	-2.047	.818	.050	-2.015	.820	.450	-.611	.903
.600	-.570	.906	.100	-1.424	.855	.100	-1.362	.859	.600	-.569	.906
.800	-.377	.917	.150	-1.200	.868	.150	-1.111	.873	.800	-.398	.916
.950	.024	.941	.200	-1.057	.877	.200	-1.006	.880			
			.300	-.876	.887	.300	-.851	.889			
			.350	-.805	.892	.350	-.776	.893			
			.400	-.763	.894	.400	-.723	.896			
			.450	-.697	.898	.450	-.711	.897			
			.500	-.706	.897	.500	-.691	.898			
			.550	-.675	.899	.550	-.648	.901			
			.600	-.627	.902	.600	-.615	.903			
			.650	-.606	.903	.700	-.474	.911			
			.700	-.558	.906	.800	-.234	.925			
			.800	-.368	.918	.900	-.199	.928			
			.900	-.113	.933	.950	-.197	.928			
			.950	-.015	.938	.990	-.203	.927			
			.990	.012	.940						
					LOWER SURFACE						
.100	.084	.944	.025	.587	.574	.025	.707	.981	.100	-.034	.937
.300	-.193	.928	.050	.332	.659	.050	.290	.957	.300	-.211	.927
.600	-.194	.928	.100	.116	.646	.100	.081	.944	.600	-.126	.932
.800	.267	.955	.200	-.068	.935	.200	-.076	.935	.800	.320	.958
			.300	-.171	.929	.300	-.157	.930			
			.400	-.221	.926	.400	-.194	.928			
			.500	-.277	.923	.500	-.197	.928			
			.600	-.111	.933	.600	-.074	.935			
			.700	.119	.946	.700	.185	.950			
			.800	.300	.957	.800	.367	.961			
			.900	.367	.961	.900	.336	.959			
			.950	.329	.959	.950	.329	.959			
			1.000	.025	.941						
CN=				.7984			.8220				
CM=				-.0914			-.0978				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50

$\delta_a = 0^o$; $\alpha = -4.16^o$; $C_L = -0.092$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.392	.785	0.000	1.024	.994	0.000	.065	.852	.050	-.319	.795
.150	-.467	.774	.012	.339	.893	.012	.299	.887	.150	-.402	.783
.300	-.494	.775	.025	-.066	.833	.025	.016	.845	.300	-.412	.782
.450	-.433	.779	.050	-.310	.797	.050	-.290	.800	.450	-.412	.782
.600	-.464	.774	.100	-.388	.785	.100	-.347	.791	.600	-.464	.774
.800	-.406	.783	.150	-.421	.780	.150	-.359	.790	.800	-.336	.793
.950	.060	.851	.200	-.448	.776	.200	-.412	.782			
			.300	-.457	.775	.300	-.454	.775			
			.350	-.455	.775	.350	-.427	.779			
			.400	-.460	.775	.400	-.419	.781			
			.450	-.453	.776	.450	-.462	.774			
			.500	-.499	.769	.500	-.497	.769			
			.550	-.514	.767	.550	-.509	.767			
			.600	-.494	.769	.600	-.506	.768			
			.650	-.530	.764	.700	-.455	.775			
			.700	-.504	.768	.800	-.331	.794			
			.800	-.379	.787	.900	-.070	.832			
			.900	-.108	.827	.950	.020	.846			
			.950	.020	.846	.990	.052	.850			
			.990	.107	.858						
					LOWER SURFACE						
.100	-.892	.711	.025	-.802	.724	.025	-.802	.724	.100	-1.084	.682
.300	-.660	.745	.050	-1.095	.681	.050	-1.179	.668	.300	-.635	.749
.600	-.338	.793	.100	-.977	.698	.100	-.968	.699	.600	-.308	.797
.800	.143	.864	.200	-.780	.727	.200	-.756	.731	.800	.161	.866
			.300	-.721	.736	.300	-.688	.741			
			.400	-.634	.749	.400	-.642	.748			
			.500	-.585	.756	.500	-.514	.767			
			.600	-.289	.800	.600	-.302	.798			
			.700	.031	.847	.700	-.009	.841			
			.800	.193	.871	.800	.215	.874			
			.900	.279	.884	.900	.266	.882			
			.950	.291	.886	.950	.289	.885			
			1.000	.126	.861						
CN=				-.0150			-.0357				
CM=				-.1072			-.1048				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = -2.91^o$; $C_L = 0.037$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.632	.749	0.000	1.050	.998	0.000	.061	.852	.050	-.474	.772
.150	-.551	.761	.012	.126	.861	.012	.034	.848	.150	-.476	.772
.300	-.516	.766	.025	-.301	.798	.025	-.198	.813	.300	-.468	.773
.450	-.469	.773	.050	-.557	.760	.050	-.493	.770	.450	-.441	.777
.600	-.488	.770	.100	-.524	.765	.100	-.508	.767	.600	-.478	.772
.800	-.409	.782	.150	-.571	.758	.150	-.463	.774	.800	-.353	.790
.960	.055	.851	.200	-.541	.763	.200	-.500	.769			
			.300	-.543	.762	.300	-.521	.766			
			.350	-.523	.765	.350	-.494	.769			
			.400	-.523	.766	.400	-.489	.770			
			.450	-.501	.768	.450	-.515	.766			
			.500	-.546	.762	.500	-.546	.762			
			.550	-.557	.760	.550	-.547	.762			
			.600	-.533	.764	.600	-.532	.764			
			.650	-.546	.762	.700	-.469	.773			
			.700	-.524	.765	.800	-.339	.792			
			.800	-.387	.785	.900	-.075	.831			
			.900	-.108	.827	.950	.002	.843			
			.950	.021	.846	.990	.039	.848			
			.990	.097	.857						
					LOWER SURFACE						
.100	-.742	.733	.025	-.544	.762	.025	-.503	.768	.100	-.883	.712
.300	-.605	.753	.050	-.834	.719	.050	-.913	.708	.300	-.568	.759
.600	-.327	.794	.100	-.773	.728	.100	-.811	.723	.600	-.310	.797
.800	.177	.869	.200	-.636	.741	.200	-.661	.745	.800	.198	.872
			.300	-.658	.745	.300	-.628	.750			
			.400	-.585	.756	.400	-.583	.756			
			.500	-.557	.760	.500	-.482	.771			
			.600	-.264	.803	.600	-.284	.800			
			.700	.048	.850	.700	.010	.844			
			.800	.218	.875	.800	.257	.881			
			.900	.307	.888	.900	.294	.886			
			.950	.316	.889	.950	.317	.890			
			1.000	.114	.859						
CN=				.1138			.0953				
CM=				-.1087			-.1068				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = -2.30^o$; $C_L = 0.101$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.758	.730	0.000	1.046	.997	0.000	.067	.852	.050	-.648	.747
.150	-.642	.747	.012	-.033	.838	.012	-.063	.833	.150	-.554	.760
.300	-.536	.763	.025	-.482	.771	.025	-.310	.797	.300	-.503	.768
.450	-.497	.769	.050	-.689	.741	.050	-.616	.751	.450	-.457	.775
.600	-.494	.769	.100	-.613	.752	.100	-.579	.757	.600	-.496	.769
.800	-.417	.781	.150	-.620	.751	.150	-.534	.763	.800	-.366	.788
.950	.052	.850	.200	-.623	.750	.200	-.573	.758			
			.300	-.562	.759	.300	-.551	.761			
			.350	-.549	.761	.350	-.509	.767			
			.400	-.540	.763	.400	-.518	.766			
			.450	-.530	.764	.450	-.535	.763			
			.500	-.563	.759	.500	-.556	.760			
			.550	-.570	.758	.550	-.560	.760			
			.600	-.540	.763	.600	-.552	.761			
			.650	-.559	.760	.700	-.477	.772			
			.700	-.539	.763	.800	-.340	.792			
			.800	-.386	.785	.900	-.074	.832			
			.900	-.111	.826	.950	-.009	.841			
			.950	.013	.844	.990	.029	.847			
			.990	.055	.857						
					LOWER SURFACE						
.100	-.658	.745	.025	-.419	.780	.025	-.395	.784	.100	-.817	.722
.300	-.571	.759	.050	-.729	.735	.050	-.802	.724	.300	-.551	.761
.600	-.315	.796	.100	-.711	.737	.100	-.696	.739	.600	-.303	.798
.800	.199	.872	.200	-.625	.750	.200	-.619	.751	.800	.214	.874
			.300	-.620	.751	.300	-.598	.754			
			.400	-.559	.760	.400	-.565	.759			
			.500	-.541	.762	.500	-.465	.774			
			.600	-.259	.804	.600	-.279	.801			
			.700	.051	.850	.700	.015	.845			
			.800	.239	.878	.800	.260	.881			
			.900	.327	.891	.900	.299	.887			
			.950	.312	.889	.950	.322	.890			
			1.000	.101	.857						
CN=				.1747			.1559				
CM=				-.1088			-.1049				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = -1.71^o$; $C_L = 0.160$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.848	.717	0.000	1.044	.997	0.000	.074	.853	.050	-.752	.731
.150	-.686	.741	.012	-.133	.822	.012	-.199	.813	.150	-.570	.758
.300	-.583	.756	.025	-.640	.748	.025	-.472	.773	.300	-.536	.763
.450	-.514	.767	.050	-.788	.726	.050	-.738	.733	.450	-.474	.772
.600	-.514	.767	.100	-.709	.738	.100	-.661	.745	.600	-.499	.769
.800	-.408	.782	.150	-.659	.745	.150	-.581	.757	.800	-.357	.790
.950	.037	.848	.200	-.661	.745	.200	-.615	.752			
			.300	-.599	.754	.300	-.577	.757			
			.350	-.573	.758	.350	-.537	.763			
			.400	-.568	.759	.400	-.531	.764			
			.450	-.557	.760	.450	-.546	.762			
			.500	-.589	.755	.500	-.574	.758			
			.550	-.585	.756	.550	-.582	.756			
			.600	-.560	.760	.600	-.556	.760			
			.650	-.576	.757	.700	-.480	.772			
			.700	-.554	.761	.800	-.333	.793			
			.800	-.390	.785	.900	-.074	.832			
			.900	-.115	.826	.950	-.008	.841			
			.950	.010	.844	.990	.023	.846			
			.990	.092	.856						
					LOWER SURFACE						
.100	-.608	.753	.025	-.323	.795	.025	-.236	.808	.100	-.726	.735
.300	-.540	.763	.050	-.622	.751	.050	-.693	.740	.300	-.527	.765
.600	-.308	.797	.100	-.629	.750	.100	-.619	.751	.600	-.302	.798
.800	.201	.872	.200	-.587	.756	.200	-.566	.759	.800	.223	.875
			.300	-.585	.756	.300	-.552	.761			
			.400	-.539	.763	.400	-.540	.763			
			.500	-.529	.764	.500	-.453	.776			
			.600	-.248	.806	.600	-.276	.802			
			.700	.060	.851	.700	.025	.846			
			.800	.250	.880	.800	.268	.882			
			.900	.330	.891	.900	.308	.888			
			.950	.325	.891	.950	.334	.892			
			1.000	.103	.858						
CN=				.2327			.2155				
CM=				-.1099			-.1023				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = -1.10^o$; $C_L = 0.216$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.963	.700	0.000	1.058	.999	0.000	.070	.853	.050	-.901	.709
.150	-.718	.734	.012	-.272	.807	.012	-.350	.791	.150	-.649	.746
.300	-.608	.752	.025	-.686	.741	.025	-.560	.760	.300	-.566	.759
.450	-.534	.763	.050	-.904	.709	.050	-.867	.714	.450	-.500	.769
.600	-.525	.765	.100	-.759	.730	.100	-.740	.733	.600	-.503	.768
.800	-.416	.781	.150	-.729	.735	.150	-.641	.748	.900	-.359	.789
.950	.049	.850	.200	-.705	.738	.200	-.654	.746			
			.300	-.645	.747	.300	-.615	.751			
			.350	-.615	.751	.350	-.566	.759			
			.400	-.595	.754	.400	-.564	.759			
			.450	-.580	.757	.450	-.577	.757			
			.500	-.597	.754	.500	-.595	.754			
			.550	-.602	.753	.550	-.589	.755			
			.600	-.571	.758	.600	-.564	.759			
			.650	-.580	.757	.700	-.487	.770			
			.700	-.547	.762	.900	-.344	.792			
			.800	-.390	.785	.900	-.081	.830			
			.900	-.114	.826	.950	-.020	.840			
			.950	.012	.844	.990	.003	.843			
			.990	.040	.854						
					LOWER SURFACE						
.100	-.502	.768	.025	-.232	.808	.025	-.105	.827	.100	-.703	.738
.300	-.509	.767	.050	-.510	.767	.050	-.594	.755	.300	-.505	.768
.600	-.311	.796	.100	-.558	.760	.100	-.545	.762	.600	-.299	.798
.800	.219	.875	.200	-.548	.761	.200	-.521	.765	.800	.235	.877
			.300	-.545	.762	.300	-.539	.763			
			.400	-.515	.766	.400	-.521	.765			
			.500	-.503	.768	.500	-.438	.778			
			.600	-.239	.807	.600	-.256	.805			
			.700	.066	.952	.700	.026	.846			
			.800	.256	.880	.800	.268	.882			
			.900	.342	.893	.900	.310	.888			
			.950	.323	.891	.950	.331	.851			
			1.000	.095	.857						
CN=				.2856			.2728				
CM=				-.1095			-.1011				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = -0.48^o$; $C_L = 0.274$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.073	.684	0.000	1.044	.997	0.000	.074	.853	.050	-.992	.696
.150	-.780	.727	.012	-.439	.770	.012	-.462	.774	.150	-.711	.737
.300	-.635	.748	.025	-.881	.712	.025	-.695	.740	.300	-.590	.755
.450	-.546	.762	.050	-1.066	.685	.050	-.979	.698	.450	-.505	.768
.600	-.537	.763	.100	-.871	.714	.100	-.826	.720	.600	-.512	.767
.800	-.406	.782	.150	-.766	.729	.150	-.684	.741	.900	-.357	.790
.950	.042	.843	.200	-.741	.733	.200	-.700	.739			
			.300	-.666	.744	.300	-.648	.747			
			.350	-.653	.746	.350	-.589	.755			
			.400	-.624	.750	.400	-.576	.757			
			.450	-.603	.753	.450	-.583	.756			
			.500	-.634	.749	.500	-.593	.755			
			.550	-.611	.752	.550	-.598	.754			
			.600	-.591	.755	.600	-.578	.757			
			.650	-.535	.756	.700	-.484	.771			
			.700	-.557	.760	.800	-.325	.794			
			.800	-.339	.785	.900	-.079	.831			
			.900	-.171	.828	.950	-.023	.839			
			.950	.012	.844	.990	.001	.843			
			.990	.074	.853						
					LOWER SURFACE						
.100	-.425	.730	.025	-.115	.825	.025	.027	.846	.100	-.592	.755
.300	-.488	.770	.050	-.391	.785	.050	-.438	.778	.300	-.487	.770
.600	-.295	.799	.100	-.481	.771	.100	-.487	.770	.600	-.242	.801
.800	.225	.876	.200	-.491	.770	.200	-.474	.772	.800	.238	.878
			.300	-.514	.766	.300	-.494	.769			
			.400	-.496	.769	.400	-.492	.770			
			.500	-.488	.770	.500	-.411	.782			
			.600	-.230	.808	.600	-.250	.805			
			.700	.065	.852	.700	.034	.849			
			.800	.264	.882	.800	.278	.884			
			.900	.343	.893	.900	.321	.890			
			.950	.326	.891	.950	.335	.892			
			1.000	.085	.855						
CN=				.3441			.3282				
CM=				-.1063			-.0976				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 0.08^o$; $C_L = 0.327$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.213	.663	0.000	1.031	.595	0.000	.073	.853	.050	-1.114	.678
.150	-.784	.727	.012	-.551	.761	.012	-.559	.760	.150	-.745	.732
.300	-.679	.742	.025	-.994	.695	.025	-.877	.713	.300	-.614	.752
.450	-.554	.761	.050	-1.152	.672	.050	-1.052	.687	.450	-.522	.765
.600	-.539	.763	.100	-.933	.704	.100	-.876	.713	.600	-.531	.764
.800	-.410	.782	.150	-.831	.719	.150	-.732	.734	.800	-.363	.789
.950	.046	.849	.200	-.796	.725	.200	-.731	.734			
			.300	-.731	.734	.300	-.692	.740			
			.350	-.661	.745	.350	-.632	.749			
			.400	-.634	.749	.400	-.596	.754			
			.450	-.620	.751	.450	-.609	.752			
			.500	-.639	.748	.500	-.621	.751			
			.550	-.626	.750	.550	-.609	.752			
			.600	-.608	.753	.600	-.580	.757			
			.650	-.597	.754	.700	-.489	.770			
			.700	-.554	.761	.800	-.317	.796			
			.800	-.341	.786	.900	-.089	.829			
			.900	-.104	.827	.950	-.036	.837			
			.950	.013	.844	.990	-.041	.836			
			.990	.057	.852						
					LOWER SURFACE						
.100	-.359	.781	.025	-.008	.841	.025	.055	.851	.100	-.551	.761
.300	-.441	.774	.050	-.323	.795	.050	-.405	.783	.300	-.481	.771
.600	-.293	.793	.100	-.418	.781	.100	-.430	.779	.600	-.285	.800
.900	.238	.874	.200	-.449	.776	.200	-.441	.777	.800	.235	.877
			.300	-.488	.770	.300	-.479	.772			
			.400	-.467	.773	.400	-.486	.771			
			.500	-.471	.773	.500	-.415	.781			
			.600	-.225	.809	.600	-.240	.807			
			.700	.057	.852	.700	.035	.848			
			.800	.266	.882	.800	.273	.883			
			.900	.341	.893	.900	.317	.889			
			.950	.328	.891	.950	.331	.892			
			1.000	.066	.852						
CN=				.3906			.3673				
CM=				-.1046			-.0967				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 0.70$; $C_L = 0.379$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.338	.645	0.000	1.004	.591	0.000	.077	.854	.050	-1.262	.656
.150	-.869	.714	.012	-.725	.735	.012	-.767	.729	.150	-.758	.730
.300	-.691	.740	.025	-1.216	.662	.025	-.963	.700	.300	-.646	.747
.450	-.571	.758	.050	-1.296	.651	.050	-1.213	.663	.450	-.533	.764
.600	-.547	.761	.100	-1.035	.689	.100	-.938	.704	.600	-.523	.765
.800	-.397	.784	.150	-.890	.711	.150	-.817	.722	.800	-.348	.791
.950	.043	.849	.200	-.859	.715	.200	-.779	.727			
			.300	-.748	.732	.300	-.718	.736			
			.350	-.695	.740	.350	-.650	.746			
			.400	-.671	.743	.400	-.631	.749			
			.450	-.644	.747	.450	-.621	.751			
			.500	-.653	.746	.500	-.640	.749			
			.550	-.642	.748	.550	-.623	.750			
			.600	-.605	.753	.600	-.586	.756			
			.650	-.596	.754	.700	-.480	.771			
			.700	-.560	.760	.800	-.308	.797			
			.800	-.336	.785	.900	-.084	.830			
			.900	-.089	.829	.950	-.052	.835			
			.950	.010	.844	.990	-.037	.837			
			.990	.059	.851						
					LOWER SURFACE						
.100	-.309	.797	.025	.075	.854	.025	.182	.869	.100	-.464	.774
.300	-.433	.774	.050	-.235	.808	.050	-.253	.805	.300	-.451	.776
.600	-.290	.800	.100	-.343	.792	.100	-.349	.791	.600	-.279	.801
.800	.243	.878	.200	-.384	.786	.200	-.399	.783	.800	.241	.878
			.300	-.443	.777	.300	-.435	.778			
			.400	-.435	.778	.400	-.461	.774			
			.500	-.461	.774	.500	-.382	.786			
			.600	-.215	.811	.600	-.239	.807			
			.700	.075	.854	.700	.042	.849			
			.800	.274	.883	.800	.281	.884			
			.900	.345	.893	.900	.322	.890			
			.950	.333	.892	.950	.329	.891			
			1.000	.063	.852						
CN=				.4542			.4279				
CM=				-.1023			-.0923				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 1.88^o$; $C_L = 0.488$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.590	.607	0.000	.950	.583	0.000	.075	.854	.050	-1.576	.610
.150	-.956	.701	.012	-1.151	.672	.012	-1.144	.673	.150	-.868	.714
.300	-.754	.731	.025	-1.546	.614	.025	-1.365	.641	.300	-.685	.741
.450	-.605	.753	.050	-1.627	.602	.050	-1.507	.620	.450	-.561	.760
.600	-.558	.760	.100	-1.195	.666	.100	-1.115	.678	.600	-.528	.764
.800	-.381	.786	.150	-1.015	.692	.150	-.878	.713	.800	-.341	.792
.950	.035	.848	.200	-.925	.706	.200	-.864	.715			
			.300	-.806	.723	.300	-.778	.727			
			.350	-.743	.733	.350	-.699	.739			
			.400	-.711	.737	.400	-.677	.742			
			.450	-.677	.742	.450	-.658	.745			
			.500	-.675	.743	.500	-.662	.745			
			.550	-.651	.746	.550	-.637	.748			
			.600	-.623	.750	.600	-.600	.754			
			.650	-.604	.753	.700	-.476	.772			
			.700	-.560	.760	.800	-.295	.799			
			.800	-.376	.787	.900	-.096	.828			
			.900	-.082	.830	.950	-.065	.833			
			.950	.010	.844	.990	-.069	.832			
			.990	.050	.850						
					LOWER SURFACE						
.100	-.197	.814	.025	.229	.876	.025	.360	.896	.100	-.358	.790
.300	-.370	.788	.050	-.070	.832	.050	-.112	.826	.300	-.407	.782
.600	-.263	.804	.100	-.214	.811	.100	-.240	.807	.600	-.269	.803
.800	.254	.880	.200	-.312	.796	.200	-.310	.797	.800	.248	.879
			.300	-.381	.786	.300	-.382	.786			
			.400	-.385	.786	.400	-.409	.782			
			.500	-.416	.781	.500	-.359	.789			
			.600	-.193	.814	.600	-.223	.810			
			.700	.087	.855	.700	.047	.849			
			.800	.290	.886	.800	.288	.885			
			.900	.366	.897	.900	.324	.891			
			.950	.335	.892	.950	.332	.892			
			1.000	.053	.850						
CN=				.5605			.5319				
CM=				-.0978			-.0866				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 3.09^o$; $C_L = 0.596$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.847	.569	0.000	.846	.568	0.000	.075	.854	.050	-1.865	.567
.150	-1.079	.683	.012	-1.497	.621	.012	-1.493	.622	.150	-.961	.700
.300	-.798	.724	.025	-1.913	.560	.025	-1.607	.605	.300	-.733	.734
.450	-.633	.749	.050	-1.945	.555	.050	-1.786	.578	.450	-.586	.756
.600	-.575	.757	.100	-1.351	.643	.100	-1.283	.653	.600	-.538	.763
.800	-.379	.786	.150	-1.129	.675	.150	-1.049	.687	.800	-.336	.793
.950	.020	.845	.200	-1.023	.690	.200	-.965	.700			
			.300	-.878	.713	.300	-.844	.718			
			.350	-.790	.726	.350	-.755	.731			
			.400	-.746	.732	.400	-.703	.738			
			.450	-.719	.736	.450	-.693	.740			
			.500	-.710	.737	.500	-.681	.742			
			.550	-.678	.742	.550	-.657	.745			
			.600	-.655	.746	.600	-.617	.751			
			.650	-.620	.751	.700	-.471	.773			
			.700	-.556	.760	.800	-.280	.801			
			.800	-.361	.789	.900	-.104	.827			
			.900	-.082	.830	.950	-.092	.829			
			.950	-.015	.840	.990	-.093	.829			
			.990	.020	.846						
					LOWER SURFACE						
.100	-.071	.832	.025	.378	.898	.025	.481	.914	.100	-.224	.809
.300	-.321	.795	.050	.038	.848	.050	.027	.846	.300	-.350	.791
.600	-.244	.806	.100	-.088	.829	.100	-.131	.823	.600	-.265	.803
.800	.261	.881	.200	-.226	.805	.200	-.236	.808	.800	.246	.879
			.300	-.321	.795	.300	-.323	.795			
			.400	-.342	.792	.400	-.377	.787			
			.500	-.382	.786	.500	-.337	.793			
			.600	-.171	.817	.600	-.196	.814			
			.700	.090	.856	.700	.052	.850			
			.800	.287	.885	.800	.294	.886			
			.900	.372	.898	.900	.310	.888			
			.950	.334	.892	.950	.331	.891			
			1.000	.027	.846						
CN=				.6672			.6329				
CM=				-.0929			-.0815				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 4.28^o$; $C_L = 0.703$

STATION .1542			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.183	.520	0.000	.722	.949	0.000	.087	.855	.050	-2.216	.515
.150	-1.147	.667	.012	-1.939	.556	.012	-1.831	.572	.150	-1.072	.684
.300	-.855	.716	.025	-2.406	.487	.025	-2.037	.541	.300	-.766	.729
.450	-.659	.745	.050	-2.278	.505	.050	-2.165	.522	.450	-.595	.754
.600	-.583	.756	.100	-1.434	.627	.100	-1.415	.633	.600	-.531	.764
.800	-.357	.790	.150	-1.264	.656	.150	-1.134	.675	.800	-.327	.794
.950	.009	.844	.200	-1.127	.676	.200	-1.055	.686			
			.300	-.918	.707	.300	-.988	.711			
			.350	-.832	.719	.350	-.794	.725			
			.400	-.800	.724	.400	-.746	.732			
			.450	-.756	.731	.450	-.718	.736			
			.500	-.740	.733	.500	-.707	.738			
			.550	-.697	.739	.550	-.673	.743			
			.600	-.651	.746	.600	-.613	.752			
			.650	-.621	.751	.700	-.462	.774			
			.700	-.559	.760	.800	-.255	.805			
			.800	-.347	.791	.900	-.112	.826			
			.900	-.085	.830	.950	-.105	.827			
			.950	-.015	.840	.990	-.111	.826			
			.990	-.002	.847						
					LOWER SURFACE						
.100	.028	.847	.025	.510	.918	.025	.624	.935	.100	-.133	.823
.300	-.272	.802	.050	.226	.876	.050	.198	.872	.300	-.283	.801
.600	-.228	.809	.100	.027	.847	.100	.011	.844	.600	-.243	.807
.800	.279	.884	.200	-.158	.819	.200	-.166	.818	.800	.240	.878
			.300	-.250	.806	.300	-.247	.806			
			.400	-.296	.799	.400	-.325	.794			
			.500	-.358	.790	.500	-.396	.799			
			.600	-.158	.819	.600	-.192	.814			
			.700	.107	.858	.700	.066	.852			
			.800	.308	.888	.800	.288	.885			
			.900	.377	.898	.900	.331	.892			
			.950	.334	.892	.950	.327	.891			
			1.000	.011	.844						
CN=				.7748			.7348				
CM=				-.0875			-.0721				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 5.43^o$; $C_L = 0.799$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.748	.436	0.000	.591	.930	0.000	.078	.854	.050	-2.628	.454
.150	-1.282	.653	.012	-2.180	.520	.012	-2.344	.496	.150	-1.147	.673
.300	-.893	.710	.025	-2.852	.421	.025	-2.309	.501	.300	-.806	.723
.450	-.673	.743	.050	-2.807	.427	.050	-2.488	.474	.450	-.617	.751
.600	-.583	.756	.100	-1.619	.603	.100	-1.536	.615	.600	-.525	.765
.800	-.339	.792	.150	-1.359	.641	.150	-1.243	.659	.800	-.328	.794
.950	-.011	.841	.200	-1.201	.665	.200	-1.123	.676			
			.300	-.962	.700	.300	-.938	.704			
			.350	-.870	.714	.350	-.826	.720			
			.400	-.810	.723	.400	-.776	.728			
			.450	-.778	.727	.450	-.742	.733			
			.500	-.735	.734	.500	-.721	.736			
			.550	-.695	.740	.550	-.673	.743			
			.600	-.649	.747	.600	-.609	.752			
			.650	-.615	.752	.700	-.441	.777			
			.700	-.534	.763	.800	-.261	.804			
			.800	-.303	.798	.900	-.131	.823			
			.900	-.084	.830	.950	-.129	.823			
			.950	-.052	.835	.990	-.127	.824			
			.990	-.032	.838						
					LOWER SURFACE						
.100	.137	.863	.025	.627	.935	.025	.744	.953	.100	-.005	.842
.300	-.218	.810	.050	.355	.895	.050	.277	.884	.300	-.252	.805
.600	-.217	.810	.100	.118	.860	.100	.084	.855	.600	-.232	.808
.800	.271	.883	.200	-.086	.830	.200	-.080	.831	.800	.249	.879
			.300	-.199	.814	.300	-.203	.812			
			.400	-.254	.805	.400	-.289	.800			
			.500	-.320	.795	.500	-.276	.802			
			.600	-.136	.822	.600	-.173	.817			
			.700	.114	.859	.700	.073	.853			
			.800	.315	.889	.800	.290	.885			
			.900	.383	.899	.900	.329	.891			
			.950	.332	.892	.950	.325	.891			
			1.000	-.020	.840						
CN=				.8630			.8725				
CM=				-.0786			-.0662				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 6.57^o$; $C_L = 0.887$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.172	.373	0.000	.498	.916	0.000	.085	.855	.050	-2.949	.406
.150	-1.333	.645	.012	-2.503	.472	.012	-2.667	.448	.150	-1.205	.664
.300	-.925	.706	.025	-3.150	.376	.025	-3.061	.390	.300	-.832	.719
.450	-.683	.741	.050	-3.135	.371	.050	-2.966	.404	.450	-.616	.751
.600	-.572	.758	.100	-1.661	.597	.100	-1.679	.594	.600	-.523	.765
.800	-.305	.797	.150	-1.411	.634	.150	-1.323	.647	.800	-.339	.792
.950	-.022	.839	.200	-1.256	.657	.200	-1.182	.668			
			.300	-.958	.695	.300	-.972	.699			
			.350	-.895	.710	.350	-.866	.714			
			.400	-.841	.718	.400	-.802	.724			
			.450	-.792	.725	.450	-.757	.730			
			.500	-.748	.732	.500	-.722	.736			
			.550	-.700	.739	.550	-.674	.743			
			.600	-.645	.747	.600	-.604	.753			
			.650	-.586	.756	.700	-.418	.781			
			.700	-.507	.768	.800	-.235	.808			
			.800	-.279	.801	.900	-.137	.822			
			.900	-.089	.829	.950	-.133	.823			
			.950	-.051	.835	.990	-.145	.821			
			.990	-.053	.835						
					LOWER SURFACE						
.100	.222	.875	.025	.725	.950	.025	.841	.967	.100	.068	.853
.300	-.161	.819	.050	.445	.908	.050	.412	.903	.300	-.227	.809
.600	-.203	.812	.100	.208	.873	.100	.180	.869	.600	-.226	.809
.800	.276	.883	.200	-.006	.842	.200	-.040	.837	.800	.242	.878
			.300	-.150	.820	.300	-.161	.819			
			.400	-.226	.809	.400	-.252	.805			
			.500	-.293	.799	.500	-.248	.806			
			.600	-.121	.825	.600	-.158	.819			
			.700	.115	.860	.700	.070	.853			
			.800	.310	.888	.800	.299	.887			
			.900	.378	.898	.900	.329	.891			
			.950	.334	.892	.950	.320	.890			
			1.000	-.033	.838						
CN=				.9325			.9111				
CM=				-.0699			-.0543				

(b) M = 0.50. Continued.

$\delta_a = 0^o$; $\alpha = 7.77^o$; $C_L = 0.983$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.369	.344	0.000	.316	.889	0.000	.082	.855	.050	-3.019	.396
.150	-1.443	.629	.012	-2.725	.439	.012	-2.974	.403	.150	-1.293	.651
.300	-.954	.701	.025	-3.437	.334	.025	-3.355	.346	.300	-.862	.715
.450	-.685	.741	.050	-3.341	.348	.050	-3.276	.358	.450	-.637	.748
.600	-.560	.760	.100	-2.284	.505	.100	-1.878	.565	.600	-.507	.768
.800	-.308	.797	.150	-1.623	.602	.150	-1.435	.630	.800	-.336	.793
.950	-.017	.840	.200	-1.301	.650	.200	-1.254	.657			
			.300	-1.024	.691	.300	-1.008	.693			
			.350	-.925	.706	.350	-.887	.711			
			.400	-.852	.717	.400	-.811	.723			
			.450	-.793	.725	.450	-.763	.730			
			.500	-.749	.732	.500	-.714	.737			
			.550	-.696	.740	.550	-.656	.746			
			.600	-.635	.749	.600	-.584	.756			
			.650	-.569	.758	.700	-.405	.783			
			.700	-.489	.770	.800	-.229	.809			
			.800	-.287	.800	.900	-.148	.821			
			.900	-.099	.828	.950	-.129	.824			
			.950	-.063	.833	.990	-.123	.824			
			.990	-.038	.837						
					LOWER SURFACE						
.100	.315	.889	.025	.798	.961	.025	.913	.978	.100	.158	.866
.300	-.108	.827	.050	.550	.924	.050	.509	.918	.300	-.172	.817
.600	-.174	.817	.100	.282	.884	.100	.276	.883	.600	-.204	.812
.800	.297	.886	.200	.056	.851	.200	.033	.847	.800	.252	.880
			.300	-.090	.829	.300	-.107	.827			
			.400	-.168	.818	.400	-.209	.812			
			.500	-.257	.805	.500	-.202	.813			
			.600	-.095	.829	.600	-.133	.823			
			.700	.136	.863	.700	.086	.855			
			.800	.321	.890	.800	.310	.888			
			.900	.388	.900	.900	.335	.892			
			.950	.341	.893	.950	.340	.893			
			1.000	-.043	.836						
CN=				1.0360			.9979				
CM=				-.0643			-.0489				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(b) M = 0.50. Concluded.

$\delta_a = 0^o$; $\alpha = 8.81^o$; $C_L = 1.040$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.155	.376	0.000	.236	.877	0.000	.062	.852	.050	-2.934	.408
.150	-1.801	.576	.012	-2.881	.416	.012	-3.064	.389	.150	-1.416	.633
.300	-.952	.702	.025	-3.500	.325	.025	-3.545	.318	.300	-1.222	.662
.450	-.656	.745	.050	-3.251	.361	.050	-3.287	.356	.450	-.747	.732
.600	-.514	.766	.100	-2.502	.472	.100	-2.316	.500	.600	-.540	.763
.800	-.252	.805	.150	-1.868	.566	.150	-1.725	.587	.800	-.361	.789
.950	-.092	.829	.200	-1.471	.625	.200	-1.313	.648			
			.300	-1.038	.689	.300	-1.011	.693			
			.350	-.907	.708	.350	-.901	.709			
			.400	-.831	.720	.400	-.815	.722			
			.450	-.774	.728	.450	-.753	.731			
			.500	-.711	.737	.500	-.684	.741			
			.550	-.642	.748	.550	-.627	.750			
			.600	-.578	.757	.600	-.558	.760			
			.650	-.502	.768	.700	-.382	.786			
			.700	-.440	.777	.800	-.250	.806			
			.800	-.239	.807	.900	-.165	.818			
			.900	-.140	.822	.950	-.173	.817			
			.950	-.085	.829	.990	-.140	.822			
			.990	-.047	.836						
					LOWER SURFACE						
.100	.473	.898	.025	.852	.969	.025	.943	.982	.100	.216	.874
.300	-.078	.831	.050	.616	.934	.050	.577	.928	.300	-.139	.822
.600	-.181	.816	.100	.352	.895	.100	.322	.890	.600	-.201	.813
.800	.289	.885	.200	.105	.858	.200	.080	.854	.800	.256	.880
			.300	-.056	.834	.300	-.066	.833			
			.400	-.136	.822	.400	-.180	.816			
			.500	-.241	.807	.500	-.196	.814			
			.600	-.091	.829	.600	-.126	.824			
			.700	.130	.862	.700	.098	.857			
			.800	.326	.891	.800	.302	.887			
			.900	.388	.900	.900	.337	.892			
			.950	.338	.893	.950	.332	.892			
			1.000	-.071	.832						
CN=				1.0788			1.0630				
CM=				-.0542			-.0427				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60

$\delta_a = -6^o$; $\alpha = -4.51^o$; $C_L = -0.194$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.324	.720	0.000	1.017	.584	0.000	.068	.757	.050	-.171	.750
.150	-.447	.695	.012	.439	.881	.012	.427	.868	.150	-.347	.715
.300	-.455	.694	.025	.087	.803	.025	.137	.811	.300	-.336	.706
.450	-.372	.710	.050	-.305	.723	.050	-.139	.746	.450	-.346	.707
.600	-.471	.691	.100	-.372	.710	.100	-.302	.724	.600	-.342	.708
.800	-.404	.704	.150	-.357	.705	.150	-.300	.724	.800	-.203	.744
.950	.083	.800	.200	-.445	.696	.200	-.389	.707			
			.300	-.456	.693	.300	-.423	.700			
			.350	-.433	.698	.350	-.408	.704			
			.400	-.452	.694	.400	-.398	.705			
			.450	-.422	.700	.450	-.424	.700			
			.500	-.512	.683	.500	-.451	.695			
			.550	-.522	.681	.550	-.432	.698			
			.600	-.461	.693	.600	-.424	.700			
			.650	-.523	.679	.700	-.267	.731			
			.700	-.499	.685	.800	-.193	.746			
			.800	-.345	.716	.900	-.044	.775			
			.900	-.273	.763	.950	.059	.795			
			.950	.052	.794	.990	.147	.813			
			.990	.123	.808						
					LOWER SURFACE						
.100	-.958	.594	.025	-.586	.589	.025	-.917	.602	.100	-1.511	.485
.300	-.757	.634	.050	-1.431	.507	.050	-1.494	.488	.300	-.739	.638
.600	-.316	.721	.100	-1.140	.558	.100	-1.280	.531	.600	-.392	.706
.800	.060	.797	.200	-.932	.599	.200	-.935	.599	.800	-.014	.781
			.300	-.845	.617	.300	-.847	.615			
			.400	-.742	.637	.400	-.784	.629			
			.500	-.668	.652	.500	-.662	.653			
			.600	-.313	.729	.600	-.426	.699			
			.700	.012	.786	.700	-.129	.758			
			.800	.136	.811	.800	.075	.799			
			.900	.223	.828	.900	.128	.809			
			.950	.260	.835	.950	.192	.822			
			1.000	.136	.811						
CN=				-.1187			-.2657				
CM=				-.0943			-.0551				

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = -3.01^o$; $C_L = -0.031$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.541	.667	0.000	1.070	.595	0.000	.074	.798	.050	-.412	.702
.150	-.543	.676	.012	.207	.825	.012	.206	.824	.150	-.466	.691
.300	-.534	.674	.025	-.224	.739	.025	-.073	.769	.300	-.479	.689
.450	-.425	.700	.050	-.532	.678	.050	-.425	.700	.450	-.427	.699
.600	-.495	.686	.100	-.516	.682	.100	-.454	.693	.600	-.403	.704
.800	-.407	.704	.150	-.534	.678	.150	-.443	.696	.800	-.204	.743
.950	.078	.779	.200	-.543	.668	.200	-.501	.685			
			.300	-.541	.677	.300	-.506	.684			
			.350	-.528	.679	.350	-.478	.689			
			.400	-.510	.683	.400	-.465	.692			
			.450	-.531	.685	.450	-.483	.688			
			.500	-.557	.674	.500	-.501	.686			
			.550	-.558	.673	.550	-.477	.693			
			.600	-.513	.681	.600	-.456	.694			
			.650	-.554	.674	.700	-.292	.729			
			.700	-.524	.680	.800	-.203	.744			
			.800	-.363	.712	.900	-.053	.773			
			.900	-.072	.770	.950	.054	.794			
			.950	.046	.793	.990	.143	.812			
			.990	.111	.806						
					LOWER SURFACE						
.100	-.697	.648	.025	-.637	.658	.025	-.572	.670	.100	-1.071	.572
.300	-.684	.648	.050	-1.017	.582	.050	-1.126	.561	.300	-.686	.648
.600	-.324	.720	.100	-.914	.603	.100	-.970	.592	.600	-.432	.698
.800	.109	.805	.200	-.808	.624	.200	-.800	.625	.800	.040	.792
			.300	-.744	.636	.300	-.776	.630			
			.400	-.691	.647	.400	-.734	.638			
			.500	-.639	.657	.500	-.641	.657			
			.600	-.298	.725	.600	-.431	.699			
			.700	.031	.790	.700	-.138	.756			
			.800	.183	.821	.800	.024	.808			
			.900	.290	.841	.900	.191	.922			
			.950	.292	.842	.950	.256	.834			
			1.000	.118	.807						
CN=				.0329			-.1090				
CM=				-.0999			-.0549				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = -1.70^o$; $C_L = 0.111$

STATION .1542			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.742	.627	0.000	1.031	.557	0.000	.075	.793	.050	-.659	.654
.150	-.677	.650	.012	.011	.786	.012	-.044	.775	.150	-.570	.671
.300	-.611	.664	.025	-.453	.654	.025	-.377	.709	.300	-.538	.678
.450	-.585	.644	.050	-.753	.635	.050	-.682	.643	.450	-.461	.693
.600	-.525	.630	.100	-.735	.639	.100	-.651	.655	.500	-.416	.701
.800	-.404	.704	.150	-.666	.648	.150	-.586	.668	.800	-.206	.743
.950	.060	.776	.200	-.682	.649	.200	-.618	.662			
			.300	-.615	.659	.300	-.590	.667			
			.350	-.587	.664	.350	-.557	.674			
			.400	-.572	.667	.400	-.525	.680			
			.450	-.552	.675	.450	-.534	.678			
			.500	-.612	.663	.500	-.533	.677			
			.550	-.605	.664	.550	-.510	.683			
			.600	-.580	.673	.600	-.484	.688			
			.650	-.556	.679	.700	-.298	.725			
			.700	-.536	.678	.800	-.221	.740			
			.800	-.367	.711	.900	-.059	.772			
			.900	-.072	.770	.950	.045	.793			
			.950	.040	.792	.990	.126	.809			
			.990	.088	.801						
					LOWER SURFACE						
.100	-.576	.670	.025	-.403	.704	.025	-.422	.720	.100	-.508	.685
.300	-.617	.662	.050	-.733	.638	.050	-.807	.624	.300	-.638	.658
.600	-.520	.721	.100	-.733	.639	.100	-.771	.632	.600	-.433	.698
.800	.160	.815	.200	-.665	.649	.200	-.691	.647	.800	.076	.799
			.300	-.665	.653	.300	-.701	.645			
			.400	-.628	.660	.400	-.687	.648			
			.500	-.607	.664	.500	-.615	.662			
			.600	-.291	.728	.600	-.426	.700			
			.700	.049	.794	.700	-.136	.757			
			.800	.212	.826	.800	.145	.813			
			.900	.302	.844	.900	.235	.833			
			.950	.307	.845	.950	.294	.842			
			1.000	.106	.805						
CN=				.1674			.0332				
CM=				-.1007			-.0533				

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = -0.38^o$; $C_L = 0.243$

STATION .1542			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.123	.561	0.000	1.075	.557	0.000	.081	.800	.050	-.569	.694
.150	-.822	.622	.012	-.364	.711	.012	-.377	.710	.150	-.703	.645
.300	-.693	.647	.025	-.909	.625	.025	-.650	.655	.300	-.635	.665
.450	-.634	.674	.050	-1.057	.567	.050	-.771	.592	.450	-.496	.686
.600	-.547	.678	.100	-.833	.599	.100	-.711	.624	.500	-.435	.698
.800	-.401	.709	.150	-.846	.617	.150	-.736	.639	.800	-.212	.742
.950	.052	.774	.200	-.741	.639	.200	-.714	.643			
			.300	-.727	.644	.300	-.664	.653			
			.350	-.671	.651	.350	-.609	.664			
			.400	-.641	.657	.400	-.575	.670			
			.450	-.612	.665	.450	-.574	.671			
			.500	-.659	.656	.500	-.575	.670			
			.550	-.635	.659	.550	-.546	.676			
			.600	-.586	.668	.600	-.505	.684			
			.650	-.532	.667	.700	-.308	.723			
			.700	-.553	.675	.800	-.224	.740			
			.800	-.357	.712	.900	-.062	.772			
			.900	-.079	.768	.950	.041	.792			
			.950	.026	.790	.990	.116	.807			
			.990	.077	.799						
					LOWER SURFACE						
.100	-.430	.707	.025	-.137	.757	.025	-.041	.776	.100	-.704	.645
.300	-.557	.674	.050	-.444	.694	.050	-.572	.671	.300	-.580	.669
.600	-.313	.721	.100	-.554	.675	.100	-.535	.683	.600	-.434	.698
.800	.141	.823	.200	-.552	.673	.200	-.600	.665	.800	.102	.804
			.300	-.541	.675	.300	-.627	.660			
			.400	-.531	.677	.400	-.639	.658			
			.500	-.573	.671	.500	-.579	.670			
			.600	-.271	.731	.600	-.409	.703			
			.700	.052	.794	.700	-.132	.754			
			.800	.244	.832	.800	.156	.815			
			.900	.334	.850	.900	.252	.834			
			.950	.326	.848	.950	.306	.844			
			1.000	.078	.800						
CN=				.3059			.1612				
CM=				-.0950			-.0481				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = 0.99^o$; $C_L = 0.376$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.477	.492	0.000	1.050	.992	0.000	.079	.800	.050	-1.322	.523
.150	-.971	.592	.012	-.625	.660	.012	-.714	.643	.150	-.811	.624
.300	-.746	.637	.025	-1.177	.551	.025	-.928	.601	.300	-.665	.652
.450	-.575	.670	.050	-1.430	.491	.050	-1.312	.525	.450	-.527	.680
.600	-.563	.673	.100	-1.155	.556	.100	-1.077	.571	.600	-.448	.695
.800	-.386	.708	.150	-.913	.592	.150	-.860	.614	.800	-.212	.742
.950	.039	.792	.200	-.915	.603	.200	-.944	.617			
			.300	-.778	.630	.300	-.752	.635			
			.350	-.729	.640	.350	-.684	.649			
			.400	-.693	.649	.400	-.634	.659			
			.450	-.662	.653	.450	-.621	.661			
			.500	-.682	.649	.500	-.611	.663			
			.550	-.661	.653	.550	-.575	.670			
			.600	-.622	.661	.600	-.526	.680			
			.650	-.618	.662	.700	-.321	.720			
			.700	-.558	.674	.800	-.228	.739			
			.800	-.355	.714	.900	-.062	.772			
			.900	-.074	.769	.950	.037	.791			
			.950	.020	.788	.990	.102	.804			
			.990	.058	.795						
					LOWER SURFACE						
.100	-.213	.742	.025	.067	.757	.025	.181	.820	.100	-.548	.676
.300	-.461	.693	.050	-.251	.734	.050	-.349	.715	.300	-.529	.679
.600	-.304	.724	.100	-.355	.714	.100	-.406	.704	.600	-.432	.699
.800	.214	.826	.200	-.456	.694	.200	-.475	.690	.800	.116	.807
			.300	-.467	.686	.300	-.551	.675			
			.400	-.524	.680	.400	-.577	.670			
			.500	-.533	.679	.500	-.540	.677			
			.600	-.256	.733	.600	-.389	.707			
			.700	.065	.797	.700	-.127	.759			
			.800	.261	.836	.900	.167	.817			
			.900	.355	.854	.900	.263	.836			
			.950	.338	.851	.950	.316	.846			
			1.000	.070	.798						
CN=				.4425			.3029				
CM=				-.0947			-.0426				

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = 2.30^o$; $C_L = 0.501$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.890	.411	0.000	.990	.980	0.000	.092	.800	.050	-1.777	.433
.150	-1.050	.577	.012	-.944	.537	.012	-.973	.592	.150	-.927	.601
.300	-.800	.626	.025	-1.555	.477	.025	-1.245	.539	.300	-.715	.643
.450	-.625	.661	.050	-1.852	.418	.050	-1.920	.425	.450	-.551	.675
.600	-.575	.671	.100	-1.400	.508	.100	-1.230	.541	.600	-.455	.694
.800	-.367	.712	.150	-1.086	.570	.150	-.980	.590	.800	-.206	.743
.990	.024	.789	.200	-1.008	.585	.200	-.947	.597			
			.300	-.841	.618	.300	-.815	.623			
			.350	-.783	.629	.350	-.737	.638			
			.400	-.751	.636	.400	-.680	.650			
			.450	-.712	.643	.450	-.659	.654			
			.500	-.725	.641	.500	-.642	.657			
			.550	-.683	.649	.550	-.593	.667			
			.600	-.632	.659	.600	-.539	.678			
			.650	-.616	.662	.700	-.324	.720			
			.700	-.555	.674	.800	-.224	.740			
			.800	-.319	.721	.900	-.060	.772			
			.900	-.072	.770	.950	.029	.790			
			.950	-.007	.783	.990	.080	.800			
			.990	.028	.790						
					LOWER SURFACE						
.100	-.111	.762	.025	.243	.832	.025	.365	.854	.100	-.364	.706
.300	-.402	.705	.050	-.062	.772	.050	-.134	.757	.300	-.472	.691
.600	-.293	.726	.100	-.210	.743	.100	-.269	.733	.600	-.417	.702
.800	.225	.828	.200	-.361	.713	.200	-.378	.709	.800	.122	.808
			.300	-.434	.698	.300	-.474	.691			
			.400	-.456	.694	.400	-.523	.681			
			.500	-.503	.685	.500	-.502	.685			
			.600	-.240	.737	.600	-.370	.711			
			.700	.075	.799	.700	-.121	.760			
			.800	.282	.840	.800	.172	.818			
			.900	.357	.855	.900	.272	.838			
			.950	.336	.850	.950	.322	.848			
			1.000	.034	.791						
CN=				.5015			.4261				
CM=				-.0884			-.0358				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = 3.66^o$; $C_L = 0.634$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.235	.344	0.000	.904	.963	0.000	.084	.801	.050	-2.106	.368
.150	-1.066	.573	.012	-1.161	.555	.012	-1.269	.533	.150	-.991	.588
.300	-.342	.614	.025	-1.830	.428	.025	-1.481	.491	.300	-.755	.635
.450	-.640	.654	.050	-2.167	.356	.050	-2.097	.379	.450	-.564	.673
.600	-.581	.669	.100	-2.155	.350	.100	-2.011	.387	.600	-.444	.696
.800	-.358	.718	.150	-1.127	.561	.150	-1.059	.575	.800	-.204	.744
.950	.027	.739	.200	-1.020	.583	.200	-.995	.588			
			.300	-.901	.606	.300	-.867	.613			
			.350	-.829	.620	.350	-.775	.631			
			.400	-.773	.631	.400	-.713	.643			
			.450	-.734	.639	.450	-.677	.650			
			.500	-.729	.640	.500	-.655	.655			
			.550	-.696	.646	.550	-.599	.666			
			.600	-.649	.656	.600	-.543	.677			
			.650	-.606	.664	.700	-.323	.720			
			.700	-.548	.676	.800	-.220	.741			
			.800	-.314	.722	.900	-.060	.772			
			.900	-.063	.772	.950	.016	.787			
			.950	-.005	.783	.990	.063	.797			
			.990	.015	.787						
					LOWER SURFACE						
.100	-.016	.781	.025	.413	.866	.025	.524	.888	.100	-.252	.734
.300	-.340	.717	.050	.152	.814	.050	.046	.793	.300	-.421	.701
.600	-.272	.730	.100	-.083	.768	.100	-.144	.756	.600	-.399	.705
.800	.245	.832	.200	-.248	.735	.200	-.282	.728	.800	.127	.809
			.300	-.237	.717	.300	-.398	.705			
			.400	-.392	.707	.400	-.470	.691			
			.500	-.445	.696	.500	-.463	.693			
			.600	-.210	.747	.600	-.355	.714			
			.700	.097	.801	.700	-.110	.762			
			.800	.295	.842	.900	.178	.819			
			.900	.381	.859	.300	.279	.839			
			.950	.343	.852	.950	.319	.847			
			1.000	.017	.787						
CN=				.6925			.5538				
CM=				-.0813			-.0252				

(c) M = 0.60. Continued.

$\delta_a = -6^o$; $\alpha = 5.06^o$; $C_L = 0.781$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.494	.292	0.000	.838	.950	0.000	.084	.801	.050	-2.354	.319
.150	-1.467	.494	.012	-1.410	.533	.012	-1.564	.474	.150	-1.195	.548
.300	-.867	.613	.025	-2.032	.383	.025	-1.872	.414	.300	-.774	.631
.450	-.663	.653	.050	-2.415	.307	.050	-2.299	.330	.450	-.571	.671
.600	-.584	.669	.100	-2.539	.283	.100	-2.405	.309	.600	-.437	.698
.800	-.349	.715	.150	-2.212	.328	.150	-1.659	.457	.800	-.217	.741
.950	.025	.749	.200	-1.056	.576	.200	-1.043	.578			
			.300	-.878	.611	.300	-.882	.610			
			.350	-.839	.619	.350	-.794	.627			
			.400	-.800	.626	.400	-.731	.640			
			.450	-.760	.634	.450	-.700	.646			
			.500	-.745	.637	.500	-.669	.652			
			.550	-.707	.644	.550	-.601	.664			
			.600	-.653	.655	.600	-.546	.676			
			.650	-.616	.662	.700	-.324	.720			
			.700	-.558	.674	.800	-.225	.740			
			.800	-.326	.720	.900	-.068	.771			
			.900	-.081	.768	.950	.004	.786			
			.950	-.003	.784	.990	.053	.794			
			.990	.033	.790						
					LOWER SURFACE						
.100	.083	.802	.025	.547	.852	.025	.666	.716	.100	-.115	.761
.300	-.270	.731	.050	.256	.835	.050	.208	.825	.300	-.356	.714
.600	-.236	.737	.100	.049	.794	.100	-.002	.784	.600	-.389	.707
.800	.270	.817	.200	-.143	.755	.200	-.183	.748	.900	.128	.809
			.300	-.262	.737	.300	-.318	.721			
			.400	-.332	.719	.400	-.417	.702			
			.500	-.402	.705	.500	-.418	.701			
			.600	-.181	.748	.600	-.333	.718			
			.700	.102	.804	.700	-.101	.764			
			.800	.312	.846	.900	.184	.820			
			.900	.402	.864	.900	.291	.842			
			.950	.371	.857	.950	.322	.848			
			1.000	.044	.754						
CN=				.8536			.6834				
CM=				-.0753			-.0166				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = -4.40^o$; $C_L = -0.163$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.328	.719	0.000	1.027	.587	0.000	.064	.797	.050	-.216	.741
.150	-.454	.654	.012	.383	.859	.012	.396	.862	.150	-.377	.709
.300	-.482	.688	.025	.049	.753	.025	.103	.804	.300	-.427	.689
.450	-.394	.706	.050	-.347	.715	.050	-.232	.738	.450	-.417	.701
.600	-.475	.690	.100	-.385	.737	.100	-.342	.716	.600	-.427	.699
.800	-.399	.705	.150	-.429	.695	.150	-.339	.717	.800	-.274	.730
.950	.070	.797	.200	-.450	.695	.200	-.413	.702			
			.300	-.466	.692	.300	-.440	.697			
			.350	-.468	.691	.350	-.436	.697			
			.400	-.496	.691	.400	-.427	.699			
			.450	-.444	.696	.450	-.460	.693			
			.500	-.516	.681	.500	-.482	.688			
			.550	-.526	.680	.550	-.487	.687			
			.600	-.493	.688	.600	-.477	.689			
			.650	-.527	.679	.700	-.353	.714			
			.700	-.506	.684	.800	-.270	.730			
			.800	-.355	.713	.900	-.045	.775			
			.300	-.371	.770	.950	.059	.795			
			.950	.055	.795	.990	.127	.809			
			.990	.122	.808						
					LOWER SURFACE						
.100	-.911	.603	.025	-.895	.606	.025	-.853	.615	.100	-1.454	.496
.300	-.747	.636	.050	-1.298	.527	.050	-1.435	.500	.300	-.721	.641
.600	-.332	.713	.100	-1.169	.552	.100	-1.192	.543	.600	-.366	.711
.800	.084	.800	.200	-.897	.606	.200	-.908	.604	.800	.053	.794
			.300	-.818	.622	.300	-.819	.622			
			.400	-.735	.634	.400	-.748	.636			
			.500	-.664	.652	.500	-.619	.661			
			.600	-.290	.726	.600	-.374	.710			
			.700	.015	.787	.700	-.077	.768			
			.800	.135	.810	.800	.133	.810			
			.900	.262	.835	.300	.184	.820			
			.950	.280	.839	.950	.243	.832			
			1.000	.136	.811						
CN=				-.0565			-.1773				
CM=				-.0954			-.0781				

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = -3.03^o$; $C_L = -0.014$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.593	.667	0.000	1.074	.954	0.000	.072	.798	.050	-.473	.690
.150	-.575	.670	.012	.155	.820	.012	.165	.816	.150	-.484	.688
.300	-.549	.675	.025	-.265	.731	.025	-.115	.761	.300	-.486	.688
.450	-.446	.696	.050	-.534	.678	.050	-.467	.692	.450	-.455	.694
.600	-.500	.685	.100	-.547	.676	.100	-.496	.686	.600	-.447	.695
.800	-.409	.703	.150	-.547	.675	.150	-.461	.693	.800	-.284	.728
.950	.065	.797	.200	-.557	.672	.200	-.519	.681			
			.300	-.556	.674	.300	-.538	.677			
			.350	-.543	.675	.350	-.498	.685			
			.400	-.538	.678	.400	-.492	.687			
			.450	-.516	.682	.450	-.512	.683			
			.500	-.581	.669	.500	-.538	.678			
			.550	-.575	.670	.550	-.526	.680			
			.600	-.524	.680	.600	-.519	.681			
			.650	-.567	.672	.700	-.371	.711			
			.700	-.542	.677	.300	-.281	.728			
			.800	-.365	.712	.900	-.056	.773			
			.900	-.075	.769	.950	.049	.794			
			.950	.044	.792	.990	.108	.805			
			.990	.101	.804						
					LOWER SURFACE						
.100	-.686	.668	.025	-.585	.668	.025	-.512	.683	.100	-1.085	.569
.300	-.692	.667	.050	-.993	.587	.050	-1.077	.571	.300	-.672	.651
.600	-.324	.720	.100	-.936	.599	.100	-.939	.593	.600	-.390	.707
.800	.126	.809	.200	-.776	.630	.200	-.775	.631	.800	.097	.803
			.300	-.739	.638	.300	-.751	.635			
			.400	-.670	.651	.400	-.710	.643			
			.500	-.630	.659	.500	-.600	.665			
			.600	-.291	.726	.600	-.375	.710			
			.700	.036	.781	.700	-.075	.769			
			.800	.130	.821	.800	.162	.816			
			.900	.285	.840	.900	.228	.829			
			.950	.302	.844	.950	.278	.839			
			1.000	.115	.807						
CN=				.0505			-.0303				
CM=				-.1039			-.0764				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = -1.61^o$; $C_L = 0.138$

STATION .1592			STATION .4245			STATION .7425			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.443	.617	0.000	1.036	.558	0.000	.076	.799	.050	-.751	.535
.150	-.723	.541	.010	-.674	.769	.010	-.123	.759	.150	-.634	.658
.300	-.610	.663	.025	-.528	.679	.025	-.379	.709	.300	-.569	.671
.450	-.499	.695	.050	-.302	.625	.050	-.730	.639	.450	-.432	.686
.600	-.532	.673	.100	-.743	.637	.100	-.701	.645	.600	-.468	.691
.800	-.406	.704	.150	-.704	.644	.150	-.623	.660	.800	-.289	.726
.950	.057	.795	.200	-.696	.646	.200	-.640	.657			
			.300	-.643	.656	.300	-.619	.661			
			.350	-.616	.662	.350	-.580	.669			
			.400	-.602	.665	.400	-.562	.674			
			.450	-.594	.671	.450	-.567	.671			
			.500	-.625	.660	.500	-.574	.670			
			.550	-.616	.662	.550	-.564	.672			
			.600	-.536	.668	.600	-.544	.676			
			.650	-.597	.666	.700	-.387	.707			
			.700	-.551	.675	.800	-.292	.726			
			.900	-.369	.711	.900	-.059	.772			
			.950	-.038	.766	.950	.038	.791			
			.990	.023	.788	.990	.091	.802			
			.990	.090	.802						
					LOWER SURFACE						
.100	-.527	.679	.025	-.332	.718	.025	-.254	.733	.100	-.842	.617
.300	-.601	.665	.050	-.668	.643	.050	-.754	.634	.300	-.615	.662
.600	-.333	.713	.100	-.733	.639	.100	-.720	.641	.600	-.387	.707
.800	.173	.813	.200	-.662	.653	.200	-.655	.654	.800	.137	.811
			.300	-.641	.657	.300	-.666	.652			
			.400	-.618	.661	.400	-.651	.655			
			.500	-.592	.667	.500	-.564	.672			
			.600	-.278	.729	.600	-.360	.712			
			.700	.052	.784	.700	-.066	.771			
			.800	.226	.828	.800	.194	.822			
			.900	.318	.847	.900	.264	.836			
			.950	.314	.846	.950	.305	.844			
			1.000	.100	.803						
CN=				.1351			.1207				
CM=				-.1055			-.0749				

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = -0.26^o$; $C_L = 0.274$

STATION .1592			STATION .4245			STATION .7425			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.130	.556	0.000	1.076	.557	0.000	.073	.793	.050	-1.036	.579
.150	-.872	.611	.010	-.372	.710	.010	-.447	.695	.150	-.757	.634
.300	-.692	.647	.025	-.930	.606	.025	-.676	.650	.300	-.631	.659
.450	-.548	.675	.050	-1.159	.555	.050	-1.077	.571	.450	-.530	.679
.600	-.550	.675	.100	-.538	.638	.100	-.864	.613	.600	-.488	.687
.800	-.409	.703	.150	-.855	.613	.150	-.745	.635	.800	-.294	.726
.950	.044	.793	.200	-.823	.621	.200	-.756	.634			
			.300	-.726	.640	.300	-.705	.644			
			.350	-.690	.647	.350	-.648	.656			
			.400	-.658	.654	.400	-.619	.661			
			.450	-.624	.660	.450	-.614	.662			
			.500	-.667	.652	.500	-.623	.661			
			.550	-.652	.655	.550	-.592	.667			
			.600	-.607	.664	.600	-.565	.672			
			.650	-.615	.662	.700	-.393	.705			
			.700	-.564	.672	.800	-.290	.726			
			.800	-.368	.711	.900	-.064	.771			
			.900	-.070	.770	.950	.022	.788			
			.950	.019	.788	.990	.067	.797			
			.990	.072	.798						
					LOWER SURFACE						
.100	-.360	.713	.025	-.332	.764	.025	-.009	.782	.100	-.678	.650
.300	-.524	.680	.050	-.415	.732	.050	-.533	.678	.300	-.559	.673
.600	-.314	.722	.100	-.524	.680	.100	-.560	.673	.600	-.396	.708
.800	.184	.821	.200	-.547	.676	.200	-.543	.676	.800	.165	.816
			.300	-.582	.669	.300	-.589	.667			
			.400	-.556	.673	.400	-.603	.664			
			.500	-.550	.673	.500	-.621	.681			
			.600	-.264	.732	.600	-.349	.715			
			.700	.059	.795	.700	-.062	.771			
			.800	.245	.832	.800	.210	.825			
			.900	.339	.851	.900	.282	.840			
			.950	.333	.850	.950	.319	.847			
			1.000	.040	.800						
CN=				.3345			.2553				
CM=				-.1611			-.0711				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = 1.10^o$; $C_L = 0.406$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.507	.486	0.000	1.016	.591	0.000	.074	.794	.050	-1.457	.495
.150	-.995	.587	.012	-.665	.645	.012	-.763	.633	.150	-.844	.614
.300	-.756	.644	.025	-1.197	.547	.025	-.934	.587	.300	-.650	.647
.450	-.588	.667	.050	-1.542	.475	.050	-1.406	.506	.450	-.556	.674
.600	-.563	.671	.100	-1.144	.557	.100	-1.113	.564	.500	-.438	.686
.800	-.394	.706	.150	-.993	.587	.150	-.875	.611	.600	-.295	.725
.950	.042	.799	.200	-.838	.595	.200	-.678	.613			
			.300	-.913	.623	.300	-.784	.629			
			.350	-.749	.636	.350	-.724	.641			
			.400	-.704	.644	.400	-.671	.651			
			.450	-.666	.644	.450	-.661	.653			
			.500	-.655	.646	.500	-.655	.654			
			.550	-.677	.650	.550	-.670	.661			
			.600	-.647	.653	.600	-.682	.669			
			.650	-.615	.661	.700	-.735	.705			
			.700	-.560	.673	.800	-.287	.727			
			.800	-.350	.713	.900	-.067	.771			
			.900	-.071	.770	.950	.009	.795			
			.950	.016	.787	.998	.044	.792			
			.990	.045	.792						
					LOWER SURFACE						
.100	-.229	.734	.025	.056	.803	.025	.206	.524	.100	-.500	.685
.300	-.494	.694	.050	-.240	.735	.050	-.304	.724	.300	-.507	.683
.600	-.291	.725	.100	-.352	.714	.100	-.382	.709	.450	-.328	.709
.800	.225	.828	.200	-.431	.699	.200	-.463	.692	.800	.175	.814
			.300	-.482	.688	.300	-.505	.684			
			.400	-.509	.684	.400	-.545	.676			
			.500	-.513	.681	.500	-.484	.647			
			.600	-.242	.735	.600	-.324	.719			
			.700	.075	.793	.700	-.054	.773			
			.800	.269	.837	.800	.218	.827			
			.900	.355	.854	.900	.296	.842			
			.950	.343	.852	.950	.327	.848			
			1.000	.052	.794						
CN=				.4587			.1876				
CM=				-.0577			-.0651				

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = 2.38^o$; $C_L = 0.527$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.440	.499	0.000	.577	.577	0.000	.042	.830	.050	-1.516	.474
.150	-1.061	.574	.012	-.954	.592	.012	-.994	.585	.150	-.966	.592
.300	-.817	.622	.025	-1.514	.513	.025	-1.243	.545	.300	-.761	.637
.450	-.619	.661	.050	-1.867	.414	.050	-1.871	.512	.450	-.583	.669
.600	-.578	.669	.100	-1.443	.494	.100	-1.274	.531	.500	-.506	.684
.800	-.467	.711	.150	-1.083	.565	.150	-.996	.565	.600	-.276	.729
.950	.022	.784	.200	-1.035	.579	.200	-.865	.578			
			.300	-.873	.611	.300	-.842	.617			
			.350	-.800	.625	.350	-.764	.642			
			.400	-.752	.635	.400	-.705	.654			
			.450	-.725	.640	.450	-.677	.657			
			.500	-.726	.640	.500	-.677	.659			
			.550	-.693	.646	.550	-.639	.668			
			.600	-.634	.658	.600	-.589	.677			
			.650	-.622	.661	.700	-.394	.706			
			.700	-.596	.675	.800	-.271	.739			
			.800	-.337	.717	.900	-.064	.778			
			.900	-.071	.770	.950	-.014	.791			
			.950	-.011	.781	.998	.014	.786			
			.990	.013	.787						
					LOWER SURFACE						
.100	-.099	.744	.025	.215	.830	.025	.401	.664	.100	-.342	.716
.300	-.392	.706	.050	-.043	.775	.050	-.162	.743	.300	-.446	.695
.600	-.291	.729	.100	-.214	.741	.100	-.244	.734	.500	-.356	.711
.800	.236	.840	.200	-.333	.719	.200	-.355	.713	.600	.142	.820
			.300	-.423	.700	.400	-.434	.698			
			.400	-.469	.695	.400	-.495	.685			
			.500	-.483	.688	.500	-.459	.693			
			.600	-.224	.729	.600	-.312	.722			
			.700	.070	.797	.700	-.051	.774			
			.800	.274	.849	.800	.225	.828			
			.900	.357	.865	.900	.305	.844			
			.950	.336	.861	.950	.329	.849			
			1.000	.032	.790						
CN=				.5797			.5016				
CM=				-.0908			-.0676				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = -3^o$; $\alpha = 3.73^o$; $C_L = 0.663$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.192	.350	0.000	.862	.960	0.000	.082	.900	.050	-2.135	.350
.150	-1.076	.571	.012	-1.197	.547	.012	-1.311	.524	.150	-.575	.590
.300	-.864	.613	.025	-1.742	.429	.025	-1.540	.479	.300	-.768	.631
.450	-.656	.654	.050	-2.133	.331	.050	-2.089	.370	.450	-.595	.667
.600	-.585	.668	.100	-2.251	.334	.100	-2.083	.371	.600	-.491	.686
.800	-.370	.710	.150	-1.846	.417	.150	-1.024	.581	.800	-.273	.729
.950	.030	.780	.200	-.488	.583	.200	-.486	.589			
			.300	-.900	.605	.300	-.490	.607			
			.350	-.845	.616	.350	-.804	.624			
			.400	-.790	.629	.400	-.740	.637			
			.450	-.755	.634	.450	-.718	.641			
			.500	-.736	.637	.500	-.699	.645			
			.550	-.710	.643	.550	-.664	.655			
			.600	-.692	.652	.600	-.594	.668			
			.650	-.631	.659	.700	-.493	.706			
			.700	-.560	.673	.800	-.266	.731			
			.800	-.329	.713	.900	-.074	.769			
			.900	-.072	.769	.950	-.016	.780			
			.950	-.005	.783	.990	.006	.785			
			.990	.021	.788						
					LOWER SURFACE						
.100	.032	.790	.025	.423	.867	.025	.547	.890	.100	-.222	.738
.300	-.334	.718	.050	.139	.811	.050	.048	.793	.300	-.380	.708
.600	-.254	.732	.100	-.033	.765	.100	-.090	.756	.600	-.353	.714
.800	.257	.844	.200	-.232	.738	.200	-.240	.736	.800	.188	.821
			.300	-.337	.717	.300	-.362	.712			
			.400	-.378	.709	.400	-.446	.695			
			.500	-.437	.697	.500	-.414	.701			
			.600	-.195	.745	.600	-.290	.725			
			.700	.056	.803	.700	-.034	.776			
			.800	.292	.841	.800	.236	.830			
			.900	.381	.859	.900	.315	.846			
			.950	.348	.852	.950	.331	.849			
			1.000	.027	.789						
CN=				.7157			.6299				
CM=				-.0846			-.0483				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -4.30^o$; $C_L = -0.134$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.561	.712	0.000	1.040	.989	0.000	.072	.798	.050	-.278	.724
.150	-.480	.688	.012	.419	.864	.012	.375	.858	.150	-.409	.703
.300	-.491	.695	.025	-.028	.774	.025	.071	.797	.300	-.451	.694
.450	-.434	.677	.050	-.322	.720	.050	-.276	.724	.451	-.444	.696
.600	-.444	.684	.100	-.429	.698	.100	-.338	.716	.600	-.478	.689
.800	-.416	.701	.150	-.459	.693	.150	-.352	.714	.800	-.323	.720
.950	.071	.798	.200	-.486	.687	.200	-.436	.697			
			.300	-.482	.689	.300	-.467	.691			
			.350	-.477	.689	.350	-.448	.695			
			.400	-.478	.689	.400	-.459	.693			
			.450	-.471	.690	.450	-.490	.686			
			.500	-.534	.679	.500	-.527	.679			
			.550	-.544	.676	.550	-.537	.677			
			.600	-.524	.690	.600	-.535	.678			
			.650	-.550	.674	.700	-.457	.693			
			.700	-.536	.677	.800	-.320	.720			
			.800	-.374	.709	.900	-.047	.774			
			.900	-.083	.767	.950	.007	.785			
			.950	.049	.793	.990	.037	.791			
			.990	.119	.807						
					LOWER SURFACE						
.100	-.989	.583	.025	-.839	.607	.025	-.787	.628	.100	-1.286	.529
.300	-.725	.640	.050	-1.250	.536	.050	-1.387	.509	.300	-.693	.646
.600	-.419	.720	.100	-1.101	.565	.100	-1.181	.550	.600	-.315	.721
.800	.048	.803	.200	-.870	.611	.200	-.871	.611	.800	.114	.806
			.300	-.819	.621	.300	-.789	.627			
			.400	-.703	.644	.400	-.709	.643			
			.500	-.640	.657	.500	-.566	.671			
			.600	-.269	.726	.600	-.313	.721			
			.700	.032	.790	.700	-.009	.782			
			.800	.170	.817	.800	.190	.821			
			.900	.240	.831	.900	.255	.834			
			.950	.287	.840	.950	.292	.841			
			1.000	.126	.809						
CN=				-.0553			-.0848				
CM=				-.1047			-.1062				

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -2.91^o$; $C_L = 0.018$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.613	.662	0.000	1.068	.995	0.000	.069	.797	.050	-.562	.672
.150	-.622	.663	.012	.157	.823	.012	.110	.805	.150	-.546	.675
.300	-.564	.672	.025	-.237	.727	.025	-.225	.739	.300	-.509	.683
.450	-.486	.687	.050	-.573	.670	.050	-.508	.683	.450	-.476	.689
.600	-.517	.681	.100	-.602	.664	.100	-.550	.675	.600	-.509	.683
.800	-.413	.702	.150	-.588	.667	.150	-.475	.693	.800	-.355	.713
.950	.089	.797	.200	-.602	.664	.200	-.540	.677			
			.300	-.572	.670	.300	-.563	.672			
			.350	-.550	.675	.350	-.517	.681			
			.400	-.555	.674	.400	-.518	.681			
			.450	-.544	.676	.450	-.544	.676			
			.500	-.583	.668	.500	-.580	.669			
			.550	-.594	.666	.550	-.579	.669			
			.600	-.564	.671	.600	-.563	.672			
			.650	-.581	.668	.700	-.480	.688			
			.700	-.560	.673	.800	-.321	.720			
			.800	-.393	.706	.900	-.060	.772			
			.900	-.092	.765	.950	-.011	.781			
			.950	.039	.791	.990	.010	.785			
			.990	.103	.804						
					LOWER SURFACE						
.100	-.824	.620	.025	-.578	.669	.025	-.505	.684	.100	-1.024	.581
.300	-.649	.655	.050	-.867	.612	.050	-1.042	.577	.300	-.626	.659
.600	-.426	.719	.100	-.901	.605	.100	-.894	.606	.600	-.321	.720
.800	.148	.813	.200	-.763	.632	.200	-.769	.631	.800	.192	.822
			.300	-.727	.639	.300	-.708	.643			
			.400	-.658	.653	.400	-.663	.652			
			.500	-.611	.662	.500	-.541	.676			
			.600	-.285	.727	.600	-.310	.722			
			.700	.054	.794	.700	-.002	.783			
			.800	.210	.825	.800	.252	.833			
			.900	.322	.847	.900	.290	.841			
			.950	.294	.842	.950	.318	.846			
			1.000	.111	.806						
CN=				.0482			.0650				
CM=				-.1105			-.1063				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -2.21^o$; $C_L = 0.093$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.825	.620	0.000	1.073	.996	0.000	.076	.798	.050	-.660	.653
.150	-.650	.655	.012	.019	.787	.012	.017	.787	.150	-.603	.664
.300	-.594	.666	.025	-.403	.704	.025	-.304	.723	.300	-.563	.672
.450	-.509	.683	.050	-.710	.643	.050	-.669	.651	.450	-.505	.683
.600	-.533	.678	.100	-.653	.654	.100	-.605	.664	.600	-.523	.680
.800	-.420	.701	.150	-.656	.654	.150	-.594	.666	.800	-.357	.713
.950	.055	.794	.200	-.659	.653	.200	-.614	.662			
			.300	-.595	.666	.300	-.599	.665			
			.350	-.595	.668	.350	-.558	.673			
			.400	-.591	.668	.400	-.551	.674			
			.450	-.578	.669	.450	-.578	.669			
			.500	-.614	.662	.500	-.602	.664			
			.550	-.617	.661	.550	-.605	.664			
			.600	-.536	.667	.600	-.584	.668			
			.650	-.530	.667	.700	-.486	.687			
			.700	-.570	.671	.800	-.326	.719			
			.800	-.391	.706	.900	-.076	.768			
			.900	-.091	.765	.950	-.020	.779			
			.950	.032	.790	.990	.005	.784			
			.990	.098	.803						
					LOWER SURFACE						
.100	-.674	.650	.025	-.416	.701	.025	-.371	.710	.100	-.587	.588
.300	-.630	.659	.050	-.776	.630	.050	-.866	.612	.300	-.614	.662
.600	-.321	.720	.100	-.778	.629	.100	-.900	.625	.600	-.321	.720
.800	.187	.820	.200	-.713	.642	.200	-.696	.646	.800	.206	.824
			.300	-.654	.646	.300	-.667	.651			
			.400	-.612	.662	.400	-.631	.658			
			.500	-.539	.667	.500	-.520	.680			
			.600	-.278	.728	.600	-.302	.724			
			.700	.053	.794	.700	.002	.784			
			.800	.237	.830	.800	.266	.936			
			.900	.327	.848	.900	.317	.845			
			.950	.330	.849	.950	.327	.848			
			1.000	.115	.806						
CN=				.1557			.1432				
CM=				-.1118			-.1066				

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -1.51^o$; $C_L = 0.168$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.921	.601	0.000	1.083	.998	0.000	.079	.799	.050	-.842	.617
.150	-.742	.637	.012	-.100	.764	.012	-.126	.759	.150	-.675	.650
.300	-.646	.656	.025	-.581	.669	.025	-.451	.694	.300	-.609	.663
.450	-.538	.677	.050	-.804	.624	.050	-.788	.627	.450	-.516	.681
.600	-.543	.676	.100	-.781	.629	.100	-.743	.636	.600	-.521	.680
.800	-.418	.701	.150	-.713	.642	.150	-.682	.649	.800	-.358	.713
.950	.054	.794	.200	-.709	.643	.200	-.675	.650			
			.300	-.652	.654	.300	-.647	.655			
			.350	-.634	.658	.350	-.598	.665			
			.400	-.623	.660	.400	-.586	.668			
			.450	-.609	.663	.450	-.601	.665			
			.500	-.642	.656	.500	-.622	.660			
			.550	-.630	.659	.550	-.618	.661			
			.600	-.606	.664	.600	-.590	.667			
			.650	-.612	.662	.700	-.491	.686			
			.700	-.580	.669	.800	-.321	.720			
			.800	-.401	.704	.900	-.075	.769			
			.900	-.086	.766	.950	-.024	.779			
			.950	.033	.790	.990	-.008	.782			
			.990	.097	.803						
					LOWER SURFACE						
.100	-.597	.665	.025	-.277	.729	.025	-.143	.755	.100	-.821	.621
.300	-.582	.664	.050	-.627	.651	.050	-.490	.647	.300	-.580	.669
.600	-.325	.719	.100	-.665	.651	.100	-.684	.648	.600	-.325	.719
.800	.202	.824	.200	-.660	.653	.200	-.637	.657	.800	.226	.828
			.300	-.633	.658	.300	-.628	.659			
			.400	-.586	.668	.400	-.604	.664			
			.500	-.577	.669	.500	-.507	.683			
			.600	-.270	.730	.600	-.295	.725			
			.700	.069	.797	.700	.014	.786			
			.800	.245	.832	.800	.277	.838			
			.900	.328	.848	.900	.325	.848			
			.950	.330	.849	.950	.340	.851			
			1.000	.095	.802						
CN=				.2328			.2225				
CM=				-.1113			-.1032				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -0.83^o$; $C_L = 0.235$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.093	.567	0.000	1.073	.596	0.000	.077	.799	.050	-.560	.593
.150	-.790	.627	.012	-.224	.739	.012	-.795	.725	.150	-.698	.645
.300	-.683	.652	.025	-.731	.639	.025	-.611	.663	.300	-.634	.658
.450	-.558	.673	.050	-1.002	.585	.050	-.927	.600	.450	-.530	.679
.600	-.553	.674	.100	-.875	.610	.100	-.830	.619	.600	-.536	.678
.800	-.417	.701	.150	-.808	.624	.150	-.734	.638	.800	-.353	.714
.950	.050	.793	.200	-.783	.629	.200	-.739	.637			
			.300	-.692	.647	.300	-.677	.650			
			.350	-.665	.652	.350	-.623	.660			
			.400	-.638	.657	.400	-.615	.662			
			.450	-.634	.658	.450	-.627	.659			
			.500	-.667	.652	.500	-.644	.656			
			.550	-.654	.654	.550	-.629	.659			
			.600	-.623	.660	.600	-.606	.664			
			.650	-.623	.660	.700	-.487	.687			
			.700	-.582	.668	.800	-.323	.720			
			.800	-.384	.708	.900	-.084	.767			
			.900	-.084	.767	.950	-.041	.775			
			.950	.029	.789	.990	-.018	.780			
			.990	.080	.799						
					LOWER SURFACE						
.100	-.520	.681	.025	-.158	.752	.025	-.103	.763	.100	-.736	.638
.300	-.555	.674	.050	-.548	.675	.050	-.647	.656	.300	-.558	.673
.600	-.320	.720	.100	-.569	.671	.100	-.628	.659	.600	-.328	.719
.800	.210	.825	.200	-.570	.671	.200	-.569	.671	.800	.226	.828
			.300	-.585	.668	.300	-.592	.666			
			.400	-.567	.671	.400	-.581	.669			
			.500	-.563	.672	.500	-.495	.686			
			.600	-.258	.733	.600	-.290	.726			
			.700	.068	.797	.700	.020	.787			
			.800	.252	.833	.800	.279	.839			
			.900	.342	.851	.900	.331	.849			
			.950	.332	.849	.950	.336	.850			
			1.000	.081	.800						
CN=				.3046			.2785				
CM=				-.1082			-.1018				

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = -0.21^o$; $C_L = 0.292$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.178	.550	0.000	1.043	.598	0.000	.087	.801	.050	-1.142	.557
.150	-.835	.618	.012	-.371	.710	.012	-.409	.703	.150	-.783	.629
.300	-.696	.646	.025	-.847	.616	.025	-.733	.638	.300	-.649	.655
.450	-.574	.670	.050	-1.116	.563	.050	-1.074	.571	.450	-.554	.674
.600	-.560	.673	.100	-.988	.588	.100	-.917	.602	.600	-.545	.676
.800	-.405	.703	.150	-.869	.611	.150	-.769	.631	.800	-.340	.717
.950	.042	.792	.200	-.826	.620	.200	-.771	.631			
			.300	-.750	.635	.300	-.733	.638			
			.350	-.689	.647	.350	-.658	.653			
			.400	-.663	.652	.400	-.643	.656			
			.450	-.664	.652	.450	-.647	.655			
			.500	-.663	.652	.500	-.654	.654			
			.550	-.660	.653	.550	-.641	.657			
			.600	-.634	.658	.600	-.606	.663			
			.650	-.627	.659	.700	-.482	.688			
			.700	-.574	.670	.800	-.297	.725			
			.800	-.374	.709	.900	-.080	.768			
			.900	-.085	.767	.950	-.055	.773			
			.950	.018	.787	.990	-.053	.773			
			.990	.067	.797						
					LOWER SURFACE						
.100	-.426	.693	.025	-.079	.768	.025	.035	.790	.100	-.647	.656
.300	-.528	.679	.050	-.406	.703	.050	-.520	.681	.300	-.535	.678
.600	-.315	.721	.100	-.515	.682	.100	-.545	.676	.600	-.322	.720
.800	.227	.828	.200	-.515	.682	.200	-.542	.676	.900	.241	.831
			.300	-.570	.671	.300	-.556	.674			
			.400	-.551	.674	.400	-.560	.673			
			.500	-.535	.678	.500	-.485	.688			
			.600	-.251	.734	.600	-.279	.728			
			.700	.070	.797	.700	.027	.789			
			.800	.256	.834	.800	.280	.839			
			.900	.358	.854	.900	.326	.848			
			.950	.332	.849	.950	.334	.850			
			1.000	.070	.797						
CN=				.3551			.3322				
CM=				-.1064			-.0975				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = 0.48^o$; $C_L = 0.361$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.383	.510	0.000	1.057	.593	0.000	.078	.799	.050	-1.378	.511
.150	-.885	.608	.012	-.567	.671	.012	-.610	.663	.150	-.816	.622
.300	-.726	.640	.025	-1.056	.574	.025	-.882	.609	.300	-.679	.649
.450	-.599	.665	.050	-1.341	.518	.050	-1.242	.538	.450	-.563	.672
.600	-.570	.671	.100	-1.113	.563	.100	-1.041	.577	.600	-.545	.676
.800	-.402	.704	.150	-.937	.598	.150	-.895	.614	.800	-.351	.714
.950	.043	.792	.200	-.858	.606	.200	-.851	.615			
			.300	-.774	.630	.300	-.763	.632			
			.350	-.720	.641	.350	-.695	.646			
			.400	-.700	.645	.400	-.667	.652			
			.450	-.692	.647	.450	-.670	.651			
			.500	-.694	.646	.500	-.680	.649			
			.550	-.679	.649	.550	-.656	.654			
			.600	-.645	.656	.600	-.617	.661			
			.650	-.623	.660	.700	-.476	.689			
			.700	-.571	.671	.800	-.291	.726			
			.800	-.369	.710	.900	-.095	.765			
			.900	-.072	.769	.950	-.068	.770			
			.950	.015	.787	.990	-.058	.772			
			.990	.043	.792						
					LOWER SURFACE						
.100	-.370	.710	.025	.026	.789	.025	.122	.808	.100	-.571	.671
.300	-.484	.638	.050	-.310	.722	.050	-.374	.709	.300	-.526	.679
.600	-.302	.724	.100	-.416	.701	.100	-.456	.693	.600	-.320	.720
.800	.233	.830	.200	-.479	.689	.200	-.465	.692	.800	.244	.832
			.300	-.524	.680	.300	-.513	.682			
			.400	-.516	.681	.400	-.530	.679			
			.500	-.527	.679	.500	-.456	.693			
			.600	-.241	.736	.600	-.270	.730			
			.700	.067	.797	.700	.031	.790			
			.800	.267	.836	.800	.286	.840			
			.900	.357	.854	.900	.328	.849			
			.950	.327	.848	.950	.336	.850			
			1.000	.065	.796						
CN=				.4236			.4069				
CM=				-.1017			-.0944				

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = 1.16^o$; $C_L = 0.427$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.560	.475	0.000	1.024	.586	0.000	.081	.799	.050	-1.463	.494
.150	-.957	.594	.012	-.723	.640	.012	-.750	.635	.150	-.874	.611
.300	-.775	.630	.025	-1.272	.532	.025	-1.057	.574	.300	-.713	.642
.450	-.615	.662	.050	-1.555	.476	.050	-1.536	.479	.450	-.587	.667
.600	-.576	.669	.100	-1.209	.544	.100	-1.170	.552	.600	-.562	.672
.800	-.406	.704	.150	-1.014	.583	.150	-.908	.604	.800	-.353	.714
.950	.029	.749	.200	-.950	.595	.200	-.909	.603			
			.300	-.819	.621	.300	-.802	.625			
			.350	-.765	.632	.350	-.734	.638			
			.400	-.728	.639	.400	-.699	.645			
			.450	-.722	.641	.450	-.692	.647			
			.500	-.715	.642	.500	-.695	.646			
			.550	-.685	.648	.550	-.669	.651			
			.600	-.643	.656	.600	-.626	.659			
			.650	-.630	.659	.700	-.478	.689			
			.700	-.594	.668	.800	-.280	.728			
			.800	-.361	.712	.900	-.100	.764			
			.900	-.032	.767	.950	-.076	.769			
			.950	.006	.785	.990	-.077	.768			
			.990	.040	.791						
					LOWER SURFACE						
.100	-.284	.727	.025	.100	.801	.025	.249	.833	.100	-.520	.680
.300	-.443	.696	.050	-.215	.741	.050	-.260	.732	.300	-.432	.688
.600	-.299	.724	.100	-.350	.712	.100	-.353	.714	.600	-.315	.721
.800	.231	.829	.200	-.422	.700	.200	-.434	.698	.800	.243	.832
			.300	-.436	.687	.300	-.494	.686			
			.400	-.439	.687	.400	-.502	.684			
			.500	-.512	.682	.500	-.440	.696			
			.600	-.236	.737	.600	-.267	.731			
			.700	.074	.798	.700	.028	.789			
			.800	.277	.833	.800	.284	.840			
			.900	.361	.855	.900	.329	.849			
			.950	.336	.850	.950	.337	.850			
			1.000	.055	.794						
CN=				.4880			.4732				
CM=				-.1006			-.0887				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = 2.50^o$; $C_L = 0.548$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.925	.403	0.000	.977	.577	0.000	.087	.801	.050	-1.893	.409
.150	-1.074	.571	.012	-.977	.590	.012	-1.075	.571	.150	-.969	.592
.300	-.825	.620	.025	-1.574	.472	.025	-1.325	.521	.300	-.761	.633
.450	-.634	.658	.050	-1.928	.402	.050	-1.895	.409	.450	-.604	.664
.600	-.579	.669	.100	-1.769	.433	.100	-1.528	.481	.600	-.551	.675
.800	-.367	.711	.150	-1.078	.570	.150	-1.000	.586	.800	-.341	.716
.950	.023	.788	.200	-1.049	.576	.200	-.988	.588			
			.300	-.873	.611	.300	-.860	.613			
			.350	-.804	.625	.350	-.763	.633			
			.400	-.761	.633	.400	-.729	.639			
			.450	-.747	.636	.450	-.713	.642			
			.500	-.724	.640	.500	-.709	.643			
			.550	-.657	.646	.550	-.674	.650			
			.600	-.663	.652	.600	-.623	.660			
			.650	-.619	.661	.700	-.451	.694			
			.700	-.553	.674	.800	-.263	.731			
			.800	-.330	.718	.900	-.109	.762			
			.900	-.059	.772	.950	-.106	.763			
			.950	-.002	.783	.990	-.097	.764			
			.990	.013	.786						
					LOWER SURFACE						
.100	-.157	.752	.025	.300	.843	.025	.399	.863	.100	-.346	.715
.300	-.392	.706	.050	-.007	.782	.050	-.069	.770	.300	-.420	.700
.600	-.293	.726	.100	-.181	.748	.100	-.209	.742	.600	-.257	.725
.800	.247	.832	.200	-.346	.715	.200	-.335	.717	.800	.250	.833
			.300	-.400	.704	.300	-.410	.702			
			.400	-.428	.699	.400	-.458	.693			
			.500	-.468	.691	.500	-.411	.702			
			.600	-.212	.742	.600	-.247	.735			
			.700	.086	.801	.700	.034	.790			
			.800	.294	.842	.800	.300	.843			
			.900	.363	.855	.900	.336	.850			
			.950	.341	.851	.950	.339	.851			
			1.000	.017	.787						
CN=				.6138			.5879				
CM=				-.0890			-.0800				

(c) M = 0.60. Continued.

$\delta_a = 0^o$; $\alpha = 3.84^o$; $C_L = 0.684$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.245	.339	0.000	.876	.957	0.000	.084	.800	.050	-2.186	.351
.150	-1.013	.583	.012	-1.213	.543	.012	-1.403	.506	.150	-1.016	.582
.300	-.868	.612	.025	-1.831	.421	.025	-1.553	.476	.300	-.795	.626
.450	-.663	.652	.050	-2.225	.343	.050	-2.107	.366	.450	-.611	.663
.600	-.589	.667	.100	-2.285	.331	.100	-2.091	.370	.600	-.546	.675
.800	-.364	.711	.150	-1.309	.524	.150	-1.194	.547	.800	-.341	.716
.950	.021	.788	.200	-1.008	.584	.200	-.993	.587			
			.300	-.930	.599	.300	-.910	.603			
			.350	-.851	.615	.350	-.811	.623			
			.400	-.794	.626	.400	-.763	.632			
			.450	-.778	.629	.450	-.743	.636			
			.500	-.755	.634	.500	-.731	.639			
			.550	-.718	.641	.550	-.681	.649			
			.600	-.674	.650	.600	-.627	.659			
			.650	-.635	.658	.700	-.459	.693			
			.700	-.553	.674	.800	-.271	.730			
			.800	-.336	.717	.900	-.104	.763			
			.900	-.076	.768	.950	-.094	.765			
			.950	-.010	.781	.990	-.092	.765			
			.990	.018	.787						
					LOWER SURFACE						
.100	-.036	.776	.025	.457	.874	.025	.546	.892	.100	-.161	.752
.300	-.315	.721	.050	.144	.812	.050	.093	.802	.300	-.376	.709
.600	-.264	.731	.100	-.061	.771	.100	-.094	.765	.600	-.296	.727
.800	.274	.838	.200	-.229	.738	.200	-.206	.743	.800	.252	.833
			.300	-.329	.718	.300	-.332	.718			
			.400	-.374	.709	.400	-.403	.704			
			.500	-.417	.701	.500	-.371	.710			
			.600	-.182	.747	.600	-.220	.740			
			.700	.058	.803	.700	.044	.792			
			.800	.306	.844	.800	.302	.843			
			.900	.380	.859	.900	.339	.851			
			.950	.355	.854	.950	.346	.852			
			1.000	.038	.791						
CN=				.7398			.7112				
CM=				-.0865			-.0723				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = -4.31^o$; $C_L = -0.128$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.454	.717	0.000	1.041	.990	0.000	.067	.797	.050	-.280	.728
.150	-.443	.691	.012	.404	.863	.012	.347	.852	.150	-.427	.698
.300	-.436	.693	.025	-.001	.783	.025	.095	.802	.300	-.460	.692
.450	-.413	.700	.050	-.309	.722	.050	-.267	.730	.450	-.451	.694
.600	-.379	.688	.100	-.421	.700	.100	-.370	.710	.600	-.496	.685
.800	-.343	.704	.150	-.443	.695	.150	-.354	.713	.800	-.381	.708
.990	.043	.797	.200	-.449	.690	.200	-.442	.696			
			.300	-.488	.686	.300	-.481	.688			
			.350	-.495	.687	.350	-.466	.691			
			.400	-.476	.689	.400	-.455	.691			
			.450	-.470	.690	.450	-.502	.684			
			.500	-.530	.678	.500	-.536	.677			
			.550	-.555	.673	.550	-.541	.676			
			.600	-.512	.682	.600	-.555	.673			
			.650	-.561	.672	.700	-.467	.691			
			.700	-.533	.678	.800	-.293	.725			
			.800	-.362	.711	.900	-.081	.767			
			.900	-.082	.767	.950	-.056	.772			
			.950	.051	.793	.990	-.050	.773			
			.990	.106	.804						
					LOWER SURFACE						
.100	-.832	.606	.025	-.801	.625	.025	-.803	.624	.100	-1.268	.532
.300	-.734	.638	.050	-1.205	.544	.050	-1.380	.510	.300	-.676	.640
.600	-.633	.717	.100	-1.075	.570	.100	-1.163	.553	.600	-.282	.727
.800	.034	.802	.200	-.890	.607	.200	-.874	.610	.800	.140	.811
			.300	-.799	.625	.300	-.768	.631			
			.400	-.710	.642	.400	-.694	.646			
			.500	-.638	.657	.500	-.645	.675			
			.600	-.278	.728	.600	-.278	.728			
			.700	.030	.789	.700	.020	.787			
			.800	.148	.813	.800	.208	.825			
			.900	.233	.829	.900	.257	.834			
			.950	.261	.835	.950	.288	.840			
			1.000	.121	.807						
CN=				-.0586			-.0614				
CM=				-.1020			-.1161				

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = -2.92^o$; $C_L = 0.023$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.645	.657	0.000	1.082	.998	0.000	.073	.798	.050	-.531	.679
.150	-.530	.669	.012	.183	.870	.012	.146	.813	.150	-.525	.680
.300	-.554	.675	.025	-.244	.735	.025	-.156	.753	.300	-.529	.680
.450	-.477	.690	.050	-.535	.678	.050	-.527	.680	.450	-.491	.687
.600	-.519	.683	.100	-.567	.672	.100	-.520	.681	.600	-.529	.680
.800	-.435	.704	.150	-.577	.670	.150	-.515	.682	.800	-.401	.705
.990	.053	.769	.200	-.600	.665	.200	-.546	.676			
			.300	-.570	.671	.300	-.563	.673			
			.350	-.576	.670	.350	-.538	.678			
			.400	-.548	.676	.400	-.529	.679			
			.450	-.528	.680	.450	-.553	.675			
			.500	-.591	.667	.500	-.585	.669			
			.550	-.590	.667	.550	-.579	.670			
			.600	-.562	.673	.600	-.578	.670			
			.650	-.592	.667	.700	-.476	.690			
			.700	-.544	.677	.800	-.298	.725			
			.800	-.384	.708	.900	-.096	.765			
			.900	-.078	.769	.950	-.078	.769			
			.950	.031	.790	.990	-.075	.769			
			.990	.037	.803						
					LOWER SURFACE						
.100	-.701	.646	.025	-.548	.676	.025	-.453	.695	.100	-.991	.588
.300	-.658	.652	.050	-.568	.593	.050	-.576	.591	.300	-.625	.661
.600	-.310	.723	.100	-.887	.609	.100	-.900	.606	.600	-.290	.727
.800	.125	.809	.200	-.780	.630	.200	-.729	.640	.800	.200	.824
			.300	-.705	.645	.300	-.685	.649			
			.400	-.650	.656	.400	-.642	.657			
			.500	-.609	.664	.500	-.519	.681			
			.600	-.275	.730	.600	-.275	.730			
			.700	.033	.791	.700	.030	.790			
			.800	.199	.821	.800	.260	.835			
			.900	.284	.840	.900	.298	.843			
			.950	.300	.843	.950	.302	.844			
			1.000	.199	.806						
CN=				.0807			.0944				
CM=				-.1069			-.1137				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = -1.52^o$; $C_L = 0.172$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.914	.603	0.000	1.079	.997	0.000	.075	.759	.050	-.831	.620
.150	-.717	.642	.012	-.091	.766	.012	-.159	.752	.150	-.659	.654
.300	-.545	.656	.025	-.582	.669	.025	-.453	.654	.300	-.507	.664
.450	-.524	.680	.050	-.847	.616	.050	-.805	.625	.450	-.533	.679
.600	-.542	.677	.100	-.770	.632	.100	-.730	.640	.600	-.547	.676
.800	-.416	.702	.150	-.721	.641	.150	-.655	.654	.800	-.405	.704
.990	.057	.795	.200	-.704	.645	.200	-.677	.650			
			.300	-.661	.653	.300	-.660	.653			
			.350	-.635	.658	.350	-.619	.661			
			.400	-.612	.663	.400	-.594	.666			
			.450	-.590	.667	.450	-.608	.664			
			.500	-.639	.657	.500	-.632	.659			
			.550	-.632	.659	.550	-.617	.662			
			.600	-.606	.664	.600	-.608	.664			
			.650	-.606	.664	.700	-.488	.687			
			.700	-.570	.671	.800	-.294	.726			
			.800	-.378	.709	.900	-.119	.760			
			.900	-.081	.768	.950	-.100	.764			
			.950	.022	.788	.990	-.095	.765			
			.990	.081	.800						
					LOWER SURFACE						
.100	-.532	.677	.025	-.291	.726	.025	-.216	.741	.100	-.804	.625
.300	-.589	.668	.050	-.655	.654	.050	-.693	.647	.300	-.568	.672
.600	-.318	.721	.100	-.650	.655	.100	-.684	.649	.600	-.288	.727
.800	.170	.917	.200	-.638	.658	.200	-.635	.658	.800	.233	.830
			.300	-.624	.660	.300	-.616	.662			
			.400	-.586	.668	.400	-.593	.667			
			.500	-.550	.673	.500	-.491	.687			
			.600	-.267	.731	.600	-.263	.732			
			.700	.055	.795	.700	.050	.754			
			.800	.225	.828	.800	.294	.842			
			.900	.316	.846	.900	.326	.848			
			.950	.313	.846	.950	.321	.847			
			1.000	.088	.801						
CN=				.2332			.2409				
CM=				-.1065			-.1126				

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = -0.18^o$; $C_L = 0.308$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.192	.550	0.000	1.076	.997	0.000	.079	.799	.050	-1.104	.566
.150	-.864	.613	.012	-.413	.702	.012	-.457	.693	.150	-.785	.629
.300	-.697	.646	.025	-.851	.616	.025	-.733	.639	.300	-.663	.653
.450	-.562	.673	.050	-1.140	.554	.050	-1.108	.565	.450	-.564	.672
.600	-.539	.673	.100	-1.003	.586	.100	-.927	.600	.600	-.560	.673
.800	-.408	.703	.150	-.878	.610	.150	-.775	.631	.800	-.396	.705
.990	.048	.793	.200	-.854	.615	.200	-.786	.628			
			.300	-.747	.636	.300	-.740	.638			
			.350	-.693	.647	.350	-.670	.651			
			.400	-.671	.651	.400	-.639	.657			
			.450	-.650	.655	.450	-.649	.655			
			.500	-.677	.650	.500	-.663	.653			
			.550	-.660	.653	.550	-.648	.656			
			.600	-.629	.659	.600	-.629	.659			
			.650	-.624	.660	.700	-.482	.688			
			.700	-.572	.671	.800	-.279	.729			
			.800	-.365	.712	.900	-.130	.758			
			.900	-.085	.767	.950	-.120	.760			
			.950	.020	.788	.990	-.120	.760			
			.990	.058	.795						
					LOWER SURFACE						
.100	-.370	.711	.025	-.069	.770	.025	.050	.794	.100	-.616	.662
.300	-.530	.679	.050	-.403	.704	.050	-.454	.694	.300	-.508	.683
.600	-.313	.722	.100	-.492	.688	.100	-.498	.685	.600	-.284	.728
.800	.193	.822	.200	-.517	.682	.200	-.519	.681	.800	.261	.835
			.300	-.552	.675	.300	-.542	.677			
			.400	-.524	.680	.400	-.533	.678			
			.500	-.535	.678	.500	-.493	.686			
			.600	-.249	.735	.600	-.250	.734			
			.700	.060	.796	.700	.060	.796			
			.800	.244	.833	.800	.312	.846			
			.900	.347	.852	.900	.337	.850			
			.950	.320	.847	.950	.334	.850			
			1.000	.063	.796						
CN=				.3672			.3733				
CM=				-.1032			-.1076				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = 1.15^o$; $C_L = 0.439$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.536	.670	0.000	1.041	.590	0.000	.080	.800	.050	-1.531	.681
.150	-.387	.589	.012	-.727	.640	.012	-.788	.628	.150	-.893	.607
.300	-.749	.632	.025	-1.297	.527	.025	-1.032	.580	.300	-.728	.640
.450	-.610	.663	.050	-1.576	.472	.050	-1.532	.481	.450	-.599	.665
.600	-.574	.670	.100	-1.184	.550	.100	-1.127	.561	.600	-.574	.670
.800	-.337	.705	.150	-1.031	.580	.150	-.934	.599	.800	-.389	.707
.990	.027	.789	.200	-.974	.591	.200	-.812	.603			
			.300	-.870	.620	.300	-.805	.625			
			.350	-.770	.631	.350	-.736	.638			
			.400	-.721	.641	.400	-.701	.645			
			.450	-.718	.644	.450	-.699	.646			
			.500	-.703	.645	.500	-.699	.646			
			.550	-.692	.647	.550	-.670	.651			
			.600	-.649	.656	.600	-.641	.657			
			.650	-.632	.659	.700	-.480	.689			
			.700	-.574	.670	.800	-.265	.731			
			.800	-.370	.711	.900	-.138	.757			
			.900	-.077	.769	.950	-.138	.757			
			.950	.009	.786	.990	-.141	.756			
			.990	.024	.789						
					LOWER SURFACE						
.100	-.274	.730	.025	.117	.807	.025	.252	.834	.100	-.462	.692
.300	-.449	.695	.050	-.164	.751	.050	-.254	.734	.300	-.447	.695
.600	-.335	.726	.100	-.315	.721	.100	-.336	.717	.600	-.270	.730
.800	.214	.826	.200	-.413	.702	.200	-.414	.702	.800	.271	.837
			.300	-.453	.694	.300	-.462	.692			
			.400	-.472	.691	.400	-.486	.688			
			.500	-.494	.686	.500	-.413	.702			
			.600	-.222	.740	.600	-.228	.739			
			.700	.079	.800	.700	.070	.798			
			.800	.240	.839	.800	.324	.848			
			.900	.354	.854	.900	.340	.851			
			.950	.334	.850	.950	.339	.851			
			1.000	.046	.793						
CN=				.5071			.5060				
CM=				-.1007			-.1012				

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = 2.49^o$; $C_L = 0.563$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.959	.597	0.000	.959	.574	0.000	.092	.800	.050	-1.920	.605
.150	-1.095	.568	.012	-.970	.592	.012	-1.064	.574	.150	-.974	.591
.300	-.329	.620	.025	-1.557	.476	.025	-1.313	.524	.300	-.767	.632
.450	-.533	.658	.050	-1.583	.397	.050	-1.524	.404	.450	-.615	.662
.600	-.596	.668	.100	-1.745	.439	.100	-1.391	.509	.600	-.572	.671
.800	-.381	.709	.150	-1.101	.566	.150	-1.025	.581	.800	-.385	.708
.990	.029	.789	.200	-1.058	.575	.200	-1.001	.586			
			.300	-.990	.608	.300	-.874	.611			
			.350	-.892	.622	.350	-.791	.628			
			.400	-.765	.633	.400	-.741	.637			
			.450	-.759	.634	.450	-.724	.641			
			.500	-.746	.637	.500	-.718	.642			
			.550	-.712	.643	.550	-.681	.649			
			.600	-.659	.654	.600	-.641	.657			
			.650	-.636	.658	.700	-.457	.694			
			.700	-.554	.675	.800	-.248	.735			
			.800	-.342	.716	.900	-.157	.754			
			.900	-.090	.768	.950	-.149	.754			
			.950	-.018	.780	.990	-.150	.754			
			.990	.017	.787						
					LOWER SURFACE						
.100	-.130	.758	.025	.287	.841	.025	.409	.865	.100	-.311	.722
.300	-.391	.707	.050	-.015	.781	.050	-.046	.775	.300	-.395	.706
.600	-.233	.728	.100	-.173	.750	.100	-.181	.748	.600	-.263	.732
.800	.229	.829	.200	-.339	.723	.200	-.302	.724	.800	.278	.839
			.300	-.392	.706	.300	-.395	.706			
			.400	-.430	.699	.400	-.433	.698			
			.500	-.461	.693	.500	-.385	.708			
			.600	-.205	.744	.600	-.216	.741			
			.700	.088	.801	.700	.078	.799			
			.800	.276	.838	.800	.330	.849			
			.900	.354	.856	.900	.349	.853			
			.950	.337	.851	.950	.345	.852			
			1.000	.019	.784						
CN=				.6309			.6213				
CM=				-.0913			-.0922				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 3^o$; $\alpha = 3.84^o$; $C_L = 0.705$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.311	.328	0.000	.894	.961	0.000	.080	.800	.050	-2.246	.340
.150	-1.033	.580	.012	-1.226	.542	.012	-1.362	.515	.150	-.994	.588
.300	-.458	.613	.025	-1.858	.417	.025	-1.586	.471	.300	-.794	.627
.450	-.569	.652	.050	-2.235	.343	.050	-2.178	.354	.450	-.629	.660
.600	-.597	.666	.100	-2.376	.315	.100	-2.245	.341	.600	-.570	.671
.800	-.382	.709	.150	-1.311	.525	.150	-1.259	.535	.800	-.397	.706
.990	.029	.790	.200	-1.003	.586	.200	-.995	.588			
			.300	-.930	.600	.300	-.923	.602			
			.350	-.851	.616	.350	-.834	.619			
			.400	-.796	.627	.400	-.773	.631			
			.450	-.779	.630	.450	-.751	.636			
			.500	-.764	.633	.500	-.743	.637			
			.550	-.721	.642	.550	-.702	.645			
			.600	-.669	.652	.600	-.658	.654			
			.650	-.647	.656	.700	-.473	.691			
			.700	-.576	.670	.800	-.263	.732			
			.800	-.348	.715	.900	-.141	.756			
			.900	-.072	.770	.950	-.126	.759			
			.950	-.013	.781	.990	-.131	.758			
			.990	.010	.786						
					LOWER SURFACE						
.100	-.009	.782	.025	.440	.871	.025	.603	.903	.100	-.185	.747
.300	-.338	.723	.050	.144	.813	.050	.114	.807	.300	-.335	.718
.600	-.251	.734	.100	-.046	.775	.100	-.068	.771	.600	-.243	.736
.800	.257	.835	.200	-.211	.742	.200	-.213	.742	.800	.287	.841
			.300	-.309	.723	.300	-.319	.721			
			.400	-.357	.713	.400	-.376	.710			
			.500	-.410	.703	.500	-.337	.718			
			.600	-.178	.749	.600	-.194	.744			
			.700	.106	.805	.700	.092	.802			
			.800	.306	.845	.800	.346	.852			
			.900	.383	.860	.900	.364	.856			
			.950	.348	.853	.950	.364	.856			
			1.000	.035	.791						
CN=				.7594			.7649				
CM=				-.0880			-.0840				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = -4.28^o$; $C_L = -0.111$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.395	.703	0.000	1.046	.991	0.000	.070	.798	.050	-.298	.725
.150	-.432	.687	.012	.389	.861	.012	.336	.850	.150	-.416	.702
.300	-.443	.687	.025	-.046	.775	.025	.059	.796	.300	-.475	.690
.450	-.443	.698	.050	-.302	.724	.050	-.317	.721	.450	-.464	.692
.600	-.430	.697	.100	-.418	.702	.100	-.376	.710	.600	-.525	.680
.800	-.405	.704	.150	-.447	.696	.150	-.376	.710	.800	-.422	.701
.990	.065	.797	.200	-.495	.686	.200	-.438	.697			
			.300	-.497	.686	.300	-.501	.685			
			.350	-.495	.688	.350	-.481	.689			
			.400	-.497	.686	.400	-.480	.689			
			.450	-.476	.690	.450	-.505	.684			
			.500	-.553	.675	.500	-.543	.677			
			.550	-.566	.674	.550	-.550	.675			
			.600	-.579	.680	.600	-.559	.676			
			.650	-.565	.673	.700	-.461	.693			
			.700	-.536	.678	.800	-.227	.739			
			.800	-.383	.708	.900	-.155	.753			
			.900	-.089	.766	.950	-.153	.754			
			.950	.045	.793	.990	-.151	.754			
			.990	.109	.806						
					LOWER SURFACE						
.100	-.336	.621	.025	-.831	.620	.025	-.779	.630	.100	-1.266	.534
.300	-.718	.643	.050	-1.242	.539	.050	-1.335	.520	.300	-.656	.654
.600	-.329	.719	.100	-1.071	.572	.100	-1.091	.569	.600	-.233	.738
.800	.098	.803	.200	-.858	.614	.200	-.834	.619	.800	.175	.819
			.300	-.781	.630	.300	-.757	.634			
			.400	-.694	.647	.400	-.663	.653			
			.500	-.628	.660	.500	-.503	.685			
			.600	-.288	.727	.600	-.221	.740			
			.700	.028	.790	.700	.063	.794			
			.800	.167	.817	.800	.216	.827			
			.900	.247	.833	.900	.290	.839			
			.950	.278	.839	.950	.292	.842			
			1.000	.115	.807						
CN=				-.0373			-.0159				
CM=				-.1068			-.1258				

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = -2.86^o$; $C_L = 0.044$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.431	.659	0.000	1.074	.994	0.000	.072	.798	.050	-.575	.670
.150	-.475	.660	.012	.128	.809	.012	.086	.801	.150	-.544	.676
.300	-.533	.673	.025	-.276	.729	.025	-.188	.747	.300	-.541	.677
.450	-.493	.687	.050	-.562	.673	.050	-.557	.674	.450	-.510	.683
.600	-.520	.681	.100	-.595	.668	.100	-.565	.672	.600	-.556	.674
.800	-.413	.701	.150	-.587	.668	.150	-.525	.680	.800	-.439	.697
.990	.034	.797	.200	-.597	.666	.200	-.576	.670			
			.300	-.598	.668	.300	-.580	.669			
			.350	-.571	.671	.350	-.550	.675			
			.400	-.565	.672	.400	-.540	.677			
			.450	-.544	.676	.450	-.573	.671			
			.500	-.605	.664	.500	-.596	.666			
			.550	-.605	.664	.550	-.592	.667			
			.600	-.570	.671	.600	-.588	.668			
			.650	-.577	.670	.700	-.474	.690			
			.700	-.558	.674	.800	-.238	.737			
			.800	-.395	.706	.900	-.171	.750			
			.900	-.100	.764	.950	-.166	.751			
			.950	.026	.789	.990	-.169	.751			
			.990	.030	.802						
					LOWER SURFACE						
.100	-.435	.666	.025	-.551	.675	.025	-.452	.695	.100	-.961	.596
.300	-.651	.655	.050	-.937	.599	.050	-.958	.595	.300	-.601	.665
.600	-.315	.722	.100	-.870	.612	.100	-.850	.616	.600	-.239	.737
.800	.152	.814	.200	-.741	.637	.200	-.722	.641	.800	.244	.832
			.300	-.695	.647	.300	-.677	.650			
			.400	-.648	.656	.400	-.615	.662			
			.500	-.599	.666	.500	-.480	.689			
			.600	-.278	.729	.600	-.217	.741			
			.700	.041	.792	.700	.093	.802			
			.800	.206	.825	.800	.295	.842			
			.900	.307	.845	.900	.319	.847			
			.950	.324	.848	.950	.313	.846			
			1.000	.101	.804						
CN=				.1067			.1445				
CM=				-.1124			-.1277				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = -1.49^o$; $C_L = 0.189$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.909	.604	0.000	1.086	.598	0.000	.077	.799	.050	-.859	.614
.150	-.741	.638	.012	-.110	.762	.012	-.166	.751	.150	-.684	.660
.300	-.643	.657	.025	-.696	.664	.025	-.493	.687	.300	-.623	.661
.450	-.537	.678	.050	-.895	.607	.050	-.835	.619	.450	-.549	.676
.600	-.547	.676	.100	-.805	.625	.100	-.768	.632	.600	-.576	.670
.800	-.417	.702	.150	-.759	.634	.150	-.665	.653	.800	-.438	.697
.990	.052	.794	.200	-.717	.643	.200	-.684	.649			
			.300	-.669	.652	.300	-.672	.651			
			.350	-.626	.660	.350	-.625	.661			
			.400	-.622	.661	.400	-.604	.665			
			.450	-.601	.665	.450	-.620	.662			
			.500	-.642	.657	.500	-.639	.659			
			.550	-.650	.656	.550	-.623	.661			
			.600	-.604	.665	.600	-.612	.663			
			.650	-.613	.663	.700	-.481	.689			
			.700	-.586	.668	.800	-.243	.736			
			.800	-.392	.707	.900	-.185	.747			
			.900	-.090	.766	.950	-.182	.748			
			.950	.019	.788	.990	-.183	.748			
			.990	.066	.797						
					LOWER SURFACE						
.100	-.494	.686	.025	-.269	.731	.025	-.175	.749	.100	-.775	.631
.300	-.592	.669	.050	-.594	.668	.050	-.664	.653	.300	-.540	.677
.600	-.313	.722	.100	-.647	.656	.100	-.658	.654	.600	-.238	.737
.800	.177	.819	.200	-.633	.659	.200	-.613	.663	.900	.282	.840
			.300	-.615	.663	.300	-.594	.667			
			.400	-.587	.668	.400	-.567	.672			
			.500	-.570	.672	.500	-.448	.696			
			.600	-.261	.732	.600	-.207	.743			
			.700	.052	.794	.700	.112	.806			
			.800	.249	.833	.800	.330	.849			
			.900	.346	.852	.900	.338	.851			
			.950	.337	.851	.950	.319	.847			
			1.000	.086	.801						
CN=				.2547			.2872				
CM=				-.1121			-.1250				

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = -0.15^o$; $C_L = 0.322$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.225	.542	0.000	1.069	.595	0.000	.078	.799	.050	-1.159	.555
.150	-.871	.612	.012	-.417	.702	.012	-.481	.689	.150	-.814	.623
.300	-.706	.646	.025	-.949	.597	.025	-.750	.628	.300	-.672	.650
.450	-.570	.672	.050	-1.171	.553	.050	-1.175	.552	.450	-.575	.670
.600	-.547	.677	.100	-1.019	.583	.100	-.962	.594	.600	-.584	.668
.800	-.413	.702	.150	-.876	.611	.150	-.818	.622	.800	-.427	.700
.990	.047	.793	.200	-.829	.621	.200	-.801	.626			
			.300	-.765	.633	.300	-.759	.634			
			.350	-.715	.643	.350	-.693	.647			
			.400	-.691	.649	.400	-.660	.654			
			.450	-.669	.652	.450	-.666	.653			
			.500	-.681	.650	.500	-.679	.650			
			.550	-.679	.650	.550	-.658	.654			
			.600	-.666	.656	.600	-.633	.659			
			.650	-.633	.659	.700	-.478	.690			
			.700	-.593	.669	.800	-.238	.737			
			.800	-.389	.708	.900	-.190	.747			
			.900	-.092	.766	.950	-.189	.747			
			.950	.009	.786	.990	-.190	.746			
			.990	.052	.794						
					LOWER SURFACE						
.100	-.332	.707	.025	-.045	.775	.025	.065	.797	.100	-.592	.667
.300	-.515	.682	.050	-.369	.711	.050	-.475	.690	.300	-.468	.686
.600	-.307	.723	.100	-.474	.690	.100	-.475	.690	.600	-.231	.739
.800	.205	.824	.200	-.510	.683	.200	-.495	.686	.800	.316	.846
			.300	-.523	.681	.300	-.515	.682			
			.400	-.515	.682	.400	-.516	.682			
			.500	-.530	.679	.500	-.415	.702			
			.600	-.239	.737	.600	-.196	.745			
			.700	.069	.798	.700	.121	.808			
			.800	.264	.836	.800	.347	.853			
			.900	.360	.855	.900	.346	.852			
			.950	.376	.849	.950	.326	.848			
			1.000	.064	.797						
CN=				.3854			.4209				
CM=				-.1090			-.1190				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = 1.19^o$; $C_L = 0.452$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.643	.459	0.000	1.034	.888	0.000	.080	.800	.050	-1.588	.470
.150	-.585	.589	.012	-.698	.646	.012	-.787	.629	.150	-.890	.608
.300	-.797	.629	.025	-1.259	.527	.025	-1.105	.566	.300	-.739	.638
.450	-.627	.660	.050	-1.655	.457	.050	-1.569	.474	.450	-.610	.664
.600	-.534	.683	.100	-1.228	.541	.100	-1.171	.553	.600	-.597	.666
.800	-.399	.705	.150	-1.049	.577	.150	-.932	.600	.800	-.418	.701
.990	.033	.789	.200	-.955	.595	.200	-.922	.602			
			.300	-.818	.622	.300	-.821	.622			
			.350	-.781	.630	.350	-.746	.637			
			.400	-.745	.637	.400	-.709	.644			
			.450	-.719	.642	.450	-.704	.645			
			.500	-.720	.642	.500	-.708	.644			
			.550	-.703	.645	.550	-.676	.650			
			.600	-.661	.653	.600	-.643	.657			
			.650	-.651	.655	.700	-.466	.692			
			.700	-.589	.668	.800	-.235	.738			
			.800	-.374	.710	.900	-.193	.746			
			.900	-.095	.765	.950	-.197	.745			
			.950	-.003	.784	.990	-.198	.745			
			.990	.029	.790						
					LOWER SURFACE						
.100	-.758	.731	.025	.185	.817	.025	.272	.838	.100	-.440	.687
.300	-.437	.695	.050	-.166	.751	.050	-.228	.739	.300	-.434	.698
.600	-.233	.727	.100	-.290	.727	.100	-.313	.722	.600	-.221	.740
.800	.225	.829	.200	-.401	.705	.200	-.386	.708	.800	.324	.848
			.300	-.440	.693	.300	-.435	.698			
			.400	-.470	.691	.400	-.465	.692			
			.500	-.490	.687	.500	-.378	.709			
			.600	-.221	.740	.600	-.174	.750			
			.700	.076	.799	.700	.136	.811			
			.800	.283	.840	.800	.366	.856			
			.900	.366	.856	.900	.355	.854			
			.950	.340	.851	.950	.339	.851			
			1.000	.039	.792						
CN=				.5258			.5515				
CM=				-.1035			-.1128				

(c) M = 0.60. Continued.

$\delta_a = 6^o$; $\alpha = 2.50^o$; $C_L = 0.575$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.692	.397	0.000	.975	.877	0.000	.081	.800	.050	-1.987	.392
.150	-1.033	.563	.012	-1.006	.586	.012	-1.006	.568	.150	-.983	.590
.300	-.432	.629	.025	-1.622	.464	.025	-1.344	.519	.300	-.783	.630
.450	-.443	.657	.050	-1.986	.392	.050	-1.956	.398	.450	-.632	.659
.600	-.530	.669	.100	-1.873	.414	.100	-1.552	.478	.600	-.604	.665
.800	-.378	.709	.150	-1.087	.565	.150	-1.034	.580	.800	-.415	.702
.990	.017	.788	.200	-1.040	.575	.200	-1.013	.584			
			.300	-.891	.608	.300	-.888	.609			
			.350	-.826	.621	.350	-.802	.626			
			.400	-.771	.632	.400	-.750	.634			
			.450	-.753	.635	.450	-.735	.639			
			.500	-.738	.638	.500	-.729	.640			
			.550	-.712	.644	.550	-.687	.648			
			.600	-.671	.652	.600	-.646	.657			
			.650	-.643	.657	.700	-.451	.695			
			.700	-.574	.671	.800	-.232	.738			
			.800	-.348	.715	.900	-.196	.745			
			.900	-.073	.770	.950	-.199	.745			
			.950	-.022	.780	.990	-.199	.745			
			.990	.013	.787						
					LOWER SURFACE						
.100	-.123	.759	.025	.303	.844	.025	.443	.872	.100	-.304	.724
.300	-.373	.711	.050	.017	.788	.050	-.067	.771	.300	-.388	.708
.600	-.285	.733	.100	-.152	.754	.100	-.188	.747	.600	-.213	.742
.800	.251	.834	.200	-.294	.726	.200	-.294	.726	.800	.323	.849
			.300	-.390	.709	.300	-.362	.713			
			.400	-.417	.703	.400	-.404	.704			
			.500	-.463	.695	.500	-.344	.716			
			.600	-.207	.743	.600	-.160	.752			
			.700	.065	.801	.700	.146	.813			
			.800	.296	.843	.800	.378	.859			
			.900	.390	.859	.900	.363	.856			
			.950	.341	.851	.950	.346	.852			
			1.000	.022	.788						
CN=				.6524			.6715				
CM=				-.0929			-.1048				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(c) M = 0.60. Concluded.

$\delta_a = 6^o$; $\alpha = 3.89^o$; $C_L = 0.720$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.325	.325	0.000	.837	.560	0.000	.084	.801	.050	-2.275	.334
.150	-1.073	.572	.012	-1.268	.538	.012	-1.384	.509	.150	-1.085	.570
.300	-.870	.612	.025	-1.854	.418	.025	-1.604	.467	.300	-.815	.623
.450	-.665	.653	.050	-2.220	.346	.050	-2.157	.350	.450	-.644	.657
.600	-.599	.666	.100	-2.314	.327	.100	-2.275	.335	.600	-.604	.665
.800	-.377	.710	.150	-1.358	.516	.150	-1.234	.540	.800	-.445	.696
.990	.018	.788	.200	-1.014	.584	.200	-.594	.587			
			.300	-.574	.602	.300	-.929	.601			
			.350	-.865	.613	.350	-.845	.617			
			.400	-.805	.625	.400	-.790	.629			
			.450	-.796	.627	.450	-.770	.632			
			.500	-.781	.630	.500	-.754	.635			
			.550	-.735	.639	.550	-.711	.644			
			.600	-.692	.647	.600	-.669	.652			
			.650	-.646	.656	.700	-.466	.692			
			.700	-.578	.670	.800	-.236	.737			
			.800	-.352	.715	.900	-.134	.749			
			.900	-.088	.767	.950	-.188	.747			
			.950	-.003	.783	.990	-.184	.748			
			.990	.075	.789						
					LOWER SURFACE						
.100	.004	.785	.025	.443	.875	.025	.575	.858	.100	-.173	.750
.300	-.237	.725	.050	.174	.818	.050	.132	.810	.300	-.322	.720
.600	-.246	.735	.100	-.013	.781	.100	-.052	.774	.600	-.190	.746
.800	.270	.837	.200	-.200	.744	.200	-.186	.747	.900	.338	.851
			.300	-.295	.726	.300	-.296	.726			
			.400	-.347	.715	.400	-.349	.715			
			.500	-.407	.704	.500	-.295	.726			
			.600	-.157	.751	.600	-.135	.757			
			.700	.104	.805	.700	.165	.817			
			.800	.306	.845	.800	.393	.862			
			.900	.394	.862	.900	.378	.859			
			.950	.355	.854	.950	.362	.856			
			1.000	.031	.790						
CN=				.7740			.8094				
CM=				-.0900			-.0981				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(d) $M = 0.65$

$\delta_a = 0^o$; $\alpha = -4.45^o$; $C_L = -0.185$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.343	.675	0.000	1.063	.990	0.000	.087	.772	.050	-.269	.693
.150	-.474	.647	.012	.443	.651	.012	.417	.846	.150	-.405	.663
.300	-.473	.647	.025	.042	.762	.025	.140	.784	.300	-.466	.649
.450	-.461	.650	.050	-.270	.653	.050	-.265	.654	.450	-.458	.651
.600	-.485	.645	.100	-.356	.673	.100	-.328	.680	.600	-.493	.645
.800	-.379	.668	.150	-.447	.653	.150	-.354	.674	.800	-.320	.681
.950	.083	.771	.200	-.476	.647	.200	-.446	.653			
			.300	-.496	.642	.300	-.487	.644			
			.350	-.484	.645	.350	-.462	.650			
			.400	-.492	.643	.400	-.469	.648			
			.450	-.491	.643	.450	-.502	.641			
			.500	-.551	.630	.500	-.539	.633			
			.550	-.557	.629	.550	-.546	.631			
			.600	-.529	.635	.600	-.530	.635			
			.650	-.562	.627	.700	-.439	.655			
			.700	-.521	.637	.800	-.295	.687			
			.800	-.355	.674	.900	-.034	.745			
			.900	-.053	.741	.950	.035	.760			
			.950	.069	.768	.990	.054	.765			
			.990	.122	.780						
					LOWER SURFACE						
.100	-.961	.533	.025	-.815	.571	.025	-.748	.586	.100	-1.654	.384
.300	-.781	.579	.050	-1.469	.425	.050	-1.371	.447	.300	-.714	.594
.600	-.292	.688	.100	-1.374	.446	.100	-1.592	.398	.600	-.313	.683
.800	.039	.761	.200	-.955	.531	.200	-.915	.549	.800	.066	.767
			.300	-.883	.556	.300	-.849	.563			
			.400	-.759	.584	.400	-.762	.583			
			.500	-.656	.606	.500	-.612	.616			
			.600	-.269	.693	.600	-.314	.683			
			.700	.014	.756	.700	-.027	.747			
			.800	.120	.779	.800	.131	.782			
			.900	.201	.798	.900	.197	.797			
			.950	.243	.807	.950	.248	.808			
			1.000	.124	.780						
CN=				-.1435			-.1590				
CM=				-.1019			-.0967				

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = -2.95^o$; $C_L = -0.009$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.595	.620	0.000	1.083	.994	0.000	.080	.771	.050	-.545	.631
.150	-.614	.616	.012	.227	.803	.012	.183	.794	.150	-.532	.634
.300	-.566	.627	.025	-.204	.707	.025	-.109	.728	.300	-.539	.633
.450	-.519	.637	.050	-.567	.626	.050	-.547	.631	.450	-.487	.644
.600	-.518	.637	.100	-.562	.628	.100	-.542	.632	.600	-.510	.639
.800	-.385	.667	.150	-.604	.618	.150	-.501	.641	.800	-.330	.679
.950	.074	.769	.200	-.557	.620	.200	-.578	.624			
			.300	-.613	.616	.300	-.580	.624			
			.350	-.573	.625	.350	-.537	.633			
			.400	-.563	.627	.400	-.548	.631			
			.450	-.552	.630	.450	-.571	.626			
			.500	-.605	.618	.500	-.593	.621			
			.550	-.605	.618	.550	-.592	.621			
			.600	-.572	.625	.600	-.565	.627			
			.650	-.591	.621	.700	-.453	.652			
			.700	-.553	.630	.800	-.288	.689			
			.800	-.362	.672	.900	-.049	.742			
			.900	-.045	.743	.950	.008	.754			
			.950	.050	.764	.990	.023	.758			
			.990	.100	.775						
					LOWER SURFACE						
.100	-.737	.589	.025	-.504	.640	.025	-.488	.644	.100	-1.146	.498
.300	-.714	.594	.050	-1.005	.529	.050	-1.072	.514	.300	-.692	.599
.600	-.316	.682	.100	-.945	.542	.100	-1.056	.518	.600	-.345	.676
.800	.097	.774	.200	-.828	.568	.200	-.822	.573	.800	.122	.780
			.300	-.803	.574	.300	-.792	.576			
			.400	-.735	.596	.400	-.717	.593			
			.500	-.642	.610	.500	-.589	.622			
			.600	-.286	.689	.600	-.327	.680			
			.700	.030	.759	.700	-.018	.749			
			.800	.154	.787	.800	.184	.794			
			.900	.257	.810	.900	.239	.806			
			.950	.286	.816	.950	.277	.814			
			1.000	.110	.777						
CN=				.0425			.0116				
CM=				-.0957			-.0934				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = -2.26^o$; $C_L = 0.066$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.756	.584	0.000	1.030	.996	0.000	.089	.773	.050	-.691	.599
.150	-.682	.601	.012	.116	.779	.012	.074	.769	.150	-.591	.621
.300	-.603	.613	.025	-.331	.679	.025	-.257	.696	.300	-.576	.625
.450	-.545	.632	.050	-.705	.546	.050	-.624	.614	.450	-.520	.637
.600	-.531	.635	.100	-.667	.604	.100	-.611	.617	.600	-.524	.636
.800	-.389	.666	.150	-.678	.602	.150	-.587	.622	.800	-.337	.678
.950	.054	.765	.200	-.695	.598	.200	-.630	.613			
			.300	-.637	.611	.300	-.636	.611			
			.350	-.627	.613	.350	-.571	.626			
			.400	-.606	.618	.400	-.565	.627			
			.450	-.601	.619	.450	-.590	.621			
			.500	-.632	.612	.500	-.617	.615			
			.550	-.627	.613	.550	-.612	.617			
			.600	-.595	.622	.600	-.577	.624			
			.650	-.598	.620	.700	-.458	.651			
			.700	-.562	.628	.800	-.302	.686			
			.800	-.353	.674	.900	-.049	.742			
			.900	-.051	.741	.950	.001	.753			
			.950	.039	.761	.990	.021	.758			
			.990	.030	.771						
					LOWER SURFACE						
.100	-.593	.621	.025	-.425	.658	.025	-.315	.683	.100	-1.053	.518
.300	-.673	.603	.050	-.839	.566	.050	-.487	.555	.300	-.661	.606
.600	-.315	.683	.100	-.865	.560	.100	-.435	.567	.600	-.347	.676
.800	.123	.780	.200	-.777	.580	.200	-.766	.582	.800	.163	.789
			.300	-.758	.584	.300	-.734	.589			
			.400	-.670	.604	.400	-.693	.599			
			.500	-.634	.612	.500	-.576	.625			
			.600	-.266	.694	.600	-.319	.682			
			.700	.043	.767	.700	-.011	.750			
			.800	.175	.792	.800	.215	.801			
			.900	.274	.814	.900	.267	.812			
			.950	.290	.817	.950	.294	.814			
			1.000	.099	.773						
CN=				.1146				.0964			
CM=				-.1015				-.0930			

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = -1.54^o$; $C_L = 0.144$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.841	.565	0.000	1.041	.996	0.000	.091	.773	.050	-.869	.559
.150	-.766	.582	.012	-.067	.738	.012	-.085	.733	.150	-.674	.602
.300	-.664	.604	.025	-.511	.639	.025	-.400	.663	.300	-.619	.614
.450	-.561	.627	.050	-.862	.560	.050	-.745	.587	.450	-.530	.634
.600	-.544	.631	.100	-.799	.577	.100	-.705	.595	.600	-.534	.633
.800	-.376	.669	.150	-.745	.586	.150	-.650	.607	.800	-.344	.676
.950	.063	.766	.200	-.778	.579	.200	-.713	.593			
			.300	-.696	.597	.300	-.656	.606			
			.350	-.658	.606	.350	-.617	.615			
			.400	-.639	.610	.400	-.603	.618			
			.450	-.634	.611	.450	-.613	.616			
			.500	-.662	.605	.500	-.646	.608			
			.550	-.653	.607	.550	-.643	.609			
			.600	-.608	.617	.600	-.598	.619			
			.650	-.611	.616	.700	-.458	.650			
			.700	-.564	.627	.800	-.294	.687			
			.900	-.354	.674	.900	-.053	.741			
			.900	-.055	.740	.950	-.003	.750			
			.950	.037	.761	.990	.007	.753			
			.990	.072	.769						
					LOWER SURFACE						
.100	-.546	.631	.025	-.242	.690	.025	-.186	.711	.100	-.518	.548
.300	-.634	.611	.050	-.637	.593	.050	-.759	.583	.300	-.635	.611
.600	-.308	.684	.100	-.725	.591	.100	-.754	.584	.600	-.365	.671
.800	.132	.782	.200	-.709	.594	.200	-.702	.596	.800	.190	.795
			.300	-.700	.596	.300	-.696	.597			
			.400	-.658	.606	.400	-.672	.603			
			.500	-.619	.614	.500	-.557	.628			
			.600	-.266	.693	.600	-.323	.680			
			.700	.045	.762	.700	-.104	.751			
			.800	.197	.796	.800	.234	.805			
			.900	.295	.818	.900	.283	.816			
			.950	.310	.822	.950	.312	.822			
			1.000	.087	.772						
CN=				.1951				.1677			
CM=				-.1007				-.0929			

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = -0.82^o$; $C_L = 0.221$

STATION .1542			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.499	.530	0.000	1.035	.995	0.000	.091	.773	.050	-1.016	.526
.150	-.838	.546	.012	-.122	.726	.012	-.236	.700	.150	-.741	.588
.300	-.685	.609	.025	-.661	.601	.025	-.508	.639	.300	-.658	.606
.450	-.597	.620	.050	-1.031	.523	.050	-.963	.538	.450	-.552	.630
.600	-.554	.629	.100	-.919	.548	.100	-.828	.563	.600	-.537	.633
.800	-.372	.670	.150	-.827	.568	.150	-.752	.585	.800	-.348	.675
.950	.044	.763	.200	-.331	.567	.200	-.773	.580			
			.300	-.746	.586	.300	-.727	.591			
			.350	-.634	.598	.350	-.670	.603			
			.400	-.673	.603	.400	-.634	.611			
			.450	-.662	.605	.450	-.647	.609			
			.500	-.681	.601	.500	-.663	.605			
			.550	-.671	.603	.550	-.641	.610			
			.600	-.626	.613	.600	-.607	.618			
			.650	-.625	.613	.700	-.460	.650			
			.700	-.559	.625	.800	-.282	.690			
			.800	-.347	.675	.900	-.062	.739			
			.900	-.057	.740	.950	-.029	.746			
			.950	.031	.760	.990	-.014	.750			
			.990	.057	.765						
					LOWER SURFACE						
.100	-.404	.662	.025	-.165	.716	.025	-.051	.741	.100	-.811	.572
.300	-.595	.620	.050	-.563	.627	.050	-.648	.608	.300	-.600	.619
.600	-.306	.685	.100	-.590	.621	.100	-.640	.610	.600	-.358	.673
.800	.157	.739	.200	-.635	.611	.200	-.629	.613	.800	.227	.803
			.300	-.653	.606	.300	-.650	.608			
			.400	-.618	.615	.400	-.641	.610			
			.500	-.603	.618	.500	-.538	.633			
			.600	-.273	.692	.600	-.318	.682			
			.700	.053	.764	.700	.000	.753			
			.800	.229	.803	.800	.242	.807			
			.900	.319	.824	.900	.301	.820			
			.950	.325	.825	.950	.316	.823			
			1.000	.074	.769						
CN=				.2806			.2472				
CM=				-.1008			-.0896				

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = -0.15^o$; $C_L = 0.289$

STATION .1542			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.234	.477	0.000	1.055	.997	0.000	.081	.771	.050	-1.209	.484
.150	-.847	.555	.012	-.263	.694	.012	-.382	.668	.150	-.840	.566
.300	-.727	.581	.025	-.814	.570	.025	-.671	.603	.300	-.689	.599
.450	-.600	.611	.050	-1.165	.492	.050	-1.117	.504	.450	-.566	.627
.600	-.564	.627	.100	-1.054	.517	.100	-.949	.541	.600	-.547	.631
.800	-.371	.670	.150	-.906	.551	.150	-.799	.575	.800	-.342	.677
.950	.040	.762	.200	-.874	.558	.200	-.815	.571			
			.300	-.740	.579	.300	-.769	.582			
			.350	-.736	.589	.350	-.698	.597			
			.400	-.696	.598	.400	-.672	.603			
			.450	-.685	.600	.450	-.663	.605			
			.500	-.703	.596	.500	-.680	.601			
			.550	-.690	.601	.550	-.653	.607			
			.600	-.617	.611	.600	-.619	.617			
			.650	-.624	.614	.700	-.457	.651			
			.700	-.593	.620	.800	-.278	.691			
			.800	-.343	.676	.900	-.064	.738			
			.900	-.055	.740	.950	-.038	.744			
			.950	.018	.757	.990	-.025	.747			
			.990	.044	.763						
					LOWER SURFACE						
.100	-.348	.675	.025	-.055	.740	.025	.055	.765	.100	-.688	.600
.300	-.559	.623	.050	-.405	.663	.050	-.544	.632	.300	-.576	.624
.600	-.314	.683	.100	-.545	.631	.100	-.559	.629	.600	-.360	.673
.800	.172	.731	.200	-.513	.625	.200	-.572	.625	.800	.229	.804
			.300	-.521	.614	.300	-.604	.618			
			.400	-.586	.622	.400	-.618	.615			
			.500	-.592	.621	.500	-.526	.636			
			.600	-.254	.695	.600	-.301	.686			
			.700	.096	.765	.700	.000	.753			
			.800	.236	.805	.800	.255	.809			
			.900	.331	.828	.900	.300	.820			
			.950	.331	.826	.950	.316	.823			
			1.000	.069	.768						
CN=				.3381			.3109				
CM=				-.0959			-.0870				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = 0.55^o$; $C_L = 0.358$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.340	.454	0.000	1.076	.552	0.000	.094	.774	.050	-1.315	.460
.150	-.961	.539	.012	-.407	.662	.012	-.497	.642	.150	-.784	.579
.300	-.772	.581	.025	-.928	.546	.025	-.802	.574	.300	-.707	.595
.450	-.629	.613	.050	-1.353	.452	.050	-1.292	.465	.450	-.585	.623
.600	-.573	.625	.100	-1.356	.451	.100	-1.101	.508	.600	-.551	.630
.800	-.376	.669	.150	-.969	.537	.150	-.878	.557	.800	-.344	.676
.950	.036	.761	.200	-.961	.539	.200	-.888	.555			
			.300	-.817	.571	.300	-.824	.569			
			.350	-.773	.581	.350	-.730	.590			
			.400	-.721	.592	.400	-.698	.597			
			.450	-.707	.595	.450	-.689	.599			
			.500	-.722	.592	.500	-.697	.598			
			.550	-.690	.599	.550	-.662	.605			
			.600	-.657	.606	.600	-.615	.616			
			.650	-.619	.615	.700	-.449	.653			
			.700	-.595	.629	.800	-.277	.691			
			.800	-.331	.679	.900	-.081	.735			
			.900	-.056	.740	.950	-.053	.741			
			.950	.014	.756	.990	-.036	.745			
			.990	.045	.763						
					LOWER SURFACE						
.100	-.268	.653	.025	.017	.757	.025	.175	.792	.100	-.628	.613
.300	-.513	.639	.050	-.310	.684	.050	-.385	.667	.300	-.551	.630
.600	-.292	.688	.100	-.449	.653	.100	-.443	.653	.600	-.361	.672
.800	.178	.793	.200	-.507	.640	.200	-.511	.639	.900	.240	.806
			.300	-.581	.623	.300	-.566	.627			
			.400	-.560	.628	.400	-.587	.622			
			.500	-.569	.626	.500	-.506	.640			
			.600	-.260	.695	.600	-.290	.688			
			.700	.061	.766	.700	-.003	.752			
			.800	.245	.807	.800	.261	.811			
			.900	.344	.829	.900	.315	.823			
			.950	.319	.824	.950	.334	.827			
			1.000	.048	.763						
CN=				.4127			.3878				
CM=				-.0943			-.0847				

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = 1.25^o$; $C_L = 0.428$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.531	.412	0.000	1.057	.588	0.000	.091	.773	.050	-1.521	.414
.150	-.961	.539	.012	-.594	.620	.012	-.658	.606	.150	-.712	.594
.300	-.788	.577	.025	-1.083	.512	.025	-.886	.555	.300	-.738	.588
.450	-.638	.611	.050	-1.485	.422	.050	-1.440	.432	.450	-.601	.619
.600	-.577	.624	.100	-1.652	.385	.100	-1.438	.432	.600	-.552	.630
.800	-.355	.674	.150	-.917	.548	.150	-.888	.555	.800	-.332	.679
.950	.032	.760	.200	-.983	.533	.200	-.918	.548			
			.300	-.853	.563	.300	-.845	.565			
			.350	-.776	.580	.350	-.753	.585			
			.400	-.749	.586	.400	-.713	.594			
			.450	-.733	.589	.450	-.704	.596			
			.500	-.735	.589	.500	-.706	.595			
			.550	-.698	.597	.550	-.674	.603			
			.600	-.663	.605	.600	-.616	.616			
			.650	-.629	.613	.700	-.443	.654			
			.700	-.561	.628	.800	-.264	.694			
			.800	-.330	.679	.900	-.084	.734			
			.900	-.058	.740	.950	-.066	.738			
			.950	.008	.755	.990	-.055	.740			
			.990	.028	.759						
					LOWER SURFACE						
.100	-.191	.710	.025	.118	.779	.025	.209	.799	.100	-.506	.640
.300	-.481	.646	.050	-.190	.710	.050	-.299	.686	.300	-.514	.638
.600	-.288	.689	.100	-.363	.677	.100	-.341	.668	.600	-.348	.675
.800	.191	.795	.200	-.452	.652	.200	-.453	.652	.800	.244	.807
			.300	-.534	.634	.300	-.533	.634			
			.400	-.531	.634	.400	-.556	.629			
			.500	-.549	.630	.500	-.495	.642			
			.600	-.248	.698	.600	-.288	.689			
			.700	.069	.769	.700	.000	.753			
			.800	.257	.810	.800	.265	.812			
			.900	.349	.830	.900	.317	.823			
			.950	.336	.827	.950	.329	.826			
			1.000	.043	.762						
CN=				.4787			.4457				
CM=				-.0931			-.0797				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = 2.77^o$; $C_L = 0.612$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.764	.460	0.000	.993	.574	0.000	.083	.771	.050	-1.817	.348
.150	-1.323	.547	.012	-.796	.575	.012	-.917	.548	.150	-1.637	.388
.300	-.814	.571	.025	-1.376	.446	.025	-1.129	.501	.300	-.742	.588
.450	-.674	.603	.050	-1.755	.362	.050	-1.686	.377	.450	-.612	.616
.600	-.597	.620	.100	-1.954	.317	.100	-1.921	.325	.600	-.542	.632
.800	-.364	.672	.150	-1.879	.334	.150	-1.772	.358	.800	-.339	.677
.950	.043	.762	.200	-1.882	.334	.200	-1.181	.490			
			.300	-.749	.579	.300	-.810	.572			
			.350	-.781	.575	.350	-.762	.583			
			.400	-.759	.584	.400	-.735	.589			
			.450	-.750	.583	.450	-.730	.590			
			.500	-.748	.586	.500	-.730	.590			
			.550	-.721	.592	.550	-.703	.596			
			.600	-.679	.602	.600	-.634	.611			
			.650	-.651	.608	.700	-.476	.647			
			.700	-.589	.621	.800	-.300	.686			
			.800	-.359	.673	.900	-.079	.735			
			.900	-.067	.738	.950	-.018	.749			
			.950	.022	.758	.990	-.030	.746			
			.990	.069	.768						
					LOWER SURFACE						
.100	-.127	.725	.025	.314	.823	.025	.438	.850	.100	-.329	.679
.300	-.338	.665	.050	-.007	.751	.050	-.070	.737	.300	-.446	.653
.600	-.272	.652	.100	-.174	.714	.100	-.217	.704	.600	-.323	.681
.800	.221	.802	.200	-.329	.681	.200	-.334	.678	.800	.249	.804
			.300	-.405	.662	.300	-.423	.658			
			.400	-.433	.655	.400	-.472	.648			
			.500	-.479	.646	.500	-.433	.656			
			.600	-.195	.709	.600	-.269	.693			
			.700	.054	.774	.700	.028	.759			
			.800	.305	.821	.800	.295	.818			
			.900	.391	.840	.900	.346	.830			
			.950	.354	.834	.950	.348	.830			
			1.000	.069	.768						
CN=				.7214			.6383				
CM=				-.0895			-.0723				

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = 4.25^o$; $C_L = 0.783$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.046	.288	0.000	.929	.960	0.000	.089	.773	.050	-2.009	.305
.150	-2.044	.297	.012	-1.013	.527	.012	-1.191	.487	.150	-1.974	.313
.300	-.816	.571	.025	-1.598	.337	.025	-1.354	.451	.300	-.778	.579
.450	-.660	.606	.050	-1.925	.324	.050	-1.878	.334	.450	-.601	.619
.600	-.590	.621	.100	-2.131	.278	.100	-2.085	.288	.600	-.525	.636
.800	-.358	.673	.150	-2.058	.294	.150	-2.029	.301	.800	-.360	.673
.950	.056	.765	.200	-2.045	.297	.200	-1.967	.315			
			.300	-1.233	.478	.300	-.986	.533			
			.350	-.844	.565	.350	-.702	.596			
			.400	-.651	.608	.400	-.636	.611			
			.450	-.651	.608	.450	-.693	.598			
			.500	-.696	.598	.500	-.710	.595			
			.550	-.697	.598	.550	-.683	.601			
			.600	-.654	.607	.600	-.640	.610			
			.650	-.646	.609	.700	-.489	.644			
			.700	-.578	.624	.800	-.333	.679			
			.800	-.353	.673	.900	-.087	.733			
			.900	-.090	.733	.950	-.004	.752			
			.950	.021	.758	.990	.017	.756			
			.990	.069	.773						
					LOWER SURFACE						
.100	.013	.755	.025	.463	.856	.025	.616	.890	.100	-.131	.712
.300	-.308	.684	.050	.155	.787	.050	.091	.773	.300	-.380	.668
.600	-.247	.698	.100	-.027	.747	.100	-.038	.744	.600	-.308	.684
.800	.269	.813	.200	-.210	.706	.200	-.227	.702	.800	.257	.810
			.300	-.325	.680	.300	-.336	.678			
			.400	-.379	.668	.400	-.418	.660			
			.500	-.422	.659	.500	-.386	.667			
			.600	-.169	.715	.600	-.231	.701			
			.700	.124	.780	.700	.044	.763			
			.800	.333	.824	.800	.315	.823			
			.900	.412	.845	.900	.369	.835			
			.950	.386	.839	.950	.336	.839			
			1.000	.072	.773						
CN=				.9933			.8078				
CM=				-.0976			-.0671				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\delta_a = 0^o$; $\alpha = 5.60^o$; $C_L = 0.903$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.234	.257	0.000	.861	.545	0.000	.099	.775	.050	-2.152	.275
.150	-2.242	.255	.012	-1.169	.493	.012	-1.371	.448	.150	-2.128	.280
.300	-1.167	.494	.025	-1.781	.357	.025	-1.690	.377	.300	-.953	.541
.450	-.623	.615	.050	-2.081	.291	.050	-2.041	.300	.450	-.610	.618
.600	-.556	.630	.100	-2.279	.247	.100	-2.204	.263	.600	-.532	.635
.800	-.333	.679	.150	-2.213	.261	.150	-2.201	.264	.800	-.367	.677
.950	.046	.763	.200	-2.211	.262	.200	-2.105	.285			
			.300	-1.490	.422	.300	-1.350	.453			
			.350	-1.278	.469	.350	-1.044	.521			
			.400	-.906	.552	.400	-.703	.597			
			.450	-.643	.610	.450	-.606	.619			
			.500	-.597	.620	.500	-.631	.613			
			.550	-.592	.622	.550	-.631	.613			
			.600	-.557	.629	.600	-.575	.625			
			.650	-.534	.634	.700	-.439	.656			
			.700	-.501	.642	.800	-.304	.686			
			.800	-.305	.684	.900	-.096	.732			
			.900	-.087	.734	.950	-.025	.748			
			.950	.002	.754	.990	-.010	.751			
			.990	.054	.765						
					LOWER SURFACE						
.100	.109	.778	.025	.577	.882	.025	.696	.908	.100	-.086	.734
.300	-.249	.698	.050	.301	.820	.050	.250	.809	.300	-.321	.682
.600	-.230	.702	.100	.084	.772	.100	.042	.763	.600	-.294	.688
.800	.280	.815	.200	-.127	.725	.200	-.133	.724	.800	.255	.812
			.300	-.259	.696	.300	-.273	.693			
			.400	-.316	.683	.400	-.361	.673			
			.500	-.388	.667	.500	-.343	.677			
			.600	-.156	.719	.600	-.214	.706			
			.700	.123	.782	.700	.052	.765			
			.800	.337	.828	.800	.325	.825			
			.900	.417	.846	.900	.375	.837			
			.950	.343	.839	.950	.393	.841			
			1.000	.046	.763						
CN=				.9645			.9703				
CM=				-.0772			-.0596				

(d) M = 0.65. Concluded.

$\delta_a = 0^o$; $\alpha = 6.05^o$; $C_L = 0.934$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.262	.249	0.000	.830	.538	0.000	.090	.773	.050	-2.157	.263
.150	-2.286	.243	.012	-1.259	.472	.012	-1.419	.437	.150	-2.173	.269
.300	-1.253	.474	.025	-1.818	.348	.025	-1.724	.369	.300	-.994	.531
.450	-.613	.616	.050	-2.137	.277	.050	-2.076	.290	.450	-.625	.613
.600	-.528	.635	.100	-2.305	.239	.100	-2.235	.255	.600	-.542	.632
.800	-.309	.684	.150	-2.248	.252	.150	-2.231	.256	.800	-.354	.674
.950	.029	.759	.200	-2.238	.254	.200	-2.180	.267			
			.300	-1.504	.418	.300	-1.424	.436			
			.350	-1.409	.439	.350	-1.237	.477			
			.400	-1.067	.515	.400	-.783	.578			
			.450	-.759	.584	.450	-.606	.618			
			.500	-.626	.613	.500	-.595	.620			
			.550	-.554	.629	.550	-.589	.622			
			.600	-.536	.633	.600	-.556	.629			
			.650	-.496	.642	.700	-.417	.661			
			.700	-.443	.654	.800	-.290	.688			
			.800	-.273	.692	.900	-.093	.732			
			.900	-.098	.731	.950	-.051	.741			
			.950	-.016	.749	.990	-.001	.753			
			.990	.003	.753						
					LOWER SURFACE						
.100	.154	.787	.025	.608	.888	.025	.731	.915	.100	-.049	.742
.300	-.237	.700	.050	.335	.827	.050	.292	.818	.300	-.306	.684
.600	-.224	.703	.100	.103	.776	.100	.064	.767	.600	-.288	.688
.800	.277	.814	.200	-.094	.732	.200	-.101	.730	.300	.263	.811
			.300	-.237	.700	.300	-.251	.697			
			.400	-.301	.686	.400	-.347	.675			
			.500	-.378	.669	.500	-.344	.676			
			.600	-.149	.719	.600	-.211	.706			
			.700	.127	.781	.700	.057	.765			
			.800	.327	.826	.800	.326	.825			
			.900	.416	.845	.900	.375	.936			
			.950	.373	.836	.950	.383	.838			
			1.000	.015	.756						
CN=				.9949			.9533				
CM=				-.0741			-.0561				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70

$\delta_a = -6^o$; $\alpha = -4.80^o$; $C_L = -0.256$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.291	.643	0.000	1.033	.526	0.000	.079	.740	.050	-.194	.672
.150	-.493	.634	.012	.444	.843	.012	.462	.835	.150	-.396	.622
.300	-.474	.603	.025	.131	.753	.025	.181	.765	.300	-.483	.601
.450	-.431	.626	.050	-.228	.664	.050	-.205	.670	.450	-.457	.607
.600	-.502	.596	.100	-.364	.630	.100	-.304	.645	.600	-.448	.609
.800	-.407	.621	.150	-.437	.612	.150	-.340	.635	.800	-.221	.666
.950	.046	.741	.200	-.476	.602	.200	-.427	.614			
			.300	-.457	.557	.300	-.482	.601			
			.350	-.433	.593	.350	-.465	.605			
			.400	-.417	.600	.400	-.460	.604			
			.450	-.478	.602	.450	-.500	.597			
			.500	-.574	.578	.500	-.529	.589			
			.550	-.545	.575	.550	-.516	.593			
			.600	-.513	.593	.600	-.496	.597			
			.650	-.577	.577	.700	-.295	.647			
			.700	-.554	.583	.800	-.214	.667			
			.800	-.354	.633	.900	-.045	.709			
			.900	-.054	.707	.950	.062	.735			
			.950	.061	.735	.990	.146	.756			
			.990	.119	.750						
					LOWER SURFACE						
.100	-1.261	.401	.025	-.692	.549	.025	-.611	.569	.100	-1.622	.318
.300	-.782	.532	.050	-1.312	.395	.050	-1.240	.413	.300	-.851	.509
.600	-.285	.650	.100	-1.421	.368	.100	-1.481	.353	.600	-.410	.619
.800	.041	.740	.200	-1.444	.362	.200	-1.535	.340	.800	-.002	.720
			.300	-1.427	.357	.300	-1.501	.348			
			.400	-.534	.563	.400	-.709	.545			
			.500	-.578	.552	.500	-.599	.572			
			.600	-.297	.647	.600	-.402	.621			
			.700	.043	.731	.700	-.104	.694			
			.800	.204	.771	.800	.145	.756			
			.900	.305	.797	.900	.235	.779			
			.950	.327	.796	.950	.283	.791			
			1.000	.133	.753						
CN=				-.2144			-.3099				
CM=				-.1213			-.0779				

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = -3.28^o$; $C_L = -0.102$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.526	.549	0.000	1.101	.553	0.000	.092	.741	.050	-.423	.616
.150	-.597	.576	.012	.331	.805	.012	.269	.787	.150	-.534	.588
.300	-.583	.576	.025	-.055	.657	.025	-.050	.708	.300	-.555	.583
.450	-.494	.603	.050	-.478	.602	.050	-.439	.612	.450	-.494	.598
.600	-.526	.593	.100	-.593	.582	.100	-.489	.593	.600	-.459	.607
.800	-.389	.624	.150	-.575	.576	.150	-.482	.601	.400	-.216	.667
.950	.047	.742	.200	-.595	.572	.200	-.556	.583			
			.300	-.596	.573	.300	-.583	.576			
			.350	-.540	.577	.350	-.553	.583			
			.400	-.570	.579	.400	-.530	.589			
			.450	-.553	.583	.450	-.561	.582			
			.500	-.626	.566	.500	-.580	.577			
			.550	-.623	.566	.550	-.552	.584			
			.600	-.538	.582	.600	-.519	.592			
			.650	-.579	.572	.700	-.300	.646			
			.700	-.543	.586	.800	-.219	.664			
			.800	-.349	.637	.900	-.033	.712			
			.900	-.032	.712	.950	.075	.739			
			.950	.066	.737	.990	.154	.759			
			.990	.111	.748						
					LOWER SURFACE						
.100	-1.045	.464	.025	-.520	.592	.025	-.423	.616	.100	-1.475	.355
.300	-.793	.524	.050	-1.135	.447	.050	-1.029	.466	.300	-.650	.559
.600	-.256	.647	.100	-1.224	.417	.100	-1.315	.395	.600	-.437	.612
.800	.064	.736	.200	-1.183	.428	.200	-1.295	.400	.800	.025	.727
			.300	-.875	.504	.300	-.856	.508			
			.400	-.803	.522	.400	-.801	.522			
			.500	-.705	.546	.500	-.731	.539			
			.600	-.274	.653	.600	-.440	.612			
			.700	.042	.728	.700	-.121	.691			
			.800	.142	.755	.800	.130	.753			
			.900	.254	.783	.900	.207	.772			
			.950	.290	.792	.950	.243	.785			
			1.000	.125	.751						
CN=				-.1587			-.1603				
CM=				-.1041			-.0619				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = -1.65^o$; $C_L = 0.092$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.857	.508	0.000	1.114	.556	0.000	.085	.742	.050	-.731	.539
.150	-.823	.517	.012	.072	.738	.012	.007	.722	.150	-.705	.546
.300	-.691	.549	.025	-.335	.631	.025	-.308	.644	.300	-.631	.564
.450	-.528	.590	.050	-.748	.535	.050	-.716	.543	.450	-.540	.587
.600	-.554	.582	.100	-.933	.514	.100	-.758	.534	.600	-.475	.603
.800	-.390	.624	.150	-.752	.534	.150	-.669	.555	.800	-.208	.663
.950	.076	.739	.200	-.827	.515	.200	-.715	.543			
			.300	-.716	.543	.300	-.677	.552			
			.350	-.695	.547	.350	-.640	.562			
			.400	-.659	.557	.400	-.602	.571			
			.450	-.623	.565	.450	-.626	.565			
			.500	-.684	.551	.500	-.636	.563			
			.550	-.675	.553	.550	-.597	.572			
			.600	-.636	.570	.600	-.550	.584			
			.650	-.623	.565	.700	-.313	.643			
			.700	-.574	.578	.800	-.218	.666			
			.800	-.330	.639	.900	-.042	.710			
			.900	-.029	.713	.950	.066	.737			
			.950	.048	.732	.990	.139	.755			
			.990	.084	.741						
					LOWER SURFACE						
.100	-.745	.536	.025	-.307	.644	.025	-.169	.679	.100	-1.240	.413
.300	-.711	.544	.050	-.747	.535	.050	-.805	.521	.300	-.723	.541
.600	-.293	.648	.100	-.858	.508	.100	-.921	.492	.600	-.457	.607
.800	.117	.749	.200	-.832	.514	.200	-.864	.506	.800	.033	.729
			.300	-.815	.519	.300	-.888	.500			
			.400	-.754	.534	.400	-.783	.526			
			.500	-.697	.548	.500	-.722	.541			
			.600	-.282	.651	.600	-.452	.603			
			.700	.055	.734	.700	-.133	.687			
			.800	.192	.765	.800	.153	.758			
			.900	.296	.794	.900	.240	.780			
			.950	.314	.798	.950	.296	.794			
			1.000	.104	.746						
CN=				.1380			.0183				
CM=				-.1002			-.0535				

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = 0.06^o$; $C_L = 0.283$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.164	.433	0.000	1.103	.554	0.000	.083	.743	.050	-1.090	.451
.150	-1.174	.430	.012	-.190	.674	.012	-.255	.653	.150	-1.089	.451
.300	-.745	.536	.025	-.700	.547	.025	-.566	.590	.300	-.721	.542
.450	-.614	.569	.050	-1.052	.460	.050	-1.089	.451	.450	-.571	.579
.600	-.579	.577	.100	-1.315	.395	.100	-1.206	.422	.600	-.483	.601
.800	-.360	.632	.150	-1.139	.426	.150	-1.030	.466	.800	-.204	.670
.990	.053	.734	.200	-.906	.497	.200	-.814	.519			
			.300	-.813	.518	.300	-.828	.516			
			.350	-.752	.535	.350	-.726	.541			
			.400	-.723	.542	.400	-.673	.554			
			.450	-.691	.550	.450	-.675	.554			
			.500	-.742	.537	.500	-.673	.554			
			.550	-.709	.545	.550	-.622	.567			
			.600	-.652	.559	.600	-.560	.582			
			.650	-.638	.563	.700	-.316	.643			
			.700	-.596	.580	.800	-.212	.668			
			.800	-.313	.643	.900	-.036	.712			
			.900	-.034	.712	.950	.053	.735			
			.950	.040	.730	.990	.117	.750			
			.990	.056	.735						
					LOWER SURFACE						
.100	-.476	.603	.025	-.023	.715	.025	.060	.736	.100	-.816	.519
.300	-.614	.569	.050	-.434	.613	.050	-.518	.593	.300	-.659	.558
.600	-.315	.644	.100	-.567	.580	.100	-.624	.565	.600	-.479	.602
.800	.157	.760	.200	-.639	.563	.200	-.665	.555	.800	.095	.744
			.300	-.688	.550	.300	-.744	.537			
			.400	-.681	.552	.400	-.731	.540			
			.500	-.670	.555	.500	-.690	.550			
			.600	-.274	.653	.600	-.449	.610			
			.700	.066	.738	.700	-.131	.688			
			.800	.214	.774	.800	.169	.763			
			.900	.329	.802	.900	.270	.787			
			.950	.332	.803	.950	.320	.800			
			1.000	.068	.737						
CN=				.3299			.2052				
CM=				-.0929			-.0434				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = 1.92^o$; $C_L = 0.527$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.423	.359	0.000	1.005	.585	0.000	.092	.744	.050	-1.357	.385
.150	-1.571	.332	.012	-.457	.620	.012	-.550	.585	.150	-1.636	.316
.300	-1.042	.463	.025	-.551	.486	.025	-.730	.525	.300	-.693	.549
.450	-.600	.572	.050	-1.340	.389	.050	-1.332	.391	.450	-.558	.583
.600	-.386	.674	.100	-1.633	.324	.100	-1.512	.347	.600	-.476	.603
.800	-.383	.626	.150	-1.527	.343	.150	-1.497	.351	.800	-.205	.670
.950	.064	.737	.200	-1.534	.340	.200	-1.447	.363			
			.300	-1.535	.348	.300	-1.294	.401			
			.350	-.884	.507	.350	-.683	.552			
			.400	-.654	.559	.400	-.581	.577			
			.450	-.605	.571	.450	-.602	.572			
			.500	-.641	.562	.500	-.625	.566			
			.550	-.673	.554	.550	-.604	.571			
			.600	-.636	.563	.600	-.552	.584			
			.650	-.640	.562	.700	-.313	.642			
			.700	-.575	.579	.800	-.224	.665			
			.800	-.349	.634	.900	-.051	.703			
			.900	-.053	.708	.950	.049	.733			
			.950	.043	.732	.990	.122	.751			
			.990	.100	.746						
					LOWER SURFACE						
.100	-.270	.654	.025	-.117	.770	.025	-.283	.791	.100	-.514	.594
.300	-.502	.597	.050	-.144	.665	.050	-.213	.668	.300	-.573	.579
.600	-.277	.652	.100	-.302	.646	.100	-.370	.629	.600	-.470	.605
.800	.215	.774	.200	-.431	.614	.200	-.496	.593	.900	.119	.750
			.300	-.546	.586	.300	-.599	.573			
			.400	-.574	.579	.400	-.633	.564			
			.500	-.602	.572	.500	-.625	.566			
			.600	-.243	.661	.600	-.419	.617			
			.700	.085	.742	.700	-.117	.692			
			.800	.236	.782	.800	.190	.768			
			.900	.372	.813	.900	.293	.793			
			.950	.375	.814	.950	.345	.806			
			1.000	.112	.749						
CN=				.5860			.4302				
CM=				-.0915			-.0342				

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = 3.67^o$; $C_L = 0.735$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.696	.402	0.000	1.024	.574	0.000	.094	.744	.050	-1.563	.434
.150	-1.748	.389	.012	-.652	.560	.012	-.757	.534	.150	-1.814	.372
.300	-1.605	.424	.025	-1.195	.425	.025	-.995	.475	.300	-1.147	.437
.450	-.601	.572	.050	-1.559	.335	.050	-1.503	.344	.450	-.551	.585
.600	-.524	.591	.100	-1.790	.281	.100	-1.695	.302	.600	-.431	.614
.800	-.149	.635	.150	-1.717	.296	.150	-1.707	.299	.800	-.217	.667
.950	.079	.741	.200	-1.736	.292	.200	-1.665	.309			
			.300	-1.716	.297	.300	-1.677	.306			
			.350	-1.713	.297	.350	-1.661	.310			
			.400	-1.143	.439	.400	-.993	.475			
			.450	-.955	.485	.450	-.799	.523			
			.500	-.826	.517	.500	-.589	.575			
			.550	-.601	.572	.550	-.480	.602			
			.600	-.530	.587	.600	-.446	.611			
			.650	-.482	.602	.700	-.274	.652			
			.700	-.481	.602	.800	-.204	.671			
			.800	-.307	.646	.900	-.054	.708			
			.900	-.061	.706	.950	.040	.731			
			.950	.027	.728	.990	.110	.749			
			.990	.058	.745						
					LOWER SURFACE						
.100	-.056	.737	.025	.373	.814	.025	.496	.844	.100	-.315	.643
.300	-.391	.624	.050	.053	.734	.050	-.033	.713	.300	-.435	.601
.600	-.259	.657	.100	-.132	.688	.100	-.190	.674	.600	-.455	.608
.800	.252	.783	.200	-.273	.643	.200	-.339	.637	.300	.123	.751
			.300	-.413	.613	.300	-.466	.606			
			.400	-.476	.603	.400	-.559	.583			
			.500	-.534	.587	.500	-.562	.582			
			.600	-.214	.668	.600	-.397	.623			
			.700	.110	.743	.700	-.110	.694			
			.800	.309	.787	.800	.201	.771			
			.900	.411	.821	.900	.312	.793			
			.950	.378	.817	.950	.355	.803			
			1.000	.116	.749						
CN=				.7975			.6441				
CM=				-.0930			-.0320				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -6^o$; $\alpha = 4.86^o$; $C_L = 0.815$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.838	.267	0.000	.579	.563	0.000	.089	.743	.050	-1.671	.308
.150	-1.872	.258	.012	-.753	.525	.012	-.928	.491	.150	-1.814	.272
.300	-1.608	.323	.025	-1.321	.394	.025	-1.196	.425	.300	-1.336	.391
.450	-.742	.537	.050	-1.659	.311	.050	-1.599	.326	.450	-.587	.576
.600	-.481	.602	.100	-1.865	.260	.100	-1.799	.276	.600	-.437	.613
.800	-.292	.649	.150	-1.826	.265	.150	-1.801	.276	.800	-.223	.666
.990	.031	.729	.200	-1.837	.267	.200	-1.762	.285			
			.300	-1.584	.329	.300	-1.811	.273			
			.350	-1.225	.418	.350	-1.607	.324			
			.400	-1.166	.433	.400	-1.125	.443			
			.450	-1.122	.444	.450	-.965	.482			
			.500	-.998	.474	.500	-.743	.537			
			.550	-.828	.516	.550	-.549	.585			
			.600	-.667	.556	.600	-.424	.616			
			.650	-.505	.596	.700	-.254	.658			
			.700	-.352	.634	.800	-.177	.677			
			.800	-.224	.666	.900	-.053	.708			
			.900	-.072	.703	.950	.011	.724			
			.950	-.014	.718	.990	.069	.738			
			.990	.024	.727						
					LOWER SURFACE						
.100	.009	.723	.025	.476	.839	.025	.576	.863	.100	-.208	.669
.300	-.335	.638	.050	.175	.764	.050	.122	.751	.300	-.448	.610
.600	-.262	.656	.100	-.023	.715	.100	-.083	.700	.600	-.455	.609
.800	.269	.787	.200	-.228	.664	.200	-.259	.657	.800	.123	.751
			.300	-.352	.634	.300	-.411	.619			
			.400	-.430	.615	.400	-.526	.591			
			.500	-.507	.595	.500	-.542	.587			
			.600	-.211	.669	.600	-.394	.623			
			.700	.110	.748	.700	-.115	.692			
			.800	.310	.798	.800	.197	.770			
			.900	.400	.820	.900	.311	.798			
			.950	.366	.812	.950	.349	.807			
			1.000	.006	.727						
CN=				.9437			.7350				
CM=				-.0878			-.0295				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = -4.87^o$; $C_L = -0.247$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.277	.654	0.000	1.069	.585	0.000	.078	.741	.050	-.200	.672
.150	-.463	.607	.012	.502	.645	.017	.452	.833	.150	-.402	.622
.300	-.500	.598	.025	.124	.752	.025	.170	.763	.300	-.479	.603
.450	-.486	.626	.050	-.231	.664	.050	-.185	.675	.450	-.465	.606
.600	-.510	.595	.100	-.352	.634	.100	-.334	.639	.600	-.478	.603
.800	-.400	.622	.150	-.430	.615	.150	-.333	.639	.800	-.286	.651
.950	.041	.741	.200	-.476	.604	.200	-.427	.616			
			.300	-.512	.595	.300	-.499	.598			
			.350	-.492	.600	.350	-.486	.601			
			.400	-.509	.595	.400	-.476	.604			
			.450	-.485	.601	.450	-.518	.593			
			.500	-.583	.577	.500	-.558	.583			
			.550	-.596	.574	.550	-.556	.584			
			.600	-.525	.591	.600	-.547	.585			
			.650	-.599	.573	.700	-.378	.628			
			.700	-.565	.582	.800	-.279	.652			
			.800	-.351	.634	.900	-.036	.712			
			.900	-.056	.707	.950	.063	.737			
			.950	.062	.737	.990	.113	.749			
			.990	.111	.749						
					LOWER SURFACE						
.100	-1.144	.439	.025	-.683	.552	.025	-.623	.567	.100	-1.640	.316
.300	-.751	.536	.050	-1.324	.394	.050	-1.744	.414	.300	-.794	.525
.600	-.287	.650	.100	-1.452	.367	.100	-1.487	.354	.600	-.369	.630
.800	.076	.740	.200	-1.457	.361	.200	-1.521	.345	.800	.060	.736
			.300	-1.464	.359	.300	-1.549	.339			
			.400	-.709	.546	.400	-.633	.565			
			.500	-.677	.554	.500	-.604	.572			
			.600	-.284	.651	.600	-.362	.632			
			.700	.039	.731	.700	-.057	.707			
			.800	.158	.770	.800	.177	.765			
			.900	.288	.792	.900	.244	.781			
			.950	.295	.794	.950	.291	.793			
			1.000	.121	.751						
CN=				-.2278			-.2660				
CM=				-.1208			-.0956				

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = -3.17^o$; $C_L = -0.074$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.562	.582	0.000	1.055	.593	0.000	.084	.742	.050	-.471	.605
.150	-.630	.565	.012	.267	.787	.012	.227	.777	.150	-.553	.584
.300	-.581	.577	.025	-.152	.683	.025	-.040	.711	.300	-.559	.583
.450	-.468	.605	.050	-.479	.603	.050	-.441	.612	.450	-.512	.595
.600	-.533	.589	.100	-.579	.578	.100	-.524	.592	.600	-.498	.598
.800	-.364	.631	.150	-.614	.569	.150	-.508	.595	.800	-.278	.652
.950	.078	.740	.200	-.613	.570	.200	-.587	.576			
			.300	-.621	.568	.300	-.604	.572			
			.350	-.601	.572	.350	-.573	.579			
			.400	-.584	.577	.400	-.555	.584			
			.450	-.559	.583	.450	-.582	.577			
			.500	-.635	.564	.500	-.613	.570			
			.550	-.642	.562	.550	-.600	.573			
			.600	-.565	.581	.600	-.574	.579			
			.650	-.603	.572	.700	-.379	.627			
			.700	-.552	.585	.800	-.262	.656			
			.800	-.323	.640	.900	-.021	.716			
			.900	-.025	.715	.950	.064	.737			
			.950	.064	.737	.990	.103	.747			
			.990	.106	.747						
					LOWER SURFACE						
.100	-.855	.510	.025	-.491	.600	.025	-.413	.619	.100	-1.440	.365
.300	-.781	.528	.050	-1.043	.461	.050	-.992	.476	.300	-.668	.556
.600	-.296	.648	.100	-1.232	.417	.100	-1.292	.402	.600	-.403	.621
.800	.061	.736	.200	-.941	.489	.200	-1.238	.415	.800	.076	.740
			.300	-.894	.500	.300	-.887	.502			
			.400	-.794	.525	.400	-.797	.524			
			.500	-.702	.548	.500	-.681	.553			
			.600	-.265	.656	.600	-.378	.628			
			.700	.025	.727	.700	-.066	.705			
			.800	.144	.757	.800	.149	.758			
			.900	.261	.785	.900	.213	.774			
			.950	.284	.791	.950	.271	.788			
			1.000	.117	.750						
CN=				-.0339			-.1004				
CM=				-.1030			-.0785				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = -1.50^o$; $C_L = 0.123$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.477	.504	0.000	1.119	.998	0.000	.086	.742	.050	-.801	.523
.150	-.815	.520	.012	.050	.733	.012	-.034	.713	.150	-.737	.539
.300	-.723	.542	.025	-.427	.615	.025	-.313	.643	.300	-.669	.556
.450	-.539	.568	.050	-.817	.519	.050	-.798	.524	.450	-.558	.583
.600	-.563	.582	.100	-.820	.519	.100	-.786	.527	.600	-.515	.594
.800	-.362	.632	.150	-.776	.529	.150	-.693	.550	.900	-.274	.653
.990	.055	.735	.200	-.825	.517	.200	-.738	.539			
			.300	-.755	.534	.300	-.720	.543			
			.350	-.716	.544	.350	-.677	.554			
			.400	-.680	.553	.400	-.634	.565			
			.450	-.641	.563	.450	-.652	.560			
			.500	-.695	.549	.500	-.670	.556			
			.550	-.681	.553	.550	-.637	.564			
			.600	-.632	.565	.600	-.593	.575			
			.650	-.627	.566	.700	-.386	.626			
			.700	-.573	.580	.800	-.262	.656			
			.800	-.326	.640	.900	-.033	.713			
			.900	-.026	.715	.950	.045	.732			
			.950	.045	.737	.990	.082	.741			
			.990	.059	.738						
					LOWER SURFACE						
.100	-.586	.576	.025	-.261	.657	.025	-.151	.684	.100	-1.058	.460
.300	-.709	.544	.050	-.723	.542	.050	-.768	.531	.300	-.697	.549
.600	-.249	.650	.100	-.813	.519	.100	-.843	.513	.600	-.418	.618
.800	.119	.750	.200	-.817	.519	.200	-.804	.522	.800	.089	.743
			.300	-.746	.527	.300	-.833	.515			
			.400	-.718	.544	.400	-.764	.532			
			.500	-.677	.554	.500	-.663	.556			
			.600	-.287	.650	.600	-.384	.628			
			.700	.038	.731	.700	-.048	.704			
			.800	.174	.764	.800	.171	.763			
			.900	.298	.795	.900	.247	.782			
			.950	.301	.796	.950	.299	.795			
			1.000	.083	.742						
CN=				.1615			.0979				
CM=				-.0984			-.0696				

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = -0.31^o$; $C_L = 0.264$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.084	.454	0.000	1.103	.994	0.000	.085	.743	.050	-1.029	.469
.150	-1.097	.451	.012	-.113	.693	.012	-.210	.670	.150	-1.038	.466
.300	-.773	.531	.025	-.625	.553	.025	-.526	.592	.300	-.721	.544
.450	-.608	.572	.050	-1.026	.469	.050	-1.011	.472	.450	-.583	.578
.600	-.589	.576	.100	-1.263	.410	.100	-1.185	.429	.600	-.529	.591
.800	-.358	.633	.150	-1.032	.467	.150	-.962	.484	.900	-.277	.653
.990	.057	.736	.200	-.913	.496	.200	-.836	.515			
			.300	-.859	.507	.300	-.828	.517			
			.350	-.756	.535	.350	-.726	.542			
			.400	-.721	.544	.400	-.677	.555			
			.450	-.696	.550	.450	-.686	.552			
			.500	-.745	.538	.500	-.697	.550			
			.550	-.707	.547	.550	-.660	.559			
			.600	-.663	.558	.600	-.613	.570			
			.650	-.637	.565	.700	-.395	.624			
			.700	-.572	.580	.800	-.266	.656			
			.800	-.326	.641	.900	-.044	.711			
			.900	-.042	.711	.950	.023	.727			
			.950	.031	.729	.990	.054	.735			
			.990	.053	.735						
					LOWER SURFACE						
.100	-.416	.619	.025	-.092	.699	.025	.022	.727	.100	-.818	.520
.300	-.628	.567	.050	-.430	.603	.050	-.569	.581	.300	-.657	.559
.600	-.287	.651	.100	-.617	.565	.100	-.618	.569	.600	-.431	.615
.800	.166	.763	.200	-.668	.557	.200	-.686	.552	.900	.144	.757
			.300	-.706	.549	.300	-.742	.539			
			.400	-.663	.559	.400	-.723	.543			
			.500	-.660	.559	.500	-.653	.560			
			.600	-.230	.653	.600	-.394	.625			
			.700	.063	.737	.700	-.070	.704			
			.800	.243	.787	.800	.212	.774			
			.900	.351	.808	.900	.295	.794			
			.950	.354	.809	.950	.329	.803			
			1.000	.072	.739						
CN=				.3193			.2415				
CM=				-.1015			-.0671				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 0.09^o$; $C_L = 0.302$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.180	.629	0.000	1.106	.555	0.000	.088	.743	.050	-1.105	.448
.150	-1.243	.615	.012	-.184	.660	.012	-.300	.647	.150	-1.202	.424
.300	-.765	.527	.025	-.717	.544	.025	-.565	.581	.300	-.737	.539
.450	-.622	.567	.050	-1.125	.442	.050	-1.076	.455	.450	-.597	.573
.600	-.573	.578	.100	-1.333	.362	.100	-1.221	.419	.600	-.530	.590
.800	-.452	.634	.150	-1.253	.412	.150	-1.110	.447	.800	-.270	.654
.950	.054	.734	.200	-.935	.490	.200	-.915	.520			
			.300	-.854	.513	.300	-.850	.511			
			.350	-.762	.533	.350	-.738	.539			
			.400	-.727	.541	.400	-.696	.549			
			.450	-.711	.545	.450	-.706	.547			
			.500	-.749	.535	.500	-.713	.545			
			.550	-.719	.543	.550	-.667	.555			
			.600	-.642	.562	.600	-.617	.570			
			.650	-.628	.566	.700	-.384	.626			
			.700	-.530	.588	.800	-.255	.658			
			.900	-.318	.642	.900	-.040	.711			
			.300	-.047	.712	.950	.022	.727			
			.950	.027	.726	.990	.053	.734			
			.990	.051	.734						
					LOWER SURFACE						
.100	-.382	.627	.025	-.009	.719	.025	.045	.732	.100	-.747	.536
.300	-.620	.563	.050	-.363	.630	.050	-.497	.598	.300	-.634	.564
.600	-.401	.647	.100	-.552	.595	.100	-.600	.573	.600	-.427	.616
.800	.143	.756	.200	-.626	.566	.200	-.647	.561	.800	.137	.755
			.300	-.677	.554	.300	-.703	.547			
			.400	-.660	.558	.400	-.705	.547			
			.500	-.639	.563	.500	-.628	.566			
			.600	-.274	.653	.600	-.380	.627			
			.700	.056	.735	.700	-.065	.705			
			.800	.214	.774	.800	.198	.770			
			.900	.334	.804	.900	.277	.790			
			.950	.328	.802	.950	.318	.800			
			1.000	.066	.737						
CN=				.3512			.2726				
CM=				-.0330			-.0433				

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 1.13^o$; $C_L = 0.449$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.367	.582	0.000	1.054	.550	0.000	.089	.743	.050	-1.258	.409
.150	-1.456	.560	.012	-.373	.623	.012	-.416	.618	.150	-1.482	.354
.300	-.714	.544	.025	-.865	.507	.025	-.680	.552	.300	-.714	.544
.450	-.630	.565	.050	-1.243	.412	.050	-1.260	.409	.450	-.562	.574
.600	-.603	.572	.100	-1.502	.349	.100	-1.414	.371	.600	-.529	.590
.800	-.446	.625	.150	-1.427	.367	.150	-1.384	.374	.800	-.287	.650
.950	.056	.734	.200	-1.491	.359	.200	-1.357	.385			
			.300	-1.100	.448	.300	-.798	.523			
			.350	-.834	.564	.350	-.653	.559			
			.400	-.658	.558	.400	-.666	.556			
			.450	-.734	.546	.450	-.695	.549			
			.500	-.737	.539	.500	-.693	.548			
			.550	-.731	.540	.550	-.670	.555			
			.600	-.678	.553	.600	-.627	.566			
			.650	-.655	.556	.700	-.405	.621			
			.700	-.603	.572	.800	-.288	.650			
			.800	-.386	.630	.900	-.057	.707			
			.900	-.049	.708	.950	.026	.727			
			.950	.035	.729	.990	.077	.740			
			.990	.056	.737						
					LOWER SURFACE						
.100	-.245	.660	.025	.097	.745	.025	.223	.776	.100	-.589	.575
.300	-.531	.589	.050	-.220	.666	.050	-.332	.639	.300	-.586	.576
.600	-.292	.643	.100	-.428	.615	.100	-.462	.606	.600	-.424	.616
.800	.207	.772	.200	-.504	.596	.200	-.529	.590	.300	.174	.764
			.300	-.575	.578	.300	-.637	.563			
			.400	-.587	.575	.400	-.637	.563			
			.500	-.611	.569	.500	-.606	.571			
			.600	-.259	.657	.600	-.365	.630			
			.700	.085	.742	.700	-.056	.707			
			.800	.273	.790	.800	.238	.780			
			.900	.378	.814	.900	.320	.800			
			.950	.367	.812	.950	.357	.809			
			1.000	.250	.741						
CN=				.5062			.4055				
CM=				-.0394			-.0623				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 2.06^o$; $C_L = 0.565$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.445	.366	0.000	1.056	.582	0.000	.091	.744	.050	-1.395	.376
.150	-1.582	.330	.012	-.467	.606	.012	-.566	.581	.150	-1.654	.312
.300	-1.239	.415	.025	-1.006	.472	.025	-.829	.516	.300	-.684	.552
.450	-.616	.569	.050	-1.337	.376	.050	-1.334	.391	.450	-.592	.577
.600	-.581	.578	.100	-1.621	.321	.100	-1.560	.336	.600	-.528	.591
.800	-.383	.627	.150	-1.552	.338	.150	-1.563	.335	.800	-.279	.652
.950	.072	.739	.200	-1.553	.338	.200	-1.465	.359			
			.300	-1.501	.350	.300	-1.491	.353			
			.350	-.946	.488	.350	-.836	.515			
			.400	-.725	.542	.400	-.608	.571			
			.450	-.607	.571	.450	-.617	.570			
			.500	-.614	.565	.500	-.651	.560			
			.550	-.649	.561	.550	-.628	.566			
			.600	-.643	.562	.600	-.603	.572			
			.650	-.636	.564	.700	-.392	.624			
			.700	-.581	.578	.800	-.285	.651			
			.800	-.351	.634	.900	-.057	.707			
			.900	-.065	.705	.950	.028	.728			
			.950	.044	.732	.990	.078	.740			
			.990	.094	.744						
					LOWER SURFACE						
.100	-.131	.689	.025	.136	.770	.025	.303	.796	.100	-.477	.603
.300	-.466	.606	.050	-.115	.693	.050	-.196	.673	.300	-.535	.589
.600	-.278	.652	.100	-.274	.653	.100	-.340	.637	.600	-.413	.619
.800	.202	.771	.200	-.410	.620	.200	-.455	.609	.800	.173	.764
			.300	-.521	.592	.300	-.551	.585			
			.400	-.533	.589	.400	-.602	.572			
			.500	-.565	.582	.500	-.565	.582			
			.600	-.231	.664	.600	-.351	.635			
			.700	.098	.745	.700	-.049	.709			
			.800	.274	.789	.800	.239	.780			
			.900	.379	.815	.900	.320	.800			
			.950	.377	.814	.950	.355	.809			
			1.000	.100	.746						
CN=				.6187			.5284				
CM=				-.0933			-.0570				

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 2.49^o$; $C_L = 0.625$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.487	.353	0.000	1.055	.582	0.000	.098	.745	.050	-1.426	.368
.150	-1.640	.315	.012	-.550	.585	.012	-.616	.568	.150	-1.715	.296
.300	-1.432	.366	.025	-1.074	.455	.025	-.849	.511	.300	-.796	.524
.450	-.580	.577	.050	-1.427	.368	.050	-1.406	.373	.450	-.575	.578
.600	-.580	.577	.100	-1.653	.312	.100	-1.569	.333	.600	-.503	.596
.800	-.388	.625	.150	-1.599	.327	.150	-1.589	.328	.800	-.286	.650
.950	.064	.737	.200	-1.599	.325	.200	-1.542	.339			
			.300	-1.623	.319	.300	-1.543	.339			
			.350	-1.559	.335	.350	-1.473	.356			
			.400	-.903	.497	.400	-.764	.532			
			.450	-.658	.555	.450	-.587	.575			
			.500	-.587	.576	.500	-.590	.575			
			.550	-.596	.573	.550	-.578	.573			
			.600	-.617	.568	.600	-.567	.580			
			.650	-.613	.569	.700	-.387	.625			
			.700	-.566	.581	.800	-.291	.649			
			.800	-.344	.636	.900	-.065	.705			
			.900	-.064	.705	.950	.030	.728			
			.950	.040	.731	.990	.091	.743			
			.990	.104	.746						
					LOWER SURFACE						
.100	-.158	.682	.025	.231	.778	.025	.358	.809	.100	-.436	.613
.300	-.439	.612	.050	-.068	.704	.050	-.128	.687	.300	-.513	.594
.600	-.259	.657	.100	-.264	.655	.100	-.280	.651	.600	-.412	.619
.800	.238	.780	.200	-.333	.626	.200	-.405	.620	.800	.187	.767
			.300	-.480	.602	.300	-.508	.595			
			.400	-.523	.591	.400	-.578	.578			
			.500	-.545	.586	.500	-.553	.584			
			.600	-.223	.666	.600	-.349	.634			
			.700	.112	.748	.700	-.040	.711			
			.800	.306	.796	.800	.260	.765			
			.900	.402	.820	.900	.345	.806			
			.950	.337	.816	.950	.380	.815			
			1.000	.112	.748						
CN=				.6906			.6031				
CM=				-.0983			-.0606				

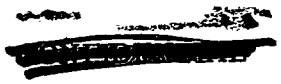


TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 3.65^o$; $C_L = 0.751$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.642	.315	0.000	1.018	.573	0.000	.093	.744	.050	-1.583	.330
.150	-1.751	.293	.012	-.656	.553	.012	-.764	.532	.150	-1.627	.270
.300	-1.623	.320	.025	-1.249	.412	.025	-.994	.475	.300	-1.256	.411
.450	-.678	.554	.050	-1.559	.336	.050	-1.505	.349	.450	-.581	.578
.600	-.523	.592	.100	-1.767	.284	.100	-1.700	.301	.600	-.486	.601
.800	-.350	.635	.150	-1.734	.293	.150	-1.716	.297	.800	-.290	.649
.950	.075	.740	.200	-1.730	.294	.200	-1.669	.308			
			.300	-1.727	.294	.300	-1.698	.301			
			.350	-1.688	.304	.350	-1.680	.306			
			.400	-1.114	.446	.400	-1.033	.466			
			.450	-.543	.487	.450	-.835	.515			
			.500	-.776	.529	.500	-.682	.552			
			.550	-.620	.568	.550	-.547	.585			
			.600	-.523	.592	.600	-.493	.599			
			.650	-.532	.590	.700	-.352	.634			
			.700	-.470	.605	.800	-.270	.654			
			.800	-.306	.646	.900	-.072	.703			
			.900	-.051	.709	.950	.021	.726			
			.950	.035	.730	.990	.085	.742			
			.990	.095	.745						
					LOWER SURFACE						
.100	.010	.724	.025	.375	.814	.025	.481	.840	.100	-.317	.643
.300	-.370	.630	.050	.057	.738	.050	.000	.721	.300	-.467	.606
.600	-.254	.658	.100	-.130	.689	.100	-.173	.678	.600	-.403	.621
.800	.254	.734	.200	-.301	.647	.200	-.322	.641	.800	.183	.766
			.300	-.358	.623	.300	-.447	.611			
			.400	-.466	.606	.400	-.527	.591			
			.500	-.516	.593	.500	-.515	.594			
			.600	-.204	.671	.600	-.330	.640			
			.700	.108	.743	.700	-.037	.712			
			.800	.314	.799	.800	.259	.785			
			.900	.403	.821	.900	.348	.807			
			.950	.334	.816	.950	.377	.814			
			1.000	.106	.747						
CN=					.7393			.7178			
CM=					-.0929			-.0582			

(e) M = 0.70. Continued.

$\delta_a = -3^o$; $\alpha = 4.76^o$; $C_L = 0.804$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.766	.285	0.000	.984	.564	0.000	.089	.743	.050	-1.687	.304
.150	-1.820	.271	.012	-.774	.530	.012	-.900	.499	.150	-1.827	.270
.300	-1.618	.321	.025	-1.318	.396	.025	-1.157	.435	.300	-1.399	.375
.450	-.713	.545	.050	-1.654	.313	.050	-1.604	.325	.450	-.588	.576
.600	-.470	.605	.100	-1.848	.265	.100	-1.791	.279	.600	-.431	.602
.800	-.261	.657	.150	-1.809	.276	.150	-1.802	.276	.800	-.287	.650
.950	-.055	.708	.200	-1.690	.304	.200	-1.747	.289			
			.300	-1.239	.415	.300	-1.748	.279			
			.350	-1.137	.440	.350	-1.641	.316			
			.400	-1.108	.447	.400	-1.094	.451			
			.450	-1.020	.469	.450	-.930	.491			
			.500	-.862	.508	.500	-.732	.540			
			.550	-.831	.523	.550	-.594	.574			
			.600	-.620	.568	.600	-.484	.602			
			.650	-.531	.590	.700	-.324	.641			
			.700	-.445	.611	.800	-.245	.661			
			.800	-.233	.651	.900	-.074	.703			
			.900	-.164	.681	.950	.003	.722			
			.950	-.108	.694	.990	.070	.739			
			.990	-.095	.698						
					LOWER SURFACE						
.100	.083	.742	.025	.456	.834	.025	.584	.865	.100	-.217	.668
.300	-.353	.644	.050	.153	.759	.050	.093	.744	.300	-.431	.615
.600	-.266	.655	.100	-.045	.710	.100	-.074	.703	.600	-.394	.624
.800	.249	.782	.200	-.234	.663	.200	-.270	.655	.800	.187	.767
			.300	-.368	.630	.300	-.405	.621			
			.400	-.441	.612	.400	-.502	.597			
			.500	-.511	.595	.500	-.482	.602			
			.600	-.226	.665	.600	-.324	.641			
			.700	.101	.746	.700	-.034	.713			
			.800	.302	.796	.800	.256	.784			
			.900	.373	.819	.900	.343	.806			
			.950	.352	.808	.950	.376	.814			
			1.000	-.091	.659						
CN=					.7954			.7853			
CM=					-.0973			-.0544			

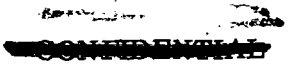


TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = -4.70^o$; $C_L = -0.221$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.287	.650	0.000	1.082	.989	0.000	.077	.740	.050	-.244	.660
.150	-.449	.606	.012	.470	.837	.012	.433	.828	.150	-.422	.616
.300	-.499	.597	.025	.109	.748	.025	.181	.766	.300	-.499	.597
.450	-.463	.606	.050	-.252	.658	.050	-.196	.672	.450	-.478	.602
.600	-.508	.595	.100	-.395	.623	.100	-.347	.635	.600	-.521	.592
.800	-.382	.626	.150	-.444	.611	.150	-.358	.632	.800	-.333	.638
.950	.083	.741	.200	-.501	.597	.200	-.462	.606			
			.300	-.529	.590	.300	-.522	.592			
			.350	-.508	.595	.350	-.489	.600			
			.400	-.522	.592	.400	-.505	.596			
			.450	-.519	.592	.450	-.537	.588			
			.500	-.593	.574	.500	-.586	.576			
			.550	-.557	.583	.550	-.595	.573			
			.600	-.551	.584	.600	-.564	.581			
			.650	-.556	.583	.700	-.450	.609			
			.700	-.557	.583	.800	-.272	.653			
			.800	-.353	.633	.900	-.026	.714			
			.900	-.028	.714	.950	.011	.723			
			.950	.059	.735	.990	.029	.728			
			.990	.099	.745						
					LOWER SURFACE						
.100	-1.123	.443	.025	-.664	.557	.025	-.594	.574	.100	-1.632	.317
.300	-.786	.524	.050	-1.301	.399	.050	-1.232	.416	.300	-.682	.552
.600	-.258	.657	.100	-1.450	.362	.100	-1.473	.355	.600	-.334	.638
.800	.055	.734	.200	-1.435	.366	.200	-1.494	.351	.800	.124	.751
			.300	-.973	.480	.300	-1.314	.396			
			.400	-.720	.543	.400	-.615	.569			
			.500	-.680	.552	.500	-.565	.581			
			.600	-.288	.649	.600	-.313	.643			
			.700	.031	.728	.700	-.010	.718			
			.800	.179	.765	.800	.200	.770			
			.900	.280	.790	.900	.252	.783			
			.950	.305	.796	.950	.275	.789			
			1.000	.112	.749						
CN=				-.1724			-.1959				
CM=				-.1199			-.1090				

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = -3.11^o$; $C_L = -0.059$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.488	.600	0.000	1.114	.956	0.000	.083	.742	.050	-.520	.593
.150	-.628	.566	.012	.300	.795	.012	.229	.773	.150	-.531	.590
.300	-.606	.571	.025	-.127	.690	.025	-.063	.706	.300	-.565	.581
.450	-.511	.595	.050	-.501	.597	.050	-.492	.599	.450	-.521	.592
.600	-.536	.589	.100	-.552	.582	.100	-.537	.588	.600	-.541	.587
.800	-.384	.631	.150	-.608	.571	.150	-.530	.590	.800	-.321	.642
.950	.065	.737	.200	-.635	.564	.200	-.594	.574			
			.300	-.625	.567	.300	-.620	.569			
			.350	-.589	.575	.350	-.564	.582			
			.400	-.557	.583	.400	-.566	.581			
			.450	-.585	.576	.450	-.602	.572			
			.500	-.637	.564	.500	-.640	.563			
			.550	-.643	.562	.550	-.626	.566			
			.600	-.592	.575	.600	-.597	.574			
			.650	-.604	.572	.700	-.440	.612			
			.700	-.554	.584	.800	-.269	.654			
			.800	-.333	.640	.900	-.037	.712			
			.900	-.032	.713	.950	-.003	.720			
			.950	.061	.736	.990	.011	.724			
			.990	.088	.743						
					LOWER SURFACE						
.100	-.823	.518	.025	-.488	.600	.025	-.391	.624	.100	-1.428	.368
.300	-.786	.527	.050	-1.106	.448	.050	-1.000	.474	.300	-.689	.551
.600	-.283	.651	.100	-1.238	.422	.100	-1.273	.406	.600	-.357	.633
.800	.058	.735	.200	-.943	.488	.200	-1.137	.440	.800	.133	.755
			.300	-.888	.502	.300	-.902	.498			
			.400	-.765	.532	.400	-.770	.531			
			.500	-.680	.553	.500	-.625	.566			
			.600	-.272	.654	.600	-.313	.644			
			.700	.030	.728	.700	-.016	.717			
			.800	.140	.756	.800	.175	.764			
			.900	.251	.783	.900	.244	.781			
			.950	.276	.789	.950	.274	.789			
			1.000	.094	.744						
CN=				-.0238			-.0412				
CM=				-.1037			-.0951				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = -2.27^o$; $C_L = 0.040$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.667	.556	0.000	1.101	.993	0.000	.071	.738	.050	-.720	.543
.150	-.711	.545	.012	.152	.759	.012	.097	.745	.150	-.615	.569
.300	-.672	.555	.025	-.302	.646	.025	-.197	.672	.300	-.457	.558
.450	-.593	.574	.050	-.636	.559	.050	-.601	.572	.450	-.542	.587
.600	-.593	.584	.100	-.720	.543	.100	-.689	.551	.600	-.552	.585
.800	-.366	.631	.150	-.710	.545	.150	-.676	.566	.800	-.324	.641
.950	.041	.735	.200	-.746	.536	.200	-.704	.547			
			.300	-.691	.550	.300	-.689	.551			
			.350	-.654	.559	.350	-.612	.565			
			.400	-.643	.562	.400	-.605	.571			
			.450	-.608	.571	.450	-.637	.564			
			.500	-.671	.555	.500	-.668	.556			
			.550	-.661	.557	.550	-.659	.558			
			.600	-.623	.567	.600	-.612	.570			
			.650	-.618	.568	.700	-.449	.610			
			.700	-.561	.582	.800	-.254	.659			
			.800	-.324	.641	.900	-.047	.709			
			.900	-.227	.714	.950	-.010	.718			
			.950	.047	.733	.990	.000	.721			
			.990	.088	.743						
					LOWER SURFACE						
.100	-.624	.567	.025	-.351	.634	.025	-.274	.653	.100	-1.327	.393
.300	-.733	.540	.050	-.353	.507	.050	-.874	.505	.300	-.703	.547
.600	-.247	.650	.100	-.857	.499	.100	-1.185	.428	.600	-.354	.633
.900	.070	.738	.200	-.944	.488	.200	-.876	.504	.900	.126	.752
			.300	-.847	.511	.300	-.881	.503			
			.400	-.747	.536	.400	-.762	.533			
			.500	-.676	.554	.500	-.638	.563			
			.600	-.268	.655	.600	-.321	.642			
			.700	.033	.729	.700	-.020	.716			
			.800	.158	.760	.800	.181	.766			
			.900	.260	.785	.900	.239	.780			
			.950	.282	.791	.950	.293	.793			
			1.000	.091	.743						
CN=				.0827			.0510				
CM=				-.0974			-.0913				

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = -1.44^o$; $C_L = 0.138$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.883	.504	0.000	1.103	.995	0.000	.092	.744	.050	-.844	.513
.150	-.822	.518	.012	.031	.729	.012	-.039	.712	.150	-.730	.541
.300	-.739	.537	.025	-.429	.615	.025	-.334	.639	.300	-.686	.552
.450	-.610	.570	.050	-.825	.517	.050	-.770	.531	.450	-.575	.579
.600	-.566	.581	.100	-.862	.508	.100	-.739	.526	.600	-.564	.582
.800	-.359	.642	.150	-.787	.527	.150	-.700	.548	.800	-.322	.642
.950	.041	.731	.200	-.901	.498	.200	-.775	.530			
			.300	-.748	.536	.300	-.770	.531			
			.350	-.726	.542	.350	-.689	.551			
			.400	-.691	.550	.400	-.653	.560			
			.450	-.691	.550	.450	-.659	.558			
			.500	-.705	.547	.500	-.697	.549			
			.550	-.657	.559	.550	-.674	.555			
			.600	-.645	.562	.600	-.615	.569			
			.650	-.632	.565	.700	-.444	.611			
			.700	-.554	.582	.800	-.263	.656			
			.800	-.324	.641	.900	-.059	.707			
			.900	-.033	.713	.950	-.023	.715			
			.950	.036	.730	.990	-.010	.719			
			.990	.051	.734						
					LOWER SURFACE						
.100	-.545	.546	.025	-.262	.656	.025	-.120	.691	.100	-1.057	.460
.300	-.679	.553	.050	-.744	.537	.050	-.765	.532	.300	-.671	.555
.600	-.299	.647	.100	-.736	.527	.100	-.809	.521	.600	-.362	.637
.800	.089	.743	.200	-.817	.519	.200	-.761	.533	.800	.142	.756
			.300	-.783	.528	.300	-.785	.527			
			.400	-.720	.543	.400	-.739	.538			
			.500	-.661	.558	.500	-.612	.570			
			.600	-.273	.654	.600	-.316	.643			
			.700	.050	.733	.700	-.016	.717			
			.800	.183	.766	.800	.215	.774			
			.900	.274	.789	.900	.268	.787			
			.950	.306	.797	.950	.291	.793			
			1.000	.077	.740						
CN=				.1827			.1628				
CM=				-.0954			-.0891				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = -0.61^o$; $C_L = 0.232$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.021	.468	0.000	1.112	.956	0.000	.086	.742	.050	-1.037	.465
.150	-.949	.486	.012	-.100	.696	.012	-.164	.680	.150	-.897	.499
.300	-.763	.537	.025	-.614	.569	.025	-.457	.608	.300	-.723	.542
.450	-.627	.566	.050	-1.012	.471	.050	-.968	.482	.450	-.594	.574
.600	-.578	.578	.100	-1.200	.424	.100	-1.048	.462	.600	-.570	.580
.800	-.350	.634	.150	-.814	.520	.150	-.795	.524	.800	-.329	.640
.990	.053	.734	.200	-.973	.480	.200	-.843	.513			
			.300	-.819	.518	.300	-.816	.519			
			.350	-.747	.536	.350	-.719	.543			
			.400	-.725	.542	.400	-.680	.553			
			.450	-.723	.542	.450	-.706	.546			
			.500	-.736	.539	.500	-.717	.544			
			.550	-.700	.548	.550	-.695	.549			
			.600	-.664	.557	.600	-.621	.567			
			.650	-.630	.565	.700	-.444	.611			
			.700	-.560	.583	.800	-.250	.659			
			.800	-.305	.646	.900	-.057	.707			
			.900	-.036	.712	.950	-.037	.712			
			.950	.024	.727	.990	-.026	.715			
			.990	.051	.734						
					LOWER SURFACE						
.100	-.413	.619	.025	-.113	.693	.025	-.035	.712	.100	-.894	.500
.300	-.634	.564	.050	-.531	.590	.050	-.561	.582	.300	-.643	.562
.600	-.299	.647	.100	-.663	.557	.100	-.653	.560	.600	-.378	.627
.800	.121	.751	.200	-.706	.546	.200	-.707	.546	.800	.197	.770
			.300	-.733	.540	.300	-.735	.539			
			.400	-.695	.549	.400	-.702	.547			
			.500	-.660	.558	.500	-.594	.574			
			.600	-.278	.652	.600	-.322	.641			
			.700	.056	.735	.700	-.001	.721			
			.800	.202	.771	.800	.231	.778			
			.900	.307	.797	.900	.290	.793			
			.950	.317	.799	.950	.315	.799			
			1.000	.063	.737						
CN=				.2716			.2527				
CM=				-.0950			-.0851				

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = 0.25^o$; $C_L = 0.335$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.167	.432	0.000	1.102	.954	0.000	.081	.741	.050	-1.201	.424
.150	-1.252	.411	.012	-.228	.664	.012	-.328	.640	.150	-1.152	.436
.300	-.777	.529	.025	-.754	.534	.025	-.580	.578	.300	-.736	.539
.450	-.662	.557	.050	-1.152	.436	.050	-1.135	.440	.450	-.611	.570
.600	-.585	.576	.100	-1.338	.390	.100	-1.252	.411	.600	-.576	.578
.800	-.357	.634	.150	-1.283	.404	.150	-1.181	.429	.800	-.336	.638
.950	.051	.733	.200	-1.169	.432	.200	-1.057	.460			
			.300	-.763	.532	.300	-.887	.502			
			.350	-.752	.535	.350	-.743	.537			
			.400	-.750	.536	.400	-.718	.543			
			.450	-.743	.537	.450	-.719	.543			
			.500	-.752	.535	.500	-.742	.538			
			.550	-.717	.544	.550	-.703	.547			
			.600	-.676	.554	.600	-.637	.563			
			.650	-.647	.561	.700	-.442	.612			
			.700	-.563	.582	.800	-.250	.659			
			.800	-.322	.641	.900	-.070	.704			
			.900	-.049	.709	.950	-.038	.711			
			.950	.020	.726	.990	-.037	.712			
			.990	.046	.737						
					LOWER SURFACE						
.100	-.318	.642	.025	-.003	.720	.025	.145	.757	.100	-.712	.545
.300	-.587	.576	.050	-.412	.619	.050	-.448	.610	.300	-.615	.569
.600	-.289	.649	.100	-.528	.590	.100	-.543	.587	.600	-.366	.630
.800	.154	.759	.200	-.604	.572	.200	-.611	.570	.800	.224	.776
			.300	-.650	.560	.300	-.661	.558			
			.400	-.643	.562	.400	-.668	.556			
			.500	-.629	.565	.500	-.576	.578			
			.600	-.266	.655	.600	-.314	.643			
			.700	.069	.738	.700	-.004	.720			
			.800	.236	.779	.800	.238	.780			
			.900	.325	.801	.900	.310	.798			
			.950	.332	.803	.950	.336	.804			
			1.000	.060	.736						
CN=				.3873			.3683				
CM=				-.0948			-.0804				

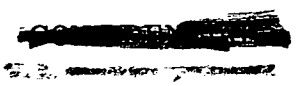


TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = 1.21^o$; $C_L = 0.463$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.303	.399	0.000	1.080	.588	0.000	.087	.743	.050	-1.332	.392
.150	-1.434	.367	.012	-.357	.633	.012	-.462	.607	.150	-1.553	.337
.300	-.799	.524	.025	-.907	.497	.025	-.716	.544	.300	-.670	.555
.450	-.667	.556	.050	-1.290	.402	.050	-1.259	.410	.450	-.617	.569
.600	-.595	.574	.100	-1.499	.350	.100	-1.438	.366	.600	-.580	.578
.800	-.367	.630	.150	-1.411	.372	.150	-1.409	.373	.800	-.338	.638
.990	.059	.736	.200	-1.439	.365	.200	-1.343	.389			
			.300	-.977	.480	.300	-.801	.523			
			.350	-.725	.542	.350	-.675	.554			
			.400	-.660	.558	.400	-.674	.555			
			.450	-.705	.547	.450	-.689	.551			
			.500	-.751	.535	.500	-.735	.539			
			.550	-.715	.544	.550	-.707	.546			
			.600	-.676	.554	.600	-.651	.560			
			.650	-.655	.559	.700	-.470	.605			
			.700	-.583	.577	.800	-.284	.651			
			.800	-.337	.638	.900	-.061	.706			
			.900	-.047	.710	.950	-.021	.716			
			.950	.037	.730	.990	-.006	.720			
			.990	.074	.739						
					LOWER SURFACE						
.100	-.221	.666	.025	.106	.747	.025	.243	.781	.100	-.596	.574
.300	-.523	.592	.050	-.210	.669	.050	-.316	.643	.300	-.557	.583
.600	-.291	.649	.100	-.368	.630	.100	-.441	.612	.600	-.376	.628
.800	.182	.766	.200	-.520	.592	.200	-.515	.594	.800	.230	.778
			.300	-.585	.577	.300	-.585	.577			
			.400	-.586	.576	.400	-.614	.569			
			.500	-.597	.574	.500	-.549	.585			
			.600	-.251	.659	.600	-.312	.644			
			.700	.086	.742	.700	.014	.724			
			.800	.248	.782	.800	.272	.788			
			.900	.351	.808	.900	.336	.804			
			.950	.352	.808	.950	.348	.807			
			1.000	.074	.739						
CN=				.4976			.4608				
CM=				-.0920			-.0780				

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = 2.13^o$; $C_L = 0.585$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.446	.363	0.000	1.057	.582	0.000	.089	.743	.050	-1.458	.360
.150	-1.559	.335	.012	-.491	.600	.012	-.584	.577	.150	-1.679	.306
.300	-1.297	.400	.025	-1.011	.471	.025	-.929	.516	.300	-.662	.557
.450	-.624	.567	.050	-1.389	.378	.050	-1.341	.389	.450	-.585	.576
.600	-.582	.577	.100	-1.593	.327	.100	-1.520	.345	.600	-.561	.582
.800	-.372	.629	.150	-1.566	.334	.150	-1.566	.334	.800	-.344	.636
.990	.072	.739	.200	-1.596	.326	.200	-1.482	.354			
			.300	-1.581	.330	.300	-1.517	.346			
			.350	-1.367	.383	.350	-.961	.483			
			.400	-.810	.521	.400	-.723	.542			
			.450	-.677	.553	.450	-.637	.563			
			.500	-.655	.559	.500	-.648	.561			
			.550	-.647	.561	.550	-.665	.557			
			.600	-.628	.566	.600	-.630	.565			
			.650	-.623	.567	.700	-.470	.605			
			.700	-.569	.580	.800	-.311	.644			
			.800	-.351	.634	.900	-.070	.704			
			.900	-.066	.705	.950	.001	.721			
			.950	.046	.732	.990	.036	.730			
			.990	.087	.743						
					LOWER SURFACE						
.100	-.100	.696	.025	.254	.784	.025	.354	.809	.100	-.465	.606
.300	-.480	.602	.050	-.106	.695	.050	-.163	.681	.300	-.514	.594
.600	-.261	.657	.100	-.294	.648	.100	-.317	.643	.600	-.360	.632
.800	.209	.773	.200	-.423	.616	.200	-.416	.618	.800	.245	.782
			.300	-.496	.598	.300	-.531	.590			
			.400	-.523	.592	.400	-.566	.581			
			.500	-.550	.585	.500	-.505	.596			
			.600	-.231	.664	.600	-.290	.649			
			.700	.101	.746	.700	.016	.725			
			.800	.282	.791	.800	.291	.793			
			.900	.383	.816	.900	.354	.808			
			.950	.368	.812	.950	.370	.812			
			1.000	.105	.747						
CN=				.6563			.6030				
CM=				-.0977			-.0786				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = 3.81^o$; $C_L = 0.780$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.681	.306	0.000	1.012	.971	0.000	.098	.745	.050	-1.660	.311
.150	-1.761	.286	.012	-.673	.555	.012	-.835	.515	.150	-1.863	.261
.300	-1.646	.314	.025	-1.207	.423	.025	-1.039	.464	.300	-1.582	.330
.450	-.757	.534	.050	-1.572	.332	.050	-1.507	.349	.450	-.589	.575
.600	-.514	.594	.100	-1.778	.282	.100	-1.718	.296	.600	-.532	.590
.800	-.325	.641	.150	-1.725	.295	.150	-1.742	.290	.800	-.342	.637
.950	.076	.740	.200	-1.759	.286	.200	-1.692	.303			
			.300	-1.739	.291	.300	-1.729	.294			
			.350	-1.716	.297	.350	-1.694	.302			
			.400	-1.106	.448	.400	-1.366	.384			
			.450	-.999	.474	.450	-.922	.493			
			.500	-.904	.498	.500	-.794	.525			
			.550	-.720	.543	.550	-.607	.571			
			.600	-.587	.576	.600	-.534	.589			
			.650	-.498	.598	.700	-.413	.619			
			.700	-.404	.621	.800	-.308	.645			
			.800	-.273	.654	.900	-.083	.700			
			.900	-.070	.704	.950	-.001	.721			
			.950	.026	.727	.990	.049	.733			
			.990	.085	.742						
					LOWER SURFACE						
.100	.037	.729	.025	.398	.819	.025	.508	.847	.100	-.304	.646
.300	-.351	.634	.050	.108	.748	.050	.046	.732	.300	-.456	.608
.600	-.259	.657	.100	-.090	.699	.100	-.147	.685	.600	-.349	.635
.800	.230	.778	.200	-.268	.655	.200	-.301	.647	.800	.251	.783
			.300	-.392	.624	.300	-.433	.614			
			.400	-.438	.613	.400	-.490	.600			
			.500	-.486	.601	.500	-.459	.608			
			.600	-.192	.674	.600	-.259	.657			
			.700	.116	.750	.700	.045	.732			
			.800	.313	.798	.800	.314	.799			
			.900	.408	.822	.900	.381	.815			
			.950	.374	.813	.950	.404	.821			
			1.000	.075	.739						
CN=				.8289			.8160				
CM=				-.0945			-.0847				

(e) M = 0.70. Continued.

$\delta_a = 0^o$; $\alpha = 4.09^o$; $C_L = 0.802$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.709	.299	0.000	1.014	.972	0.000	.095	.745	.050	-1.686	.305
.150	-1.808	.275	.012	-.679	.553	.012	-.897	.499	.150	-1.882	.256
.300	-1.681	.306	.025	-1.253	.412	.025	-1.044	.463	.300	-1.629	.319
.450	-.736	.539	.050	-1.612	.323	.050	-1.514	.347	.450	-.600	.573
.600	-.493	.599	.100	-1.810	.274	.100	-1.756	.287	.600	-.520	.593
.800	-.321	.642	.150	-1.749	.289	.150	-1.757	.287	.800	-.351	.634
.990	.055	.735	.200	-1.780	.281	.200	-1.715	.297			
			.300	-1.764	.285	.300	-1.730	.294			
			.350	-1.518	.346	.350	-1.742	.291			
			.400	-1.111	.447	.400	-1.344	.389			
			.450	-1.051	.462	.450	-.957	.485			
			.500	-.942	.488	.500	-.780	.528			
			.550	-.868	.522	.550	-.626	.566			
			.600	-.637	.564	.600	-.537	.588			
			.650	-.495	.599	.700	-.398	.623			
			.700	-.402	.622	.800	-.295	.648			
			.800	-.270	.655	.900	-.080	.701			
			.900	-.077	.702	.950	-.002	.721			
			.950	.012	.724	.990	.052	.734			
			.990	.034	.730						
					LOWER SURFACE						
.100	.046	.733	.025	.425	.826	.025	.541	.855	.100	-.256	.658
.300	-.353	.634	.050	.123	.752	.050	.072	.739	.300	-.435	.614
.600	-.251	.659	.100	-.090	.699	.100	-.119	.692	.600	-.334	.639
.800	.247	.782	.200	-.266	.655	.200	-.280	.652	.800	.251	.783
			.300	-.383	.627	.300	-.392	.624			
			.400	-.441	.612	.400	-.478	.603			
			.500	-.490	.600	.500	-.436	.614			
			.600	-.205	.671	.600	-.261	.657			
			.700	.118	.750	.700	.044	.732			
			.800	.316	.799	.800	.315	.799			
			.900	.399	.820	.900	.373	.813			
			.950	.373	.813	.950	.403	.821			
			1.000	.026	.728						
CN=				.8386			.8363				
CM=				-.0961			-.0829				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = -4.64^o$; $C_L = -0.205$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.323	.641	0.000	1.081	.988	0.000	.080	.740	.050	-.333	.663
.150	-.532	.567	.012	.476	.838	.012	.411	.822	.150	-.421	.617
.300	-.520	.592	.025	.047	.737	.025	.136	.754	.300	-.511	.594
.450	-.430	.614	.050	-.263	.656	.050	-.238	.662	.450	-.501	.567
.600	-.514	.594	.100	-.378	.627	.100	-.336	.638	.600	-.543	.586
.800	-.400	.622	.150	-.408	.620	.150	-.379	.627	.800	-.366	.630
.990	.073	.739	.200	-.511	.594	.200	-.465	.606			
			.300	-.533	.589	.300	-.544	.586			
			.350	-.525	.591	.350	-.514	.594			
			.400	-.541	.587	.400	-.513	.594			
			.450	-.502	.597	.450	-.563	.581			
			.500	-.595	.574	.500	-.611	.570			
			.550	-.610	.570	.550	-.607	.570			
			.600	-.562	.582	.600	-.607	.571			
			.650	-.615	.569	.700	-.463	.606			
			.700	-.572	.579	.800	-.241	.661			
			.800	-.357	.632	.900	-.095	.697			
			.900	-.052	.708	.950	-.088	.699			
			.950	.051	.733	.990	-.084	.700			
			.990	.108	.747						
					LOWER SURFACE						
.100	-1.097	.449	.025	-.635	.564	.025	-.584	.576	.100	-1.599	.325
.300	-.737	.524	.050	-1.297	.400	.050	-1.184	.428	.300	-.630	.565
.600	-.275	.653	.100	-1.388	.377	.100	-1.469	.357	.600	-.309	.644
.800	.035	.729	.200	-1.387	.378	.200	-1.489	.352	.800	.160	.760
			.300	-.818	.518	.300	-1.017	.469			
			.400	-.755	.534	.400	-.617	.568			
			.500	-.675	.554	.500	-.552	.584			
			.600	-.283	.651	.600	-.284	.650			
			.700	.037	.730	.700	.042	.731			
			.800	.188	.767	.800	.257	.784			
			.900	.274	.788	.900	.287	.792			
			.950	.314	.798	.950	.290	.793			
			1.000	.100	.745						
CN=				-.1359			-.1201				
CM=				-.1230			-.1285				

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = -3.08^o$; $C_L = -0.043$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.525	.591	0.000	1.088	.992	0.000	.081	.741	.050	-.524	.591
.150	-.455	.559	.012	.293	.793	.012	.210	.773	.150	-.583	.577
.300	-.592	.574	.025	-.174	.678	.025	-.081	.701	.300	-.595	.574
.450	-.502	.597	.050	-.505	.596	.050	-.504	.596	.450	-.542	.587
.600	-.542	.587	.100	-.607	.571	.100	-.554	.584	.600	-.565	.581
.800	-.382	.624	.150	-.608	.570	.150	-.520	.592	.800	-.359	.632
.990	.070	.738	.200	-.655	.559	.200	-.610	.570			
			.300	-.623	.567	.300	-.627	.565			
			.350	-.618	.568	.350	-.592	.574			
			.400	-.620	.567	.400	-.581	.577			
			.450	-.585	.576	.450	-.610	.570			
			.500	-.669	.555	.500	-.649	.560			
			.550	-.650	.560	.550	-.642	.562			
			.600	-.587	.576	.600	-.626	.566			
			.650	-.616	.568	.700	-.460	.607			
			.700	-.577	.578	.800	-.228	.664			
			.800	-.332	.639	.900	-.110	.694			
			.900	-.044	.710	.950	-.098	.696			
			.950	.053	.734	.990	-.098	.696			
			.990	.085	.742						
					LOWER SURFACE						
.100	-.306	.497	.025	-.457	.608	.025	-.377	.627	.100	-1.400	.374
.300	-.734	.527	.050	-1.070	.468	.050	-.971	.481	.300	-.661	.557
.600	-.292	.651	.100	-1.177	.429	.100	-1.274	.406	.600	-.304	.645
.800	.047	.732	.200	-.954	.485	.200	-1.019	.469	.800	.154	.759
			.300	-.873	.505	.300	-.856	.509			
			.400	-.766	.531	.400	-.744	.537			
			.500	-.680	.552	.500	-.592	.574			
			.600	-.267	.655	.600	-.274	.653			
			.700	.028	.728	.700	.027	.727			
			.800	.148	.757	.800	.215	.774			
			.900	.241	.780	.900	.274	.789			
			.950	.288	.792	.950	.297	.794			
			1.000	.104	.746						
CN=				-.0027			.0192				
CM=				-.1064			-.1125				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = -1.40^o$; $C_L = 0.158$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.884	.502	0.000	1.107	.995	0.000	.087	.742	.050	-.837	.514
.150	-.878	.504	.012	.021	.726	.012	-.083	.700	.150	-.760	.533
.300	-.704	.547	.025	-.480	.602	.025	-.348	.635	.300	-.699	.548
.450	-.575	.578	.050	-.814	.519	.050	-.822	.517	.450	-.594	.574
.600	-.572	.579	.100	-.963	.482	.100	-.826	.517	.600	-.586	.576
.800	-.375	.628	.150	-.800	.523	.150	-.724	.542	.800	-.361	.632
.990	.070	.738	.200	-.833	.515	.200	-.767	.531			
			.300	-.749	.535	.300	-.762	.532			
			.350	-.705	.546	.350	-.695	.549			
			.400	-.688	.551	.400	-.670	.555			
			.450	-.674	.554	.450	-.687	.551			
			.500	-.726	.541	.500	-.719	.543			
			.550	-.708	.546	.550	-.690	.550			
			.600	-.645	.561	.600	-.655	.559			
			.650	-.635	.564	.700	-.463	.606			
			.700	-.573	.579	.800	-.232	.663			
			.800	-.335	.638	.900	-.124	.690			
			.900	-.052	.708	.950	-.117	.692			
			.550	.030	.728	.990	-.116	.692			
			.990	.064	.737						
					LOWER SURFACE						
.100	-.569	.580	.025	-.247	.660	.025	-.145	.685	.100	-1.052	.460
.300	-.671	.555	.050	-.681	.552	.050	-.725	.541	.300	-.660	.557
.600	-.302	.646	.100	-.752	.535	.100	-.797	.524	.600	-.308	.644
.800	.115	.749	.200	-.764	.532	.200	-.770	.530	.800	.186	.767
			.300	-.771	.530	.300	-.765	.531			
			.400	-.708	.546	.400	-.708	.546			
			.500	-.659	.558	.500	-.575	.579			
			.600	-.275	.653	.600	-.280	.652			
			.700	.054	.734	.700	.042	.731			
			.800	.196	.769	.800	.264	.786			
			.900	.305	.796	.900	.319	.800			
			.550	.323	.801	.950	.322	.800			
			1.000	.078	.740						
CN=				.2065			.2150				
CM=				-.1033			-.1080				

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = -0.15^o$; $C_L = 0.311$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.123	.444	0.000	1.101	.993	0.000	.089	.743	.050	-1.086	.453
.150	-1.218	.421	.012	-.163	.681	.012	-.276	.653	.150	-1.109	.447
.300	-.804	.523	.025	-.704	.548	.025	-.562	.582	.300	-.744	.538
.450	-.630	.566	.050	-1.124	.444	.050	-1.100	.450	.450	-.620	.568
.600	-.593	.575	.100	-1.358	.386	.100	-1.208	.423	.600	-.601	.573
.800	-.366	.631	.150	-1.230	.418	.150	-1.103	.449	.800	-.365	.631
.990	.051	.734	.200	-.937	.490	.200	-.844	.513			
			.300	-.853	.511	.300	-.892	.501			
			.350	-.789	.526	.350	-.753	.535			
			.400	-.739	.539	.400	-.711	.546			
			.450	-.736	.540	.450	-.720	.544			
			.500	-.773	.530	.500	-.743	.538			
			.550	-.729	.541	.550	-.699	.549			
			.600	-.681	.553	.600	-.653	.560			
			.650	-.665	.557	.700	-.454	.609			
			.700	-.583	.577	.800	-.228	.665			
			.800	-.337	.638	.900	-.144	.686			
			.900	-.062	.706	.950	-.138	.687			
			.950	.021	.727	.990	-.143	.686			
			.990	.049	.733						
					LOWER SURFACE						
.100	-.431	.615	.025	-.028	.714	.025	.058	.736	.100	-.788	.527
.300	-.606	.572	.050	-.436	.614	.050	-.502	.597	.300	-.602	.573
.600	-.301	.647	.100	-.566	.582	.100	-.565	.582	.600	-.305	.645
.800	.156	.760	.200	-.630	.566	.200	-.631	.566	.800	.250	.783
			.300	-.649	.561	.300	-.675	.555			
			.400	-.637	.564	.400	-.655	.560			
			.500	-.628	.566	.500	-.552	.585			
			.600	-.272	.654	.600	-.275	.653			
			.700	.066	.738	.700	.064	.737			
			.800	.236	.780	.800	.316	.799			
			.900	.333	.804	.900	.348	.807			
			.550	.338	.805	.950	.342	.806			
			1.000	.058	.736						
CN=				.3731			.3730				
CM=				-.1015			-.1044				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = 0.31^o$; $C_L = 0.360$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.176	.430	0.000	1.098	.992	0.000	.091	.743	.050	-1.138	.439
.150	-1.341	.389	.012	-.231	.664	.012	-.367	.630	.150	-1.208	.422
.300	-.732	.527	.025	-.752	.535	.025	-.593	.574	.300	-.745	.537
.450	-.624	.566	.050	-1.163	.433	.050	-1.131	.441	.450	-.626	.566
.600	-.592	.574	.100	-1.362	.384	.100	-1.268	.407	.600	-.603	.572
.800	-.352	.631	.150	-1.280	.404	.150	-1.272	.406	.800	-.372	.629
.990	.049	.733	.200	-1.309	.397	.200	-.957	.484			
			.300	-.758	.533	.300	-.852	.510			
			.350	-.766	.531	.350	-.769	.531			
			.400	-.762	.533	.400	-.724	.542			
			.450	-.751	.535	.450	-.740	.538			
			.500	-.743	.532	.500	-.764	.532			
			.550	-.737	.539	.550	-.722	.542			
			.600	-.693	.550	.600	-.671	.555			
			.650	-.659	.558	.700	-.463	.606			
			.700	-.578	.578	.800	-.234	.663			
			.800	-.334	.638	.900	-.135	.687			
			.900	-.051	.708	.950	-.126	.690			
			.950	.018	.725	.990	-.126	.690			
			.990	.061	.736						
					LOWER SURFACE						
.100	-.348	.635	.025	-.021	.716	.025	.115	.749	.100	-.705	.546
.300	-.582	.577	.050	-.391	.624	.050	-.459	.607	.300	-.578	.578
.600	-.391	.649	.100	-.471	.604	.100	-.527	.591	.600	-.312	.644
.800	.171	.763	.200	-.604	.571	.200	-.560	.582	.800	.245	.781
			.300	-.646	.561	.300	-.640	.563			
			.400	-.625	.566	.400	-.627	.566			
			.500	-.611	.570	.500	-.533	.589			
			.600	-.260	.656	.600	-.269	.654			
			.700	.073	.739	.700	.061	.736			
			.800	.239	.780	.800	.310	.757			
			.900	.341	.805	.900	.350	.807			
			.950	.341	.805	.950	.352	.808			
			1.000	.056	.735						
CN=				.4215			.4215				
CM=				-.0975			-.1026				

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = 1.27^o$; $C_L = 0.497$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.319	.395	0.000	1.084	.989	0.000	.088	.743	.050	-1.310	.397
.150	-1.463	.359	.012	-.414	.619	.012	-.481	.602	.150	-1.564	.334
.300	-.743	.537	.025	-.923	.493	.025	-.702	.548	.300	-.694	.550
.450	-.642	.562	.050	-1.290	.405	.050	-1.262	.409	.450	-.619	.568
.600	-.603	.572	.100	-1.523	.345	.100	-1.447	.363	.600	-.615	.569
.800	-.379	.627	.150	-1.455	.361	.150	-1.407	.373	.800	-.389	.625
.990	.057	.735	.200	-1.460	.360	.200	-1.404	.374			
			.300	-1.141	.439	.300	-1.116	.445			
			.350	-.692	.550	.350	-.689	.551			
			.400	-.652	.560	.400	-.642	.562			
			.450	-.700	.548	.450	-.685	.552			
			.500	-.718	.544	.500	-.746	.537			
			.550	-.712	.545	.550	-.713	.545			
			.600	-.685	.552	.600	-.687	.551			
			.650	-.654	.560	.700	-.499	.598			
			.700	-.594	.577	.800	-.268	.655			
			.800	-.352	.634	.900	-.125	.690			
			.900	-.056	.707	.950	-.118	.692			
			.950	.028	.728	.990	-.119	.692			
			.990	.063	.737						
					LOWER SURFACE						
.100	-.237	.648	.025	.124	.752	.025	.229	.778	.100	-.572	.580
.300	-.434	.599	.050	-.191	.674	.050	-.286	.650	.300	-.534	.589
.600	-.234	.651	.100	-.380	.627	.100	-.412	.619	.600	-.293	.649
.800	.201	.771	.200	-.486	.601	.200	-.485	.601	.800	.279	.790
			.300	-.570	.580	.300	-.559	.583			
			.400	-.561	.582	.400	-.582	.577			
			.500	-.577	.579	.500	-.490	.600			
			.600	-.242	.661	.600	-.244	.661			
			.700	.095	.745	.700	.084	.742			
			.800	.283	.791	.800	.344	.806			
			.900	.368	.812	.900	.370	.813			
			.950	.358	.810	.950	.368	.812			
			1.000	.079	.740						
CN=				.5284			.5496				
CM=				-.0975			-.1030				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = 2.22^o$; $C_L = 0.618$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.478	.355	0.000	1.067	.985	0.000	.094	.744	.050	-1.417	.370
.150	-1.603	.324	.012	-.497	.598	.012	-.595	.574	.150	-1.685	.306
.300	-1.445	.363	.025	-1.041	.463	.025	-.843	.512	.300	-.741	.537
.450	-.597	.573	.050	-1.389	.377	.050	-1.384	.379	.450	-.602	.572
.600	-.579	.578	.100	-1.647	.313	.100	-1.580	.330	.600	-.594	.574
.800	-.382	.626	.150	-1.570	.332	.150	-1.581	.330	.800	-.394	.623
.990	.053	.736	.200	-1.577	.331	.200	-1.530	.342			
			.300	-1.576	.331	.300	-1.521	.344			
			.350	-1.506	.348	.350	-1.453	.361			
			.400	-.922	.493	.400	-.827	.516			
			.450	-.648	.561	.450	-.685	.551			
			.500	-.682	.552	.500	-.643	.562			
			.550	-.668	.556	.550	-.651	.560			
			.600	-.633	.564	.600	-.642	.562			
			.650	-.615	.569	.700	-.504	.596			
			.700	-.572	.579	.800	-.314	.643			
			.800	-.350	.634	.900	-.100	.696			
			.900	-.072	.703	.950	-.069	.704			
			.950	.032	.729	.990	-.050	.708			
			.990	.095	.744						
					LOWER SURFACE						
.100	-.132	.688	.025	.240	.780	.025	.353	.808	.100	-.456	.668
.300	-.447	.610	.050	-.073	.703	.050	-.122	.691	.300	-.483	.601
.600	-.267	.655	.100	-.260	.657	.100	-.291	.649	.600	-.292	.649
.800	.230	.778	.200	-.385	.626	.200	-.417	.618	.800	.274	.789
			.300	-.483	.601	.300	-.508	.595			
			.400	-.495	.598	.400	-.530	.590			
			.500	-.528	.590	.500	-.455	.608			
			.600	-.220	.666	.600	-.236	.662			
			.700	.112	.748	.700	.083	.741			
			.800	.295	.794	.800	.354	.808			
			.900	.385	.816	.900	.389	.817			
			.950	.369	.812	.950	.397	.819			
			1.000	.101	.746						
CN=				.6961			.6946				
CM=				-.1023			-.1017				

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = 2.65^o$; $C_L = 0.677$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.506	.349	0.000	1.042	.979	0.000	.092	.744	.050	-1.461	.361
.150	-1.655	.313	.012	-.543	.587	.012	-.660	.558	.150	-1.719	.297
.300	-1.543	.340	.025	-1.082	.454	.025	-.900	.499	.300	-1.070	.457
.450	-.579	.578	.050	-1.464	.360	.050	-1.410	.373	.450	-.597	.574
.600	-.574	.580	.100	-1.686	.305	.100	-1.595	.327	.600	-.589	.576
.800	-.373	.629	.150	-1.618	.322	.150	-1.621	.321	.800	-.393	.624
.990	.071	.739	.200	-1.632	.318	.200	-1.566	.335			
			.300	-1.653	.313	.300	-1.590	.329			
			.350	-1.596	.327	.350	-1.541	.341			
			.400	-.937	.490	.400	-.974	.481			
			.450	-.721	.543	.450	-.710	.546			
			.500	-.627	.567	.500	-.629	.566			
			.550	-.584	.577	.550	-.623	.568			
			.600	-.600	.573	.600	-.614	.570			
			.650	-.596	.574	.700	-.509	.596			
			.700	-.547	.586	.800	-.326	.641			
			.800	-.351	.635	.900	-.095	.698			
			.900	-.075	.703	.950	-.065	.705			
			.950	.038	.731	.990	-.040	.712			
			.990	.106	.747						
					LOWER SURFACE						
.100	-.144	.686	.025	.271	.788	.025	.405	.821	.100	-.400	.623
.300	-.421	.617	.050	-.041	.711	.050	-.088	.700	.300	-.470	.605
.600	-.257	.658	.100	-.196	.673	.100	-.253	.659	.600	-.276	.653
.800	.233	.779	.200	-.346	.636	.200	-.370	.630	.800	.257	.765
			.300	-.443	.612	.300	-.453	.609			
			.400	-.468	.606	.400	-.499	.598			
			.500	-.520	.593	.500	-.438	.613			
			.600	-.214	.668	.600	-.214	.669			
			.700	.123	.752	.700	.100	.746			
			.800	.299	.795	.800	.370	.813			
			.900	.411	.823	.900	.399	.820			
			.950	.382	.816	.950	.406	.821			
			1.000	.114	.749						
CN=				.7324			.7465				
CM=				-.0990			-.1048				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 3^o$; $\alpha = 3.84^o$; $C_L = 0.804$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.724	.294	0.000	1.007	.970	0.000	.092	.744	.050	-1.631	.317
.150	-1.769	.285	.012	-.672	.555	.012	-.799	.523	.150	-1.877	.256
.300	-1.666	.309	.025	-1.221	.419	.025	-1.045	.462	.300	-1.565	.336
.450	-.778	.528	.050	-1.597	.326	.050	-1.546	.338	.450	-.590	.575
.600	-.510	.595	.100	-1.813	.272	.100	-1.734	.292	.600	-.567	.581
.800	-.339	.637	.150	-1.753	.287	.150	-1.746	.289	.800	-.339	.637
.990	.074	.739	.200	-1.760	.285	.200	-1.699	.301			
			.300	-1.745	.289	.300	-1.729	.293			
			.350	-1.727	.294	.350	-1.725	.294			
			.400	-1.113	.446	.400	-1.467	.358			
			.450	-1.043	.463	.450	-.999	.474			
			.500	-.971	.481	.500	-.885	.502			
			.550	-.832	.515	.550	-.709	.545			
			.600	-.704	.547	.600	-.586	.576			
			.650	-.556	.583	.700	-.459	.607			
			.700	-.401	.622	.800	-.334	.638			
			.800	-.240	.662	.900	-.095	.697			
			.900	-.071	.703	.950	-.023	.715			
			.950	.013	.724	.990	.013	.724			
			.990	-.003	.720						
					LOWER SURFACE						
.100	.023	.725	.025	.423	.828	.025	.510	.847	.100	-.272	.653
.300	-.363	.631	.050	.117	.750	.050	.057	.735	.300	-.429	.616
.600	-.249	.659	.100	-.101	.696	.100	-.133	.688	.600	-.276	.653
.800	.247	.782	.200	-.258	.657	.200	-.280	.652	.800	-.288	.792
			.300	-.368	.630	.300	-.400	.622			
			.400	-.438	.612	.400	-.460	.607			
			.500	-.471	.604	.500	-.401	.622			
			.600	-.190	.674	.600	-.206	.670			
			.700	.122	.751	.700	.109	.748			
			.800	.311	.798	.800	.378	.814			
			.900	.381	.815	.900	.408	.822			
			.950	.379	.815	.950	.418	.824			
			1.000	-.030	.713						
CN=				.8547			.8906				
CM=				-.0958			-.1081				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 8^o$; $\alpha = -4.59^o$; $C_L = -0.186$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.325	.641	0.000	1.083	.989	0.000	.079	.741	.050	-.277	.653
.150	-.477	.603	.012	.420	.825	.012	.424	.826	.150	-.431	.615
.300	-.516	.594	.025	.052	.734	.025	.111	.749	.300	-.514	.594
.450	-.456	.608	.050	-.282	.652	.050	-.258	.658	.450	-.506	.596
.600	-.528	.591	.100	-.406	.621	.100	-.387	.626	.600	-.561	.583
.800	-.415	.619	.150	-.463	.607	.150	-.388	.625	.800	-.392	.624
.990	.079	.741	.200	-.511	.595	.200	-.489	.600			
			.300	-.541	.588	.300	-.540	.588			
			.350	-.548	.586	.350	-.522	.592			
			.400	-.533	.590	.400	-.524	.592			
			.450	-.520	.593	.450	-.567	.581			
			.500	-.627	.566	.500	-.613	.570			
			.550	-.618	.569	.550	-.612	.570			
			.600	-.565	.582	.600	-.605	.572			
			.650	-.613	.570	.700	-.450	.610			
			.700	-.583	.577	.800	-.205	.671			
			.800	-.381	.627	.900	-.159	.682			
			.900	-.056	.707	.950	-.159	.682			
			.950	.050	.734	.990	-.157	.683			
			.990	.105	.747						
					LOWER SURFACE						
.100	-1.207	.423	.025	-.640	.563	.025	-.572	.580	.100	-1.576	.332
.300	-.789	.526	.050	-1.278	.405	.050	-1.177	.430	.300	-.605	.572
.600	-.280	.652	.100	-1.418	.371	.100	-1.461	.360	.600	-.257	.658
.800	.074	.740	.200	-1.392	.377	.200	-1.465	.359	.800	.192	.769
			.300	-.757	.534	.300	-.849	.511			
			.400	-.713	.545	.400	-.614	.570			
			.500	-.684	.552	.500	-.528	.591			
			.600	-.293	.649	.600	-.226	.665			
			.700	.037	.730	.700	.084	.742			
			.800	.212	.774	.800	.277	.790			
			.900	.298	.795	.900	.296	.794			
			.950	.301	.796	.950	.298	.795			
			1.000	.116	.750						
CN=				-.1154			-.0713				
CM=				-.1277			-.1395				

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = -2.99^o$; $C_L = -0.016$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.583	.577	0.000	1.116	.997	0.000	.081	.741	.050	-.564	.582
.150	-.658	.559	.012	.259	.785	.012	.195	.769	.150	-.607	.571
.300	-.616	.569	.025	-.225	.666	.025	-.102	.696	.300	-.593	.575
.450	-.526	.591	.050	-.548	.586	.050	-.545	.587	.450	-.554	.585
.600	-.551	.585	.100	-.632	.565	.100	-.578	.579	.600	-.587	.576
.800	-.390	.625	.150	-.622	.568	.150	-.548	.586	.800	-.389	.625
.990	.071	.739	.200	-.654	.560	.200	-.616	.569			
			.300	-.650	.561	.300	-.656	.559			
			.350	-.618	.569	.350	-.607	.571			
			.400	-.618	.569	.400	-.603	.572			
			.450	-.599	.573	.450	-.628	.566			
			.500	-.665	.557	.500	-.671	.556			
			.550	-.663	.558	.550	-.656	.559			
			.600	-.612	.570	.600	-.636	.564			
			.650	-.629	.566	.700	-.445	.611			
			.700	-.586	.577	.800	-.202	.672			
			.800	-.356	.633	.900	-.161	.681			
			.900	-.047	.710	.950	-.163	.681			
			.950	.038	.731	.990	-.165	.681			
			.990	.082	.741						
					LOWER SURFACE						
.100	-.850	.511	.025	-.453	.609	.025	-.385	.626	.100	-1.406	.374
.300	-.760	.533	.050	-.921	.494	.050	-.927	.492	.300	-.654	.560
.600	-.288	.650	.100	-1.145	.438	.100	-1.258	.410	.600	-.247	.660
.800	.089	.743	.200	-.941	.489	.200	-.857	.510	.800	.174	.764
			.300	-.854	.510	.300	-.814	.520			
			.400	-.756	.535	.400	-.705	.547			
			.500	-.683	.553	.500	-.538	.588			
			.600	-.271	.654	.600	-.207	.670			
			.700	.035	.730	.700	.065	.737			
			.800	.152	.759	.800	.223	.776			
			.900	.263	.786	.900	.292	.793			
			.950	.302	.796	.950	.313	.799			
			1.000	.098	.745						
CN=				.0222			.0822				
CM=				-.1101			-.1238				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = -1.30^o$; $C_L = 0.190$

STATION .1592 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.943	.488	0.000	1.113	.996	0.000	.089	.743	.050	-.913	.495
.150	-.827	.517	.012	.002	.722	.012	-.051	.709	.150	-.785	.527
.300	-.731	.540	.025	-.499	.598	.025	-.374	.629	.300	-.711	.545
.450	-.530	.578	.050	-.877	.504	.050	-.841	.513	.450	-.603	.572
.600	-.582	.577	.100	-.938	.489	.100	-.876	.505	.600	-.605	.572
.800	-.396	.623	.150	-.809	.521	.150	-.750	.536	.800	-.386	.626
.990	.048	.733	.200	-.864	.508	.200	-.817	.519			
			.300	-.781	.528	.300	-.797	.524			
			.350	-.736	.539	.350	-.712	.545			
			.400	-.716	.544	.400	-.680	.553			
			.450	-.725	.542	.450	-.705	.547			
			.500	-.741	.538	.500	-.732	.540			
			.550	-.719	.543	.550	-.705	.547			
			.600	-.664	.557	.600	-.667	.556			
			.650	-.666	.557	.700	-.455	.609			
			.700	-.594	.574	.800	-.218	.667			
			.800	-.354	.634	.900	-.178	.677			
			.900	-.054	.708	.950	-.177	.677			
			.950	.019	.726	.990	-.178	.677			
			.990	.058	.736						
					LOWER SURFACE						
.100	-.637	.564	.025	-.192	.674	.025	-.084	.700	.100	-.965	.483
.300	-.657	.556	.050	-.631	.565	.050	-.712	.545	.300	-.641	.563
.600	-.293	.649	.100	-.725	.542	.100	-.718	.544	.600	-.251	.659
.800	.150	.758	.200	-.757	.534	.200	-.737	.539	.800	.238	.780
			.300	-.744	.537	.300	-.741	.538			
			.400	-.665	.557	.400	-.663	.557			
			.500	-.642	.563	.500	-.520	.593			
			.600	-.271	.654	.600	-.205	.670			
			.700	.053	.734	.700	.109	.748			
			.800	.231	.778	.800	.299	.795			
			.900	.345	.806	.900	.347	.807			
			.950	.343	.806	.950	.342	.806			
			1.000	.072	.739						
CN=				.2477			.2825				
CM=				-.1128			-.1235				

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = 0.40^o$; $C_L = 0.390$

STATION .1592 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.233	.417	0.000	1.091	.991	0.000	.093	.744	.050	-1.167	.433
.150	-1.347	.389	.012	-.243	.661	.012	-.356	.633	.150	-1.327	.393
.300	-.756	.535	.025	-.771	.531	.025	-.664	.557	.300	-.747	.537
.450	-.636	.564	.050	-1.196	.426	.050	-1.159	.435	.450	-.640	.563
.600	-.604	.572	.100	-1.445	.365	.100	-1.357	.386	.600	-.628	.566
.800	-.387	.626	.150	-1.377	.381	.150	-1.319	.396	.800	-.402	.622
.990	.042	.732	.200	-1.364	.385	.200	-1.230	.418			
			.300	-.743	.538	.300	-.794	.525			
			.350	-.753	.535	.350	-.764	.533			
			.400	-.754	.535	.400	-.730	.541			
			.450	-.755	.535	.450	-.757	.534			
			.500	-.790	.526	.500	-.786	.527			
			.550	-.746	.537	.550	-.744	.538			
			.600	-.697	.549	.600	-.697	.549			
			.650	-.659	.559	.700	-.475	.604			
			.700	-.590	.575	.800	-.231	.664			
			.800	-.349	.635	.900	-.183	.676			
			.900	-.057	.707	.950	-.181	.677			
			.950	.009	.724	.990	-.185	.676			
			.990	.044	.732						
					LOWER SURFACE						
.100	-.361	.632	.025	.029	.728	.025	.128	.753	.100	-.662	.558
.300	-.557	.584	.050	-.376	.641	.050	-.427	.616	.300	-.561	.583
.600	-.289	.650	.100	-.471	.605	.100	-.508	.596	.600	-.258	.658
.800	.171	.764	.200	-.553	.585	.200	-.548	.586	.800	.301	.796
			.300	-.587	.576	.300	-.612	.570			
			.400	-.598	.574	.400	-.590	.576			
			.500	-.604	.572	.500	-.474	.604			
			.600	-.247	.660	.600	-.199	.672			
			.700	.079	.741	.700	.133	.754			
			.800	.248	.788	.800	.343	.806			
			.900	.375	.814	.900	.368	.812			
			.950	.356	.809	.950	.350	.808			
			1.000	.069	.738						
CN=				.4632			.4958				
CM=				-.1038			-.1168				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = 2.36^o$; $C_L = 0.655$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.524	.345	0.000	1.057	.982	0.000	.096	.745	.050	-1.482	.355
.150	-1.600	.326	.012	-.524	.592	.012	-.615	.569	.150	-1.730	.294
.300	-1.497	.352	.025	-1.103	.449	.025	-.890	.501	.300	-.964	.483
.450	-.598	.574	.050	-1.419	.371	.050	-1.403	.375	.450	-.617	.569
.600	-.586	.576	.100	-1.657	.312	.100	-1.599	.326	.600	-.621	.568
.800	-.394	.624	.150	-1.637	.317	.150	-1.593	.328	.800	-.439	.613
.990	.063	.737	.200	-1.630	.319	.200	-1.552	.338			
			.300	-1.601	.326	.300	-1.568	.334			
			.350	-1.563	.335	.350	-1.565	.335			
			.400	-1.055	.461	.400	-.910	.497			
			.450	-.746	.537	.450	-.721	.543			
			.500	-.617	.569	.500	-.645	.562			
			.550	-.617	.569	.550	-.651	.561			
			.600	-.624	.567	.600	-.635	.564			
			.650	-.606	.572	.700	-.513	.595			
			.700	-.574	.580	.800	-.277	.653			
			.800	-.366	.631	.900	-.147	.685			
			.900	-.082	.701	.950	-.140	.687			
			.950	.027	.728	.990	-.143	.686			
			.990	.097	.745						
					LOWER SURFACE						
.100	-.167	.680	.025	.267	.787	.025	.377	.814	.100	-.404	.622
.300	-.440	.613	.050	-.055	.708	.050	-.098	.697	.300	-.443	.607
.600	-.264	.656	.100	-.221	.667	.100	-.252	.659	.600	-.232	.644
.800	.234	.779	.200	-.385	.626	.200	-.384	.627	.800	.334	.804
			.300	-.458	.608	.300	-.464	.607			
			.400	-.484	.602	.400	-.495	.599			
			.500	-.517	.594	.500	-.417	.619			
			.600	-.200	.672	.600	-.169	.680			
			.700	.113	.749	.700	.161	.761			
			.800	.319	.800	.800	.400	.820			
			.900	.408	.822	.900	.405	.821			
			.950	.394	.819	.950	.398	.820			
			1.000	.103	.747						
CN=				.7336			.7623				
CM=				-.1061			-.1177				

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = 3.93^o$; $C_L = 0.834$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.713	.298	0.000	1.000	.968	0.000	.095	.745	.050	-1.637	.317
.150	-1.786	.280	.012	-.706	.547	.012	-.813	.520	.150	-1.890	.254
.300	-1.668	.309	.025	-1.251	.412	.025	-1.073	.456	.300	-1.716	.297
.450	-.790	.526	.050	-1.603	.325	.050	-1.548	.339	.450	-.663	.558
.600	-.508	.596	.100	-1.814	.273	.100	-1.754	.288	.600	-.616	.569
.800	-.356	.633	.150	-1.754	.288	.150	-1.739	.292	.800	-.462	.607
.990	.071	.739	.200	-1.784	.281	.200	-1.722	.296			
			.300	-1.769	.284	.300	-1.758	.287			
			.350	-1.468	.359	.350	-1.739	.292			
			.400	-1.208	.423	.400	-1.665	.310			
			.450	-1.079	.455	.450	-1.061	.459			
			.500	-1.012	.471	.500	-.938	.489			
			.550	-.833	.516	.550	-.794	.525			
			.600	-.645	.562	.600	-.656	.559			
			.650	-.484	.602	.700	-.493	.600			
			.700	-.416	.618	.800	-.324	.641			
			.800	-.273	.654	.900	-.130	.689			
			.900	-.072	.704	.950	-.081	.701			
			.950	.006	.723	.990	-.061	.706			
			.990	.066	.738						
					LOWER SURFACE						
.100	-.007	.720	.025	.403	.821	.025	.554	.858	.100	-.242	.661
.300	-.336	.638	.050	.118	.750	.050	.061	.736	.300	-.386	.626
.600	-.238	.662	.100	-.078	.702	.100	-.104	.695	.600	-.214	.668
.800	.256	.784	.200	-.250	.659	.200	-.247	.660	.800	.346	.807
			.300	-.357	.633	.300	-.357	.633			
			.400	-.401	.622	.400	-.416	.618			
			.500	-.446	.611	.500	-.341	.637			
			.600	-.172	.679	.600	-.136	.688			
			.700	.137	.755	.700	.181	.766			
			.800	.333	.804	.800	.428	.827			
			.900	.428	.827	.900	.430	.828			
			.950	.390	.818	.950	.416	.824			
			1.000	.008	.723						
CN=				.8759			.9744				
CM=				-.1051			-.1307				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\delta_a = 6^o$; $\alpha = 5.05^o$; $C_L = 0.884$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.857	.263	0.000	.962	.959	0.000	.088	.743	.050	-1.746	.290
.150	-1.906	.251	.012	-.808	.522	.012	-.969	.482	.150	-1.890	.254
.300	-1.540	.341	.025	-1.342	.390	.025	-1.250	.413	.300	-1.744	.291
.450	-.901	.499	.050	-1.689	.304	.050	-1.631	.319	.450	-.678	.556
.600	-.477	.604	.100	-1.894	.254	.100	-1.846	.266	.600	-.606	.572
.800	-.292	.649	.150	-1.845	.266	.150	-1.838	.267	.800	-.484	.602
.990	-.030	.714	.200	-1.861	.262	.200	-1.798	.278			
			.300	-1.329	.393	.300	-1.821	.272			
			.350	-1.247	.414	.350	-1.514	.347			
			.400	-1.147	.438	.400	-1.194	.427			
			.450	-1.153	.437	.450	-1.090	.452			
			.500	-.795	.525	.500	-.923	.454			
			.550	-.843	.513	.550	-.800	.524			
			.600	-.702	.548	.600	-.648	.561			
			.650	-.489	.601	.700	-.467	.606			
			.700	-.502	.598	.800	-.306	.646			
			.800	-.242	.662	.900	-.206	.670			
			.900	-.145	.686	.950	-.160	.682			
			.950	-.107	.695	.990	-.131	.689			
			.990	-.143	.686						
					LOWER SURFACE						
.100	.045	.732	.025	.515	.849	.025	.617	.874	.100	-.165	.681
.300	-.313	.644	.050	.216	.775	.050	.178	.765	.300	-.354	.634
.600	-.248	.660	.100	-.002	.721	.100	-.017	.717	.600	-.208	.670
.800	.283	.791	.200	-.202	.672	.200	-.180	.677	.800	.352	.808
			.300	-.313	.644	.300	-.318	.643			
			.400	-.388	.626	.400	-.386	.626			
			.500	-.471	.605	.500	-.345	.636			
			.600	-.194	.673	.600	-.140	.687			
			.700	.108	.748	.700	.178	.765			
			.800	.326	.802	.800	.430	.828			
			.900	.399	.820	.900	.425	.826			
			.950	.371	.813	.950	.405	.821			
			1.000	-.074	.703						
CN=				.8636			1.0010				
CM=				-.1010			-.1251				

(e) M = 0.70. Concluded.

$\delta_a = 6^o$; $\alpha = 5.41^o$; $C_L = 0.895$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.976	.258	0.000	.948	.955	0.000	.081	.741	.050	-1.759	.287
.150	-1.911	.249	.012	-.799	.524	.012	-1.013	.471	.150	-1.300	.400
.300	-.992	.476	.025	-1.358	.386	.025	-1.322	.395	.300	-1.669	.309
.450	-.865	.508	.050	-1.739	.292	.050	-1.674	.308	.450	-.692	.550
.600	-.471	.605	.100	-1.914	.249	.100	-1.859	.262	.600	-.609	.571
.800	-.258	.655	.150	-1.834	.268	.150	-1.870	.259	.800	-.490	.600
.990	-.062	.706	.200	-1.591	.328	.200	-1.837	.268			
			.300	-1.282	.405	.300	-1.446	.364			
			.350	-1.257	.411	.350	-1.325	.394			
			.400	-1.202	.425	.400	-1.198	.426			
			.450	-.836	.515	.450	-1.126	.443			
			.500	-1.011	.472	.500	-1.027	.468			
			.550	-.852	.511	.550	-.808	.522			
			.600	-.781	.528	.600	-.682	.553			
			.650	-.589	.576	.700	-.448	.611			
			.700	-.494	.599	.800	-.307	.646			
			.800	-.274	.654	.900	-.201	.672			
			.900	-.147	.685	.950	-.174	.678			
			.950	-.095	.698	.990	-.136	.688			
			.990	-.219	.667						
					LOWER SURFACE						
.100	.057	.735	.025	.533	.853	.025	.659	.884	.100	-.117	.692
.300	-.310	.645	.050	.243	.781	.050	.198	.770	.300	-.346	.636
.600	-.277	.653	.100	.044	.732	.100	.005	.723	.600	-.208	.670
.800	.237	.780	.200	-.181	.677	.200	-.183	.676	.800	.356	.809
			.300	-.310	.645	.300	-.306	.646			
			.400	-.368	.630	.400	-.384	.626			
			.500	-.464	.607	.500	-.337	.638			
			.600	-.198	.672	.600	-.142	.686			
			.700	.112	.749	.700	.175	.765			
			.800	.326	.802	.800	.427	.827			
			.900	.383	.816	.900	.420	.825			
			.950	.350	.808	.950	.404	.821			
			1.000	-.064	.705						
CN=				.8849			.9859				
CM=				-.1097			-.1227				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73

$\delta_a = -6^o$; $\alpha = -4.89^o$; $C_L = -0.291$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.287	.626	0.000	1.056	.588	0.000	.038	.725	.050	-.208	.647
.150	-.456	.582	.012	.469	.624	.012	.449	.819	.150	-.421	.591
.300	-.499	.571	.025	.143	.739	.025	.161	.744	.300	-.514	.567
.450	-.415	.593	.050	-.231	.641	.050	-.231	.641	.450	-.485	.574
.600	-.525	.564	.100	-.362	.607	.100	-.342	.612	.600	-.473	.578
.800	-.384	.601	.150	-.427	.590	.150	-.352	.609	.800	-.223	.643
.950	.078	.722	.200	-.512	.567	.200	-.440	.586			
			.300	-.539	.560	.300	-.525	.564			
			.350	-.514	.567	.350	-.505	.569			
			.400	-.527	.563	.400	-.493	.572			
			.450	-.502	.570	.450	-.539	.560			
			.500	-.598	.545	.500	-.584	.549			
			.550	-.639	.542	.550	-.558	.555			
			.600	-.538	.561	.600	-.530	.563			
			.650	-.609	.542	.700	-.305	.622			
			.700	-.560	.555	.800	-.215	.645			
			.800	-.338	.613	.900	-.046	.689			
			.900	-.023	.655	.950	.059	.717			
			.950	.078	.722	.990	.139	.738			
			.990	.113	.731						
					LOWER SURFACE						
.100	-1.038	.430	.025	-.579	.550	.025	-.504	.569	.100	-1.517	.304
.300	-1.352	.347	.050	-1.210	.385	.050	-1.112	.410	.300	-1.513	.305
.600	-.256	.634	.100	-1.322	.355	.100	-1.379	.340	.600	-.407	.595
.800	.050	.715	.200	-1.398	.338	.200	-1.447	.323	.800	.013	.705
			.300	-1.439	.325	.300	-1.523	.303			
			.400	-1.017	.435	.400	-1.477	.315			
			.500	-.640	.534	.500	-.691	.521			
			.600	-.322	.617	.600	-.321	.617			
			.700	-.150	.662	.700	-.099	.675			
			.800	.039	.712	.800	.131	.736			
			.900	.140	.738	.900	.209	.756			
			.950	.170	.746	.950	.247	.766			
			1.000	.142	.739						
CN=				-.2792			-.3674				
CM=				-.0757			-.0630				

(f) M = 0.73. Continued.

$\delta_a = -6^o$; $\alpha = -3.28^o$; $C_L = -0.112$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.522	.565	0.000	1.114	.593	0.000	.087	.725	.050	-.425	.590
.150	-.633	.536	.012	.338	.790	.012	.261	.770	.150	-.547	.558
.300	-.614	.541	.025	-.085	.679	.025	-.019	.696	.300	-.595	.545
.450	-.477	.576	.050	-.450	.584	.050	-.408	.594	.450	-.528	.563
.600	-.551	.557	.100	-.560	.555	.100	-.523	.564	.600	-.486	.574
.800	-.372	.604	.150	-.588	.547	.150	-.501	.570	.800	-.212	.646
.950	.076	.721	.200	-.633	.536	.200	-.586	.548			
			.300	-.658	.529	.300	-.615	.540			
			.350	-.620	.539	.350	-.589	.547			
			.400	-.620	.539	.400	-.568	.553			
			.450	-.572	.551	.450	-.603	.543			
			.500	-.686	.522	.500	-.637	.534			
			.550	-.659	.529	.550	-.593	.546			
			.600	-.577	.550	.600	-.544	.559			
			.650	-.630	.536	.700	-.298	.623			
			.700	-.563	.554	.800	-.208	.647			
			.800	-.310	.620	.900	-.030	.693			
			.900	-.010	.699	.950	.076	.721			
			.950	.066	.719	.990	.150	.741			
			.990	.104	.729						
					LOWER SURFACE						
.100	-.861	.476	.025	-.441	.586	.025	-.349	.610	.100	-1.361	.345
.300	-1.061	.423	.050	-1.025	.433	.050	-.911	.463	.300	-1.332	.353
.600	-.256	.634	.100	-1.150	.400	.100	-1.224	.381	.600	-.448	.584
.800	.062	.718	.200	-1.202	.387	.200	-1.225	.381	.800	.054	.715
			.300	-1.270	.369	.300	-1.307	.359			
			.400	-.922	.460	.400	-1.346	.349			
			.500	-.657	.529	.500	-.567	.553			
			.600	-.259	.634	.600	-.396	.598			
			.700	.051	.715	.700	-.101	.675			
			.800	.178	.748	.800	.163	.744			
			.900	.301	.780	.900	.255	.768			
			.950	.294	.778	.950	.414	.784			
			1.000	.118	.732						
CN=				-.0760			-.1883				
CM=				-.1080			-.0640				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -6^o$; $\alpha = -1.71^o$; $C_L = 0.071$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.752	.504	0.000	1.113	.953	0.000	.093	.726	.050	-.693	.520
.150	-.424	.459	.012	.107	.729	.012	.040	.712	.150	-.779	.497
.300	-.708	.516	.025	-.347	.610	.025	-.234	.640	.300	-.696	.519
.450	-.555	.556	.050	-.745	.506	.050	-.715	.514	.450	-.569	.552
.600	-.568	.553	.100	-.905	.463	.100	-.765	.501	.600	-.494	.572
.800	-.356	.604	.150	-.752	.504	.150	-.701	.518	.800	-.199	.649
.950	.067	.719	.200	-.874	.477	.200	-.762	.502			
			.300	-.785	.496	.300	-.805	.490			
			.350	-.724	.512	.350	-.671	.525			
			.400	-.672	.525	.400	-.629	.537			
			.450	-.646	.532	.450	-.658	.529			
			.500	-.741	.507	.500	-.687	.521			
			.550	-.693	.520	.550	-.625	.538			
			.600	-.617	.540	.600	-.563	.554			
			.650	-.632	.536	.700	-.305	.621			
			.700	-.551	.557	.800	-.206	.647			
			.800	-.291	.625	.900	-.024	.695			
			.900	-.009	.699	.950	.079	.722			
			.950	.043	.713	.990	.146	.740			
			.990	.082	.723						
					LOWER SURFACE						
.100	-.604	.542	.025	-.256	.634	.025	-.165	.658	.100	-1.168	.395
.300	-.816	.488	.050	-.729	.510	.050	-.759	.502	.300	-.628	.537
.600	-.276	.629	.100	-.908	.463	.100	-1.037	.430	.600	-.454	.582
.800	.096	.727	.200	-.875	.472	.200	-.934	.457	.800	.042	.712
			.300	-.976	.446	.300	-1.075	.420			
			.400	-.931	.492	.400	-.815	.488			
			.500	-.714	.514	.500	-.751	.505			
			.600	-.252	.635	.600	-.434	.587			
			.700	.040	.712	.700	-.117	.671			
			.800	.138	.737	.800	.151	.741			
			.900	.265	.771	.900	.235	.763			
			.950	.306	.781	.950	.306	.781			
			1.000	.059	.727						
CN=				.1107			.0020				
CM=				-.0937			-.0548				

(f) M = 0.73. Continued.

$\delta_a = -6^o$; $\alpha = 0.22^o$; $C_L = 0.316$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.098	.414	0.000	1.122	.955	0.000	.098	.727	.050	-1.030	.432
.150	-1.213	.384	.012	-.106	.674	.012	-.202	.649	.150	-1.319	.356
.300	-.964	.449	.025	-.611	.542	.025	-.494	.575	.300	-.691	.521
.450	-.594	.546	.050	-1.005	.428	.050	-.993	.442	.450	-.584	.549
.600	-.582	.549	.100	-1.234	.373	.100	-1.172	.395	.600	-.498	.571
.800	-.364	.606	.150	-1.189	.390	.150	-1.163	.397	.800	-.196	.650
.950	.066	.719	.200	-1.239	.377	.200	-1.153	.400			
			.300	-1.184	.392	.300	-1.182	.392			
			.350	-1.128	.406	.350	-.864	.476			
			.400	-.689	.521	.400	-.599	.545			
			.450	-.581	.550	.450	-.653	.531			
			.500	-.677	.524	.500	-.665	.528			
			.550	-.656	.519	.550	-.618	.540			
			.600	-.660	.529	.600	-.565	.554			
			.650	-.615	.540	.700	-.308	.621			
			.700	-.557	.553	.800	-.208	.647			
			.800	-.321	.618	.900	-.027	.694			
			.900	-.030	.694	.950	.072	.720			
			.950	.052	.715	.990	.136	.737			
			.990	.079	.727						
					LOWER SURFACE						
.100	-.325	.617	.025	.005	.704	.025	.093	.726	.100	-.876	.472
.300	-.622	.533	.050	-.420	.592	.050	-.507	.569	.300	-.701	.518
.600	-.275	.630	.100	-.567	.553	.100	-.610	.542	.600	-.482	.575
.800	.145	.740	.200	-.681	.523	.200	-.685	.522	.800	.089	.725
			.300	-.735	.509	.300	-.861	.476			
			.400	-.732	.510	.400	-.755	.504			
			.500	-.692	.521	.500	-.754	.504			
			.600	-.257	.634	.600	-.436	.587			
			.700	.070	.720	.700	-.120	.670			
			.800	.213	.757	.800	.171	.746			
			.900	.320	.785	.900	.253	.768			
			.950	.338	.790	.950	.322	.786			
			1.000	.094	.726						
CN=				.3666			.2379				
CM=				-.0925			-.0407				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -6^o$; $\alpha = 2.18^o$; $C_L = 0.583$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.321	.355	0.000	1.095	.589	0.000	.101	.727	.050	-1.246	.374
.150	-1.461	.318	.012	-.331	.614	.012	-.443	.585	.150	-1.530	.300
.300	-1.391	.336	.025	-.858	.476	.025	-.704	.516	.300	-1.537	.298
.450	-.832	.483	.050	-1.214	.383	.050	-1.198	.387	.450	-.567	.552
.600	-.495	.571	.100	-1.476	.314	.100	-1.406	.332	.600	-.466	.579
.800	-.358	.607	.150	-1.448	.321	.150	-1.417	.330	.800	-.185	.653
.950	.104	.728	.200	-1.459	.319	.200	-1.393	.336			
			.300	-1.457	.319	.300	-1.421	.328			
			.350	-1.436	.325	.350	-1.436	.325			
			.400	-1.461	.319	.400	-1.422	.328			
			.450	-1.430	.326	.450	-1.315	.356			
			.500	-.905	.464	.500	-.777	.497			
			.550	-.736	.508	.550	-.574	.551			
			.600	-.570	.552	.600	-.462	.580			
			.650	-.480	.575	.700	-.265	.632			
			.700	-.435	.587	.800	-.183	.653			
			.800	-.281	.627	.900	-.079	.693			
			.900	-.047	.689	.950	.065	.718			
			.950	.043	.712	.990	.141	.738			
			.990	.116	.731						
					LOWER SURFACE						
.100	-.144	.663	.025	.227	.761	.025	.305	.781	.100	-.529	.562
.300	-.505	.569	.050	-.115	.671	.050	-.208	.646	.300	-.602	.543
.600	-.263	.632	.100	-.292	.624	.100	-.363	.606	.600	-.480	.575
.800	.201	.754	.200	-.455	.582	.200	-.494	.571	.800	.117	.732
			.300	-.561	.554	.300	-.633	.535			
			.400	-.600	.544	.400	-.677	.524			
			.500	-.621	.538	.500	-.676	.524			
			.600	-.254	.634	.600	-.421	.591			
			.700	.108	.729	.700	-.107	.673			
			.800	.273	.772	.800	.190	.751			
			.900	.377	.800	.900	.279	.774			
			.950	.385	.802	.950	.340	.790			
			1.000	.132	.736						
CN=				.6342			.5092				
CM=				-.0986			-.0451				

(f) M = 0.73. Continued.

$\delta_a = -6^o$; $\alpha = 2.83^o$; $C_L = 0.640$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.382	.340	0.000	1.067	.981	0.000	.102	.728	.050	-1.302	.361
.150	-1.519	.304	.012	-.420	.592	.012	-.522	.565	.150	-1.597	.283
.300	-1.446	.323	.025	-.944	.454	.025	-.756	.503	.300	-1.616	.278
.450	-.802	.491	.050	-1.316	.357	.050	-1.261	.371	.450	-.592	.546
.600	-.472	.578	.100	-1.535	.299	.100	-1.473	.316	.600	-.461	.581
.800	-.340	.613	.150	-1.500	.309	.150	-1.479	.314	.800	-.184	.653
.950	.087	.724	.200	-1.533	.300	.200	-1.452	.321			
			.300	-1.536	.299	.300	-1.495	.310			
			.350	-1.520	.303	.350	-1.496	.310			
			.400	-.985	.443	.400	-1.479	.314			
			.450	-1.218	.382	.450	-1.298	.362			
			.500	-.922	.460	.500	-.824	.486			
			.550	-.842	.481	.550	-.688	.521			
			.600	-.677	.524	.600	-.524	.564			
			.650	-.539	.560	.700	-.256	.634			
			.700	-.451	.583	.800	-.175	.656			
			.800	-.230	.641	.900	-.030	.694			
			.900	-.042	.691	.950	.060	.717			
			.950	.040	.712	.990	.133	.736			
			.990	.075	.721						
					LOWER SURFACE						
.100	-.093	.677	.025	.245	.766	.025	.378	.800	.100	-.453	.583
.300	-.466	.579	.050	-.053	.687	.050	-.125	.669	.300	-.576	.551
.600	-.276	.629	.100	-.229	.642	.100	-.296	.624	.600	-.482	.575
.800	.218	.758	.200	-.400	.597	.200	-.431	.589	.800	.115	.731
			.300	-.514	.567	.300	-.581	.549			
			.400	-.568	.547	.400	-.640	.534			
			.500	-.615	.540	.500	-.653	.531			
			.600	-.255	.635	.600	-.420	.591			
			.700	.106	.729	.700	-.106	.674			
			.800	.284	.776	.800	.196	.753			
			.900	.385	.802	.900	.292	.778			
			.950	.381	.801	.950	.344	.792			
			1.000	.100	.728						
CN=				.6605			.5769				
CM=				-.0940			-.0473				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = -4.87^o$; $C_L = -0.264$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.294	.625	0.000	1.058	.589	0.000	.084	.725	.050	-.202	.649
.150	-.465	.580	.012	.478	.827	.012	.431	.815	.150	-.428	.590
.300	-.528	.564	.025	.125	.736	.025	.172	.747	.300	-.515	.567
.450	-.413	.594	.050	-.233	.641	.050	-.194	.651	.450	-.494	.573
.600	-.516	.567	.100	-.365	.607	.100	-.330	.616	.600	-.511	.568
.800	-.383	.602	.150	-.411	.595	.150	-.342	.613	.800	-.289	.627
.950	.083	.724	.200	-.486	.575	.200	-.440	.587			
			.300	-.530	.563	.300	-.521	.566			
			.350	-.522	.566	.350	-.520	.566			
			.400	-.541	.561	.400	-.511	.568			
			.450	-.512	.568	.450	-.563	.555			
			.500	-.620	.540	.500	-.619	.540			
			.550	-.624	.539	.550	-.609	.543			
			.600	-.549	.559	.600	-.589	.548			
			.650	-.610	.542	.700	-.387	.601			
			.700	-.564	.555	.800	-.265	.633			
			.800	-.340	.613	.900	-.020	.697			
			.900	-.026	.695	.950	.068	.720			
			.950	.061	.718	.990	.114	.732			
			.990	.114	.737						
					LOWER SURFACE						
.100	-1.063	.424	.025	-.610	.543	.025	-.519	.566	.100	-1.504	.309
.300	-1.328	.355	.050	-1.173	.396	.050	-1.117	.410	.300	-1.500	.310
.600	-.252	.636	.100	-1.331	.354	.100	-1.378	.342	.600	-.384	.602
.800	.063	.719	.200	-1.399	.337	.200	-1.415	.332	.800	.074	.721
			.300	-1.432	.328	.300	-1.491	.312			
			.400	-1.046	.429	.400	-.906	.465			
			.500	-.533	.563	.500	-.659	.530			
			.600	-.244	.634	.600	-.311	.621			
			.700	.026	.709	.700	-.106	.674			
			.800	.189	.751	.800	.073	.721			
			.900	.292	.778	.900	.132	.737			
			.950	.302	.781	.950	.191	.752			
			1.000	.122	.736						
CN=				-.2087			-.2749				
CM=				-.1174			-.0727				

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = -3.31^o$; $C_L = -0.096$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.531	.563	0.000	1.115	.593	0.000	.092	.726	.050	-.431	.589
.150	-.594	.547	.012	.333	.789	.012	.279	.775	.150	-.566	.554
.300	-.636	.536	.025	-.077	.682	.025	-.015	.698	.300	-.590	.548
.450	-.492	.576	.050	-.463	.581	.050	-.452	.584	.450	-.544	.560
.600	-.551	.558	.100	-.573	.552	.100	-.561	.555	.600	-.519	.567
.800	-.372	.605	.150	-.598	.546	.150	-.517	.567	.800	-.270	.632
.950	.062	.718	.200	-.687	.522	.200	-.612	.542			
			.300	-.655	.531	.300	-.646	.533			
			.350	-.630	.537	.350	-.600	.545			
			.400	-.593	.547	.400	-.573	.552			
			.450	-.570	.553	.450	-.607	.543			
			.500	-.683	.524	.500	-.647	.533			
			.550	-.659	.530	.550	-.625	.539			
			.600	-.567	.554	.600	-.595	.547			
			.650	-.612	.542	.700	-.382	.602			
			.700	-.563	.555	.800	-.262	.634			
			.800	-.331	.616	.900	-.021	.696			
			.900	-.027	.695	.950	.057	.717			
			.950	.049	.715	.990	.098	.728			
			.990	.087	.725						
					LOWER SURFACE						
.100	-.869	.475	.025	-.458	.587	.025	-.318	.619	.100	-1.351	.349
.300	-1.071	.422	.050	-1.017	.436	.050	-.930	.459	.300	-1.050	.428
.600	-.256	.635	.100	-1.164	.398	.100	-1.230	.381	.600	-.409	.595
.800	.052	.716	.200	-1.157	.400	.200	-1.208	.386	.800	.104	.729
			.300	-1.220	.383	.300	-1.271	.370			
			.400	-.715	.515	.400	-.748	.506			
			.500	-.655	.521	.500	-.587	.549			
			.600	-.268	.632	.600	-.347	.611			
			.700	.044	.714	.700	-.051	.689			
			.800	.187	.751	.800	.174	.747			
			.900	.306	.782	.900	.245	.766			
			.950	.310	.783	.950	.295	.779			
			1.000	.103	.729						
CN=				-.0400			-.0854				
CM=				-.1140			-.0854				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = -1.50^o$; $C_L = 0.112$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.778	.498	0.000	1.113	.953	0.000	.089	.725	.050	-.763	.502
.150	-.903	.465	.012	.065	.719	.012	.027	.709	.150	-.768	.501
.300	-.743	.507	.025	-.404	.596	.025	-.264	.633	.300	-.722	.513
.450	-.582	.549	.050	-.787	.496	.050	-.728	.511	.450	-.590	.547
.600	-.579	.550	.100	-1.018	.435	.100	-.806	.491	.600	-.536	.561
.800	-.343	.617	.150	-.754	.504	.150	-.767	.501	.800	-.255	.635
.990	.052	.715	.200	-.895	.467	.200	-.787	.496			
			.300	-.821	.487	.300	-.855	.478			
			.350	-.774	.499	.350	-.700	.518			
			.400	-.685	.523	.400	-.645	.533			
			.450	-.669	.527	.450	-.674	.525			
			.500	-.751	.505	.500	-.712	.515			
			.550	-.731	.511	.550	-.660	.529			
			.600	-.644	.533	.600	-.611	.542			
			.650	-.620	.540	.700	-.383	.601			
			.700	-.551	.557	.800	-.246	.637			
			.800	-.300	.623	.900	-.023	.696			
			.900	-.012	.699	.950	.043	.713			
			.950	.049	.715	.990	.079	.722			
			.990	.066	.719						
					LOWER SURFACE						
.100	-.567	.553	.025	-.218	.645	.025	-.124	.669	.100	-1.122	.408
.300	-.745	.507	.050	-.703	.518	.050	-.725	.512	.300	-.699	.519
.600	-.767	.632	.100	-.813	.489	.100	-.954	.452	.600	-.422	.591
.800	.084	.724	.200	-.876	.472	.200	-.905	.465	.800	.084	.724
			.300	-.891	.469	.300	-1.017	.436			
			.400	-.805	.491	.400	-.740	.508			
			.500	-.696	.520	.500	-.695	.520			
			.600	-.261	.633	.600	-.370	.605			
			.700	.026	.708	.700	-.057	.687			
			.800	.155	.742	.800	.170	.746			
			.900	.292	.778	.900	.242	.765			
			.950	.321	.786	.950	.293	.778			
			1.000	.092	.726						
CN=				.1584			.0840				
CM=				-.0947			-.0713				

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = -0.04^o$; $C_L = 0.314$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.022	.433	0.000	1.118	.954	0.000	.096	.726	.050	-.587	.442
.150	-1.210	.384	.012	-.085	.679	.012	-.176	.655	.150	-1.297	.361
.300	-1.071	.420	.025	-.614	.540	.025	-.476	.576	.300	-.655	.529
.450	-.597	.544	.050	-1.000	.439	.050	-.975	.445	.450	-.606	.542
.600	-.586	.547	.100	-1.261	.370	.100	-1.164	.396	.600	-.551	.557
.800	-.376	.602	.150	-1.150	.400	.150	-1.166	.395	.900	-.270	.630
.950	.060	.717	.200	-1.203	.386	.200	-1.075	.419			
			.300	-1.137	.403	.300	-1.153	.399			
			.350	-1.198	.387	.350	-1.015	.435			
			.400	-.674	.524	.400	-.632	.535			
			.450	-.627	.537	.450	-.657	.529			
			.500	-.705	.516	.500	-.727	.510			
			.550	-.717	.513	.550	-.678	.523			
			.600	-.634	.522	.600	-.617	.539			
			.650	-.670	.525	.700	-.385	.600			
			.700	-.582	.548	.800	-.265	.631			
			.800	-.309	.620	.900	-.036	.692			
			.900	-.017	.697	.950	.042	.712			
			.950	.052	.715	.990	.081	.722			
			.990	.073	.720						
					LOWER SURFACE						
.100	-.389	.599	.025	-.037	.691	.025	.102	.728	.100	-.831	.483
.300	-.640	.533	.050	-.436	.587	.050	-.501	.569	.300	-.688	.521
.600	-.767	.631	.100	-.601	.543	.100	-.622	.538	.600	-.424	.590
.800	.140	.738	.200	-.692	.520	.200	-.704	.516	.900	.128	.735
			.300	-.727	.510	.300	-.850	.478			
			.400	-.712	.514	.400	-.730	.510			
			.500	-.686	.521	.500	-.697	.518			
			.600	-.257	.634	.600	-.381	.601			
			.700	.079	.722	.700	-.053	.687			
			.800	.230	.761	.800	.226	.760			
			.900	.344	.791	.900	.311	.782			
			.950	.355	.794	.950	.344	.791			
			1.000	.081	.722						
CN=				.3711			.2941				
CM=				-.0994			-.0673				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = 0.41^o$; $C_L = 0.364$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.103	.417	0.000	1.121	.595	0.000	.101	.728	.050	-1.041	.428
.150	-1.251	.374	.012	-.152	.661	.012	-.224	.643	.150	-1.343	.349
.300	-1.059	.424	.025	-.647	.532	.025	-.481	.575	.300	-.643	.533
.450	-.622	.538	.050	-1.046	.427	.050	-1.019	.434	.450	-.585	.548
.600	-.573	.551	.100	-1.295	.362	.100	-1.183	.391	.600	-.539	.560
.800	-.353	.609	.150	-1.245	.375	.150	-1.187	.390	.800	-.269	.631
.950	.054	.715	.200	-1.235	.378	.200	-1.159	.398			
			.300	-1.284	.365	.300	-1.711	.384			
			.350	-1.269	.369	.350	-1.209	.384			
			.400	-.879	.471	.400	-.843	.480			
			.450	-.572	.551	.450	-.631	.536			
			.500	-.660	.528	.500	-.646	.532			
			.550	-.629	.536	.550	-.616	.540			
			.600	-.638	.534	.600	-.597	.545			
			.650	-.619	.539	.700	-.377	.602			
			.700	-.559	.555	.800	-.252	.635			
			.800	-.318	.618	.900	-.029	.694			
			.900	-.035	.692	.950	.042	.712			
			.950	.053	.715	.990	.082	.723			
			.990	.088	.724						
					LOWER SURFACE						
.100	-.323	.616	.025	.023	.707	.025	.136	.737	.100	-.810	.489
.300	-.605	.543	.050	-.356	.608	.050	-.446	.584	.300	-.666	.527
.600	-.264	.632	.100	-.503	.569	.100	-.575	.551	.600	-.430	.588
.800	.146	.739	.200	-.632	.536	.200	-.643	.533	.800	.146	.739
			.300	-.687	.521	.300	-.757	.503			
			.400	-.676	.524	.400	-.725	.511			
			.500	-.665	.527	.500	-.661	.528			
			.600	-.254	.635	.600	-.368	.605			
			.700	.078	.722	.700	-.053	.687			
			.800	.232	.762	.800	.202	.754			
			.900	.354	.794	.900	.282	.775			
			.950	.354	.794	.950	.331	.788			
			1.000	.117	.732						
CN=				.4310			.3400				
CM=				-.0963			-.0623				

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = 1.42^o$; $C_L = 0.516$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.195	.388	0.000	1.100	.588	0.000	.095	.726	.050	-1.157	.398
.150	-1.407	.332	.012	-.254	.632	.012	-.357	.607	.150	-1.461	.318
.300	-1.305	.359	.025	-.775	.498	.025	-.621	.538	.300	-1.356	.346
.450	-.617	.539	.050	-1.154	.398	.050	-1.146	.400	.450	-.588	.547
.600	-.548	.557	.100	-1.408	.332	.100	-1.309	.358	.600	-.529	.562
.800	-.359	.607	.150	-1.353	.344	.150	-1.357	.345	.800	-.263	.632
.950	.085	.723	.200	-1.375	.341	.200	-1.339	.350			
			.300	-1.336	.338	.300	-1.342	.349			
			.350	-1.331	.339	.350	-1.345	.348			
			.400	-1.361	.344	.400	-1.339	.350			
			.450	-1.366	.343	.450	-1.181	.391			
			.500	-.869	.473	.500	-.698	.518			
			.550	-.590	.546	.550	-.568	.552			
			.600	-.530	.562	.600	-.515	.566			
			.650	-.502	.569	.700	-.354	.609			
			.700	-.466	.578	.800	-.262	.632			
			.800	-.330	.614	.900	-.044	.689			
			.900	-.054	.687	.950	.046	.713			
			.950	.061	.717	.990	.100	.727			
			.990	.124	.733						
					LOWER SURFACE						
.100	-.250	.635	.025	.128	.734	.025	.241	.764	.100	-.643	.532
.300	-.553	.556	.050	-.215	.645	.050	-.325	.616	.300	-.637	.534
.600	-.260	.633	.100	-.334	.600	.100	-.440	.586	.600	-.435	.587
.800	.193	.751	.200	-.518	.565	.200	-.521	.564	.800	.167	.745
			.300	-.556	.545	.300	-.677	.524			
			.400	-.628	.536	.400	-.673	.525			
			.500	-.631	.536	.500	-.639	.533			
			.600	-.255	.634	.600	-.362	.606			
			.700	.112	.730	.700	-.045	.689			
			.800	.288	.776	.800	.249	.766			
			.900	.337	.802	.900	.332	.788			
			.950	.388	.803	.950	.375	.799			
			1.000	.134	.736						
CN=				.5658			.4993				
CM=				-.1025			-.0709				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = 2.27^o$; $C_L = 0.611$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.360	.345	0.000	1.079	.584	0.000	.100	.727	.050	-1.288	.364
.150	-1.466	.317	.012	-.361	.607	.012	-.443	.585	.150	-1.557	.293
.300	-1.407	.333	.025	-.890	.468	.025	-.703	.517	.300	-1.545	.296
.450	-.842	.481	.050	-1.245	.375	.050	-1.202	.386	.450	-.597	.545
.600	-.502	.570	.100	-1.475	.315	.100	-1.413	.331	.600	-.509	.568
.800	-.320	.617	.150	-1.433	.326	.150	-1.436	.325	.800	-.241	.638
.990	.085	.723	.200	-1.479	.314	.200	-1.396	.336			
			.300	-1.473	.315	.300	-1.442	.324			
			.350	-1.475	.315	.350	-1.440	.324			
			.400	-1.456	.320	.400	-1.439	.324			
			.450	-1.445	.323	.450	-1.350	.347			
			.500	-.869	.474	.500	-.809	.489			
			.550	-.770	.499	.550	-.657	.529			
			.600	-.625	.538	.600	-.524	.564			
			.650	-.493	.572	.700	-.335	.614			
			.700	-.426	.590	.800	-.243	.638			
			.800	-.258	.634	.900	-.043	.690			
			.900	-.037	.691	.950	.050	.714			
			.950	.041	.712	.990	.104	.728			
			.990	.083	.723						
					LOWER SURFACE						
.100	-.121	.670	.025	.233	.762	.025	.347	.792	.100	-.501	.570
.300	-.474	.577	.050	-.121	.670	.050	-.181	.654	.300	-.568	.553
.600	-.244	.637	.100	-.279	.628	.100	-.339	.612	.600	-.430	.589
.800	.191	.751	.200	-.448	.584	.200	-.472	.577	.900	.162	.744
			.300	-.539	.560	.300	-.599	.544			
			.400	-.564	.553	.400	-.641	.533			
			.500	-.586	.548	.500	-.598	.545			
			.600	-.228	.642	.600	-.345	.611			
			.700	.098	.727	.700	-.040	.691			
			.800	.268	.771	.800	.245	.765			
			.900	.383	.801	.900	.325	.786			
			.950	.380	.801	.950	.363	.796			
			1.000	.127	.734						
CN=				.6514			.5872				
CM=				-.0989			-.0706				

(f) M = 0.73. Continued.

$\delta_a = -3^o$; $\alpha = 2.62^o$; $C_L = 0.648$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.376	.341	0.000	1.082	.585	0.000	.098	.727	.050	-1.320	.355
.150	-1.569	.293	.012	-.410	.534	.012	-.502	.570	.150	-1.583	.287
.300	-1.438	.324	.025	-.903	.465	.025	-.726	.511	.300	-1.582	.287
.450	-.987	.443	.050	-1.270	.369	.050	-1.237	.377	.450	-.625	.537
.600	-.491	.573	.100	-1.531	.300	.100	-1.447	.322	.600	-.515	.566
.800	-.333	.614	.150	-1.478	.314	.150	-1.457	.320	.800	-.252	.635
.990	.086	.724	.200	-1.523	.302	.200	-1.434	.326			
			.300	-1.520	.303	.300	-1.474	.315			
			.350	-1.516	.304	.350	-1.479	.314			
			.400	-1.512	.305	.400	-1.457	.320			
			.450	-1.389	.338	.450	-1.495	.310			
			.500	-.941	.455	.500	-.880	.471			
			.550	-.807	.490	.550	-.720	.513			
			.600	-.719	.513	.600	-.553	.556			
			.650	-.507	.568	.700	-.327	.616			
			.700	-.395	.598	.800	-.241	.638			
			.800	-.231	.641	.900	-.048	.689			
			.900	-.047	.689	.950	.045	.713			
			.950	.040	.712	.990	.104	.728			
			.990	.100	.727						
					LOWER SURFACE						
.100	-.179	.667	.025	.258	.769	.025	.377	.800	.100	-.478	.576
.300	-.467	.579	.050	-.067	.684	.050	-.147	.663	.300	-.567	.553
.600	-.244	.637	.100	-.246	.637	.100	-.296	.624	.600	-.427	.589
.800	.220	.759	.200	-.418	.592	.200	-.434	.588	.800	.180	.748
			.300	-.534	.561	.300	-.581	.549			
			.400	-.571	.552	.400	-.612	.541			
			.500	-.597	.545	.500	-.593	.546			
			.600	-.231	.641	.600	-.350	.610			
			.700	.113	.731	.700	-.041	.691			
			.800	.298	.779	.800	.260	.769			
			.900	.407	.808	.900	.350	.793			
			.950	.338	.806	.950	.386	.802			
			1.000	.074	.721						
CN=				.6900			.6354				
CM=				-.1020			-.0761				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = -4.91^o$; $C_L = -0.262$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.254	.635	0.000	1.087	.986	0.000	.092	.725	.050	-.276	.629
.150	-.448	.584	.012	.478	.826	.012	.471	.825	.150	-.413	.593
.300	-.502	.570	.025	.107	.729	.025	.166	.745	.300	-.537	.561
.450	-.461	.581	.050	-.236	.640	.050	-.192	.651	.450	-.501	.570
.600	-.523	.564	.100	-.358	.608	.100	-.347	.610	.600	-.547	.558
.800	-.365	.606	.150	-.415	.593	.150	-.353	.609	.800	-.327	.616
.990	.078	.722	.200	-.517	.566	.200	-.453	.583			
			.300	-.544	.559	.300	-.532	.562			
			.350	-.541	.560	.350	-.513	.567			
			.400	-.534	.562	.400	-.522	.565			
			.450	-.512	.567	.450	-.559	.555			
			.500	-.638	.534	.500	-.627	.537			
			.550	-.631	.536	.550	-.637	.535			
			.600	-.553	.557	.600	-.584	.548			
			.650	-.598	.545	.700	-.448	.584			
			.700	-.560	.555	.800	-.235	.640			
			.800	-.331	.615	.900	-.004	.700			
			.900	-.016	.697	.950	.013	.705			
			.950	.061	.717	.990	.026	.708			
			.990	.110	.730						
					LOWER SURFACE						
.100	-1.040	.429	.025	-.553	.556	.025	-.501	.570	.100	-1.527	.302
.300	-1.358	.346	.050	-1.187	.390	.050	-1.103	.412	.300	-1.443	.323
.600	-.239	.639	.100	-1.308	.359	.100	-1.354	.347	.600	-.338	.613
.800	.067	.719	.200	-1.361	.345	.200	-1.411	.332	.800	.109	.730
			.300	-1.457	.320	.300	-1.373	.342			
			.400	-.985	.443	.400	-.797	.493			
			.500	-.544	.559	.500	-.553	.557			
			.600	-.235	.640	.600	-.256	.634			
			.700	.042	.712	.700	-.175	.655			
			.800	.184	.750	.800	-.077	.682			
			.900	.278	.774	.900	.161	.744			
			.950	.283	.775	.950	.184	.749			
			1.000	.111	.731						
CN=				-.1964			-.2494				
CM=				-.1152			-.0687				

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = -3.19^o$; $C_L = -0.075$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.525	.564	0.000	1.123	.995	0.000	.093	.726	.050	-.529	.563
.150	-.620	.539	.012	.297	.779	.012	.285	.776	.150	-.586	.548
.300	-.640	.534	.025	-.087	.679	.025	-.035	.692	.300	-.613	.541
.450	-.619	.565	.050	-.487	.574	.050	-.415	.593	.450	-.541	.560
.600	-.548	.558	.100	-.580	.550	.100	-.555	.556	.600	-.568	.553
.800	-.345	.611	.150	-.615	.540	.150	-.514	.567	.800	-.312	.620
.990	.066	.719	.200	-.671	.526	.200	-.613	.541			
			.300	-.670	.526	.300	-.652	.531			
			.350	-.620	.539	.350	-.606	.543			
			.400	-.632	.536	.400	-.601	.544			
			.450	-.616	.540	.450	-.631	.536			
			.500	-.717	.514	.500	-.699	.518			
			.550	-.675	.525	.550	-.698	.519			
			.600	-.622	.539	.600	-.624	.538			
			.650	-.628	.537	.700	-.436	.587			
			.700	-.558	.555	.800	-.248	.636			
			.800	-.318	.618	.900	-.026	.695			
			.900	-.022	.696	.950	.003	.702			
			.950	.053	.715	.990	.006	.703			
			.990	.083	.723						
					LOWER SURFACE						
.100	-.831	.486	.025	-.411	.594	.025	-.334	.614	.100	-1.374	.342
.300	-.893	.468	.050	-.936	.456	.050	-.879	.471	.300	-.798	.493
.600	-.231	.641	.100	-1.144	.407	.100	-1.213	.384	.600	-.368	.605
.800	.007	.703	.200	-1.132	.405	.200	-1.231	.379	.800	.181	.749
			.300	-1.252	.373	.300	-1.273	.368			
			.400	-.699	.518	.400	-.824	.486			
			.500	-.670	.526	.500	-.545	.559			
			.600	-.269	.631	.600	-.277	.629			
			.700	.044	.713	.700	.004	.702			
			.800	.188	.751	.800	.210	.756			
			.900	.300	.780	.900	.261	.770			
			.950	.296	.779	.950	.287	.776			
			1.000	.099	.727						
CN=				-.0310			-.0523				
CM=				-.1125			-.1009				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = -1.46^o$; $C_L = 0.126$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.823	.486	0.000	1.119	.994	0.000	.095	.726	.050	-.771	.499
.150	-.974	.446	.012	.071	.720	.012	-.012	.698	.150	-.790	.494
.300	-.745	.506	.025	-.370	.604	.025	-.315	.619	.300	-.735	.509
.450	-.632	.536	.050	-.777	.498	.050	-.767	.501	.450	-.606	.543
.600	-.572	.552	.100	-.980	.445	.100	-.824	.486	.600	-.566	.553
.800	-.350	.610	.150	-.729	.510	.150	-.781	.497	.800	-.284	.627
.990	.061	.717	.200	-.902	.465	.200	-.772	.499			
			.300	-.824	.486	.300	-.922	.460			
			.350	-.726	.511	.350	-.744	.506			
			.400	-.710	.515	.400	-.646	.532			
			.450	-.688	.521	.450	-.691	.520			
			.500	-.787	.495	.500	-.739	.508			
			.550	-.715	.514	.550	-.708	.516			
			.600	-.673	.525	.600	-.633	.536			
			.650	-.632	.536	.700	-.423	.591			
			.700	-.541	.560	.800	-.224	.643			
			.800	-.285	.627	.900	-.061	.685			
			.900	-.017	.697	.950	-.022	.696			
			.950	.041	.712	.990	-.020	.696			
			.990	.055	.716						
					LOWER SURFACE						
.100	-.541	.560	.025	-.236	.640	.025	-.119	.670	.100	-1.114	.410
.300	-.744	.507	.050	-.690	.521	.050	-.715	.514	.300	-.698	.519
.600	-.766	.637	.100	-.858	.477	.100	-.861	.476	.600	-.366	.606
.800	.078	.722	.200	-.877	.472	.200	-.890	.468	.800	.143	.739
			.300	-.825	.485	.300	-1.030	.432			
			.400	-.801	.492	.400	-.731	.510			
			.500	-.686	.522	.500	-.647	.532			
			.600	-.276	.629	.600	-.302	.622			
			.700	.041	.712	.700	-.001	.701			
			.800	.192	.752	.800	.197	.753			
			.900	.289	.777	.900	.255	.768			
			.950	.319	.785	.950	.300	.780			
			1.000	.066	.719						
CN=				.1600			.1420				
CM=				-.0993			-.0870				

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = 0.48^o$; $C_L = 0.385$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.092	.415	0.000	1.119	.994	0.000	.098	.727	.050	-1.092	.415
.150	-1.294	.362	.012	-.175	.655	.012	-.252	.635	.150	-1.352	.347
.300	-1.142	.402	.025	-.635	.535	.025	-.533	.562	.300	-.932	.457
.450	-.607	.544	.050	-1.069	.421	.050	-1.022	.434	.450	-.599	.544
.600	-.577	.550	.100	-1.266	.370	.100	-1.219	.382	.600	-.585	.548
.800	-.339	.613	.150	-1.243	.376	.150	-1.227	.380	.800	-.324	.616
.990	.063	.718	.200	-1.250	.374	.200	-1.134	.404			
			.300	-1.247	.375	.300	-1.215	.383			
			.350	-1.263	.371	.350	-1.211	.384			
			.400	-.821	.486	.400	-1.049	.427			
			.450	-.751	.505	.450	-.640	.534			
			.500	-.592	.546	.500	-.665	.527			
			.550	-.675	.525	.550	-.669	.526			
			.600	-.639	.534	.600	-.629	.537			
			.650	-.600	.544	.700	-.437	.587			
			.700	-.551	.557	.800	-.267	.631			
			.800	-.322	.617	.900	-.051	.688			
			.900	-.030	.694	.950	-.023	.695			
			.950	.037	.711	.990	-.001	.701			
			.990	.077	.721						
					LOWER SURFACE						
.100	-.315	.619	.025	.078	.722	.025	.169	.746	.100	-.729	.510
.300	-.603	.543	.050	-.348	.610	.050	-.496	.571	.300	-.636	.535
.600	-.289	.626	.100	-.507	.569	.100	-.505	.569	.600	-.370	.604
.800	.161	.744	.200	-.610	.542	.200	-.610	.542	.800	.215	.758
			.300	-.685	.522	.300	-.763	.502			
			.400	-.679	.523	.400	-.695	.519			
			.500	-.653	.530	.500	-.593	.546			
			.600	-.245	.637	.600	-.299	.623			
			.700	.084	.723	.700	-.000	.701			
			.800	.248	.766	.800	.246	.766			
			.900	.352	.794	.900	.307	.782			
			.950	.345	.792	.950	.344	.791			
			1.000	.089	.725						
CN=				.4267			.4119				
CM=				-.0961			-.0839				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = 1.49^o$; $C_L = 0.527$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
				UPPER SURFACE							
.050	-1.257	.372	0.000	1.099	.589	0.000	.098	.727	.050	-1.255	.373
.150	-1.374	.342	.012	-.299	.623	.012	-.366	.606	.150	-1.469	.317
.300	-1.309	.359	.025	-.796	.493	.025	-.615	.541	.300	-1.361	.345
.450	-.689	.521	.050	-1.147	.401	.050	-1.133	.405	.450	-.608	.542
.600	-.530	.563	.100	-1.392	.337	.100	-1.355	.347	.600	-.581	.549
.800	-.335	.614	.150	-1.345	.349	.150	-1.352	.347	.800	-.297	.624
.990	.083	.723	.200	-1.419	.330	.200	-1.318	.356			
			.300	-1.388	.338	.300	-1.344	.350			
			.350	-1.381	.340	.350	-1.377	.341			
			.400	-1.368	.343	.400	-1.350	.348			
			.450	-1.273	.368	.450	-1.164	.397			
			.500	-.811	.489	.500	-.707	.516			
			.550	-.610	.542	.550	-.620	.539			
			.600	-.543	.559	.600	-.528	.563			
			.650	-.505	.569	.700	-.416	.593			
			.700	-.453	.583	.800	-.282	.628			
			.800	-.303	.622	.900	-.048	.689			
			.900	-.032	.693	.950	.012	.705			
			.950	.043	.713	.990	.021	.707			
			.990	.094	.726						
				LOWER SURFACE							
.100	-.163	.659	.025	.133	.736	.025	.258	.769	.100	-.607	.543
.300	-.505	.569	.050	-.218	.644	.050	-.293	.625	.300	-.603	.544
.600	-.247	.637	.100	-.358	.608	.100	-.410	.594	.600	-.365	.606
.800	.182	.749	.200	-.509	.568	.200	-.547	.558	.800	.234	.763
			.300	-.630	.537	.300	-.639	.534			
			.400	-.619	.539	.400	-.647	.532			
			.500	-.619	.540	.500	-.574	.551			
			.600	-.238	.639	.600	-.293	.625			
			.700	.097	.727	.700	.028	.709			
			.800	.276	.774	.800	.286	.776			
			.900	.380	.801	.900	.342	.791			
			.950	.369	.798	.950	.372	.799			
			1.000	.116	.732						
CN=				.5670			.5507				
CM=				-.0977			-.0889				

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = 2.33^o$; $C_L = 0.626$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
				UPPER SURFACE							
.050	-1.305	.360	0.000	1.087	.586	0.000	.094	.726	.050	-1.327	.354
.150	-1.477	.315	.012	-.358	.608	.012	-.493	.572	.150	-1.564	.292
.300	-1.401	.335	.025	-.878	.471	.025	-.694	.520	.300	-1.549	.296
.450	-.848	.479	.050	-1.261	.371	.050	-1.223	.381	.450	-.610	.542
.600	-.503	.570	.100	-1.485	.313	.100	-1.430	.327	.600	-.549	.558
.800	-.321	.617	.150	-1.447	.323	.150	-1.442	.324	.800	-.293	.625
.990	.084	.723	.200	-1.486	.312	.200	-1.394	.336			
			.300	-1.467	.317	.300	-1.453	.321			
			.350	-1.463	.318	.350	-1.463	.318			
			.400	-1.464	.318	.400	-1.418	.330			
			.450	-1.476	.315	.450	-1.452	.321			
			.500	-.918	.461	.500	-.888	.469			
			.550	-.783	.496	.550	-.656	.530			
			.600	-.642	.533	.600	-.549	.558			
			.650	-.525	.564	.700	-.394	.598			
			.700	-.425	.590	.800	-.283	.627			
			.800	-.263	.633	.900	-.056	.687			
			.900	-.039	.691	.950	.012	.705			
			.950	.033	.710	.990	.063	.718			
			.990	.056	.716						
				LOWER SURFACE							
.100	-.117	.671	.025	.239	.764	.025	.341	.791	.100	-.521	.565
.300	-.471	.578	.050	-.091	.678	.050	-.217	.646	.300	-.565	.554
.600	-.240	.638	.100	-.277	.629	.100	-.317	.618	.600	-.377	.603
.800	.198	.753	.200	-.428	.589	.200	-.438	.587	.800	.236	.763
			.300	-.524	.564	.300	-.567	.553			
			.400	-.565	.554	.400	-.610	.542			
			.500	-.583	.549	.500	-.559	.555			
			.600	-.241	.638	.600	-.299	.623			
			.700	.096	.726	.700	.016	.706			
			.800	.266	.771	.800	.297	.779			
			.900	.377	.800	.900	.354	.794			
			.950	.367	.797	.950	.384	.802			
			1.000	.076	.721						
CN=				.6626			.6491				
CM=				-.1004			-.0915				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 0^o$; $\alpha = 2.67^o$; $C_L = 0.649$

STATION .1597			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.345	.350	0.000	1.078	.584	0.000	.108	.730	.050	-1.353	.348
.150	-1.494	.311	.012	-.450	.584	.012	-.500	.571	.150	-1.582	.288
.300	-1.446	.323	.025	-.904	.465	.025	-.739	.508	.300	-1.590	.286
.450	-.750	.505	.050	-1.262	.371	.050	-1.251	.374	.450	-.608	.543
.600	-.484	.575	.100	-1.495	.310	.100	-1.437	.326	.600	-.521	.565
.800	-.306	.622	.150	-1.482	.314	.150	-1.468	.317	.800	-.262	.633
.990	.086	.724	.200	-1.506	.307	.200	-1.410	.333			
			.300	-1.516	.305	.300	-1.481	.314			
			.350	-1.471	.317	.350	-1.459	.320			
			.400	-1.470	.317	.400	-1.495	.310			
			.450	-.868	.474	.450	-1.376	.341			
			.500	-.897	.467	.500	-.864	.475			
			.550	-.783	.497	.550	-.745	.507			
			.600	-.650	.531	.600	-.584	.549			
			.650	-.518	.566	.700	-.387	.600			
			.700	-.395	.598	.800	-.267	.632			
			.800	-.229	.642	.900	-.060	.686			
			.900	-.053	.688	.950	.021	.707			
			.950	.000	.702	.990	.059	.717			
			.990	.011	.704						
					LOWER SURFACE						
.100	-.074	.682	.025	.280	.775	.025	.367	.798	.100	-.461	.581
.300	-.453	.583	.050	-.029	.694	.050	-.117	.671	.300	-.532	.563
.600	-.269	.631	.100	-.213	.646	.100	-.270	.631	.600	-.366	.606
.800	.221	.759	.200	-.382	.602	.200	-.449	.584	.800	.237	.764
			.300	-.488	.574	.300	-.547	.559			
			.400	-.534	.562	.400	-.576	.551			
			.500	-.565	.554	.500	-.526	.564			
			.600	-.229	.642	.600	-.262	.633			
			.700	.108	.730	.700	.026	.708			
			.800	.277	.774	.800	.293	.778			
			.900	.377	.800	.900	.358	.795			
			.950	.349	.793	.950	.391	.804			
			1.000	.049	.714						
CN=				.6941			.6802				
CM=				-.0992			-.0936				

[redacted]

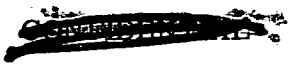


TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = -4.81^o$; $C_L = -0.241$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.785	.627	0.000	1.104	.990	0.000	.087	.724	.050	-.242	.638
.150	-.590	.570	.012	.456	.821	.012	.434	.815	.150	-.455	.582
.300	-.525	.564	.025	.051	.715	.025	.143	.739	.300	-.544	.559
.450	-.436	.587	.050	-.283	.627	.050	-.219	.644	.450	-.524	.564
.600	-.533	.562	.100	-.393	.598	.100	-.352	.609	.600	-.569	.552
.800	-.383	.601	.150	-.446	.585	.150	-.379	.602	.800	-.357	.608
.990	.071	.720	.200	-.518	.566	.200	-.478	.576			
			.300	-.545	.559	.300	-.561	.554			
			.350	-.555	.556	.350	-.536	.561			
			.400	-.556	.556	.400	-.537	.561			
			.450	-.530	.562	.450	-.583	.549			
			.500	-.677	.525	.500	-.646	.537			
			.550	-.644	.533	.550	-.647	.532			
			.600	-.581	.549	.600	-.632	.536			
			.650	-.633	.536	.700	-.451	.583			
			.700	-.577	.550	.800	-.206	.647			
			.800	-.346	.611	.900	-.096	.676			
			.900	-.031	.693	.950	-.091	.678			
			.550	.049	.714	.990	-.089	.678			
			.990	.096	.726						
					LOWER SURFACE						
.100	-1.065	.422	.025	-.571	.552	.025	-.491	.573	.100	-1.491	.311
.300	-1.331	.361	.050	-1.173	.394	.050	-1.086	.417	.300	-1.434	.326
.600	-.744	.637	.100	-1.288	.364	.100	-1.351	.348	.600	-.318	.618
.800	.065	.718	.200	-1.374	.342	.200	-1.385	.339	.800	.182	.749
			.300	-1.418	.330	.300	-1.479	.314			
			.400	-1.000	.440	.400	-1.007	.438			
			.500	-.543	.559	.500	-.522	.565			
			.600	-.240	.639	.600	-.207	.647			
			.700	.037	.711	.700	.044	.713			
			.800	.213	.757	.800	.224	.760			
			.900	.302	.781	.900	.265	.771			
			.550	.279	.774	.950	.278	.774			
			1.000	.110	.730						
CN=				-.1684			-.1677				
CM=				-.1211			-.1171				

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = -3.09^o$; $C_L = -0.050$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.559	.553	0.000	1.116	.994	0.000	.090	.725	.050	-.488	.574
.150	-.632	.531	.012	.271	.772	.012	.249	.766	.150	-.602	.544
.300	-.646	.527	.025	-.129	.668	.025	-.070	.683	.300	-.629	.537
.450	-.529	.563	.050	-.503	.570	.050	-.482	.575	.450	-.573	.551
.600	-.565	.554	.100	-.591	.547	.100	-.574	.551	.600	-.594	.546
.800	-.363	.605	.150	-.632	.536	.150	-.538	.561	.800	-.348	.610
.990	.066	.719	.200	-.695	.519	.200	-.626	.537			
			.300	-.681	.523	.300	-.681	.523			
			.350	-.640	.534	.350	-.628	.537			
			.400	-.641	.534	.400	-.609	.542			
			.450	-.603	.544	.450	-.659	.529			
			.500	-.729	.511	.500	-.716	.514			
			.550	-.703	.517	.550	-.699	.519			
			.600	-.629	.537	.600	-.653	.531			
			.650	-.657	.529	.700	-.450	.584			
			.700	-.578	.550	.800	-.216	.645			
			.800	-.316	.619	.900	-.112	.672			
			.900	-.027	.694	.950	-.106	.674			
			.950	.046	.713	.990	-.106	.674			
			.990	.087	.724						
					LOWER SURFACE						
.100	-.976	.472	.025	-.411	.594	.025	-.315	.619	.100	-1.327	.356
.300	-.902	.465	.050	-.946	.454	.050	-.882	.470	.300	-.751	.505
.600	-.274	.630	.100	-1.126	.407	.100	-1.197	.388	.600	-.322	.617
.800	.057	.716	.200	-1.145	.402	.200	-1.200	.387	.800	.210	.756
			.300	-1.163	.397	.300	-1.252	.374			
			.400	-.728	.511	.400	-.627	.537			
			.500	-.680	.523	.500	-.547	.558			
			.600	-.266	.637	.600	-.266	.637			
			.700	.043	.713	.700	.053	.715			
			.800	.178	.748	.800	.273	.773			
			.900	.283	.775	.900	.312	.783			
			.550	.310	.783	.950	.315	.784			
			1.000	.091	.725						
CN=				-.0110			.0203				
CM=				-.1135			-.1225				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = -1.41^o$; $C_L = 0.147$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.830	.484	0.000	1.119	.994	0.000	.091	.725	.050	-.775	.458
.150	-.988	.442	.012	.085	.723	.012	-.023	.695	.150	-.867	.474
.300	-.794	.493	.025	-.406	.595	.025	-.301	.623	.300	-.770	.500
.450	-.613	.541	.050	-.758	.503	.050	-.791	.494	.450	-.615	.540
.600	-.585	.548	.100	-1.049	.427	.100	-.877	.472	.600	-.606	.543
.800	-.347	.610	.150	-.776	.498	.150	-.773	.499	.800	-.334	.614
.990	.059	.719	.200	-.902	.465	.200	-.795	.493			
			.300	-.845	.480	.300	-.913	.462			
			.350	-.778	.498	.350	-.787	.495			
			.400	-.745	.506	.400	-.670	.526			
			.450	-.704	.517	.450	-.710	.515			
			.500	-.791	.494	.500	-.773	.499			
			.550	-.743	.507	.550	-.747	.506			
			.600	-.663	.528	.600	-.665	.527			
			.650	-.639	.534	.700	-.441	.586			
			.700	-.558	.555	.800	-.210	.646			
			.800	-.288	.626	.900	-.122	.669			
			.900	-.036	.692	.950	-.119	.670			
			.950	.025	.708	.990	-.119	.670			
			.990	.059	.717						
					LOWER SURFACE						
.100	-.599	.544	.025	-.209	.647	.025	-.109	.673	.100	-1.090	.416
.300	-.741	.507	.050	-.659	.529	.050	-.672	.525	.300	-.667	.527
.600	-.768	.631	.100	-.802	.491	.100	-.846	.480	.600	-.309	.620
.800	.095	.726	.200	-.867	.474	.200	-.895	.467	.800	.163	.744
			.300	-.822	.486	.300	-.941	.455			
			.400	-.786	.495	.400	-.721	.512			
			.500	-.690	.521	.500	-.600	.544			
			.600	-.266	.632	.600	-.273	.630			
			.700	.041	.712	.700	.048	.714			
			.800	.177	.746	.800	.260	.769			
			.900	.297	.779	.900	.316	.784			
			.950	.311	.783	.950	.322	.786			
			1.000	.061	.717						
CN=				.1882			.2047				
CM=				-.1003			-.1078				

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = 0.06^o$; $C_L = 0.352$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.030	.432	0.000	1.124	.996	0.000	.098	.727	.050	-1.013	.436
.150	-1.226	.380	.012	-.128	.668	.012	-.200	.669	.150	-1.328	.353
.300	-1.020	.434	.025	-.620	.539	.025	-.479	.576	.300	-.614	.541
.450	-.623	.538	.050	-1.023	.433	.050	-.990	.442	.450	-.619	.539
.600	-.594	.546	.100	-1.281	.366	.100	-1.167	.396	.600	-.614	.541
.800	-.366	.605	.150	-1.143	.397	.150	-1.177	.393	.800	-.340	.612
.990	.061	.717	.200	-1.218	.382	.200	-1.097	.414			
			.300	-1.199	.387	.300	-1.189	.390			
			.350	-1.209	.385	.350	-1.143	.402			
			.400	-.639	.534	.400	-.838	.482			
			.450	-.631	.536	.450	-.650	.531			
			.500	-.730	.510	.500	-.702	.517			
			.550	-.727	.511	.550	-.711	.515			
			.600	-.656	.530	.600	-.667	.527			
			.650	-.653	.530	.700	-.454	.583			
			.700	-.573	.551	.800	-.227	.642			
			.800	-.321	.617	.900	-.124	.669			
			.900	-.034	.692	.950	-.117	.671			
			.950	.043	.712	.990	-.111	.672			
			.990	.063	.718						
					LOWER SURFACE						
.100	-.346	.611	.025	-.022	.695	.025	.127	.734	.100	-.801	.492
.300	-.618	.539	.050	-.405	.595	.050	-.481	.575	.300	-.625	.538
.600	-.267	.631	.100	-.562	.554	.100	-.585	.548	.600	-.305	.622
.800	.167	.745	.200	-.659	.529	.200	-.662	.528	.800	.239	.764
			.300	-.704	.517	.300	-.744	.507			
			.400	-.686	.522	.400	-.669	.526			
			.500	-.650	.531	.500	-.575	.551			
			.600	-.251	.635	.600	-.259	.634			
			.700	.076	.721	.700	.079	.722			
			.800	.244	.765	.800	.324	.786			
			.900	.341	.791	.900	.363	.796			
			.950	.350	.793	.950	.366	.797			
			1.000	.083	.723						
CN=				.4009			.4224				
CM=				-.1014			-.1081				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = 0.58^o$; $C_L = 0.420$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.148	.401	0.000	1.111	.992	0.000	.096	.726	.050	-1.090	.416
.150	-1.295	.362	.012	-.152	.662	.012	-.242	.638	.150	-1.416	.331
.300	-1.161	.397	.025	-.684	.522	.025	-.527	.565	.300	-.934	.457
.450	-.532	.546	.050	-1.069	.421	.050	-1.061	.424	.450	-.613	.541
.600	-.575	.551	.100	-1.321	.355	.100	-1.253	.373	.600	-.609	.542
.800	-.364	.606	.150	-1.267	.370	.150	-1.233	.379	.800	-.339	.613
.990	.072	.720	.200	-1.237	.362	.200	-1.222	.381			
			.300	-1.316	.357	.300	-1.245	.375			
			.350	-1.265	.370	.350	-1.269	.369			
			.400	-1.291	.363	.400	-1.140	.403			
			.450	-.664	.527	.450	-.694	.520			
			.500	-.607	.542	.500	-.649	.531			
			.550	-.600	.544	.550	-.677	.524			
			.600	-.656	.530	.600	-.637	.535			
			.650	-.585	.548	.700	-.457	.582			
			.700	-.551	.557	.800	-.245	.637			
			.800	-.316	.619	.900	-.113	.672			
			.900	-.036	.697	.950	-.099	.675			
			.950	.042	.712	.990	-.091	.678			
			.990	.078	.722						
					LOWER SURFACE						
.100	-.332	.614	.025	.059	.717	.025	.156	.742	.100	-.713	.515
.300	-.588	.548	.050	-.269	.631	.050	-.397	.599	.300	-.603	.643
.600	-.271	.630	.100	-.474	.577	.100	-.537	.562	.600	-.312	.690
.800	.149	.740	.200	-.590	.547	.200	-.598	.545	.800	.231	.762
			.300	-.668	.526	.300	-.694	.520			
			.400	-.661	.528	.400	-.668	.526			
			.500	-.626	.538	.500	-.548	.558			
			.600	-.246	.637	.600	-.261	.633			
			.700	.083	.723	.700	.068	.719			
			.800	.250	.767	.800	.310	.783			
			.900	.338	.790	.900	.356	.795			
			.950	.346	.792	.950	.366	.797			
			1.000	.080	.722						
CN=				.4815			.4835				
CM=				-.0985			-.1043				

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = 1.59^o$; $C_L = 0.569$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.249	.375	0.000	1.094	.988	0.000	.099	.727	.050	-1.232	.379
.150	-1.437	.325	.012	-.296	.624	.012	-.391	.599	.150	-1.502	.309
.300	-1.361	.346	.025	-.822	.487	.025	-.668	.527	.300	-1.474	.316
.450	-.741	.508	.050	-1.178	.393	.050	-1.162	.397	.450	-.641	.534
.600	-.537	.561	.100	-1.431	.327	.100	-1.349	.349	.600	-.598	.545
.800	-.368	.605	.150	-1.376	.342	.150	-1.361	.345	.800	-.322	.617
.990	.080	.722	.200	-1.403	.335	.200	-1.334	.353			
			.300	-1.393	.337	.300	-1.385	.339			
			.350	-1.428	.328	.350	-1.398	.336			
			.400	-1.384	.339	.400	-1.371	.343			
			.450	-1.406	.334	.450	-1.421	.330			
			.500	-.875	.473	.500	-.841	.482			
			.550	-.729	.511	.550	-.629	.537			
			.600	-.596	.546	.600	-.569	.553			
			.650	-.520	.565	.700	-.451	.584			
			.700	-.492	.573	.800	-.266	.632			
			.800	-.268	.632	.900	-.099	.676			
			.900	-.054	.687	.950	-.079	.681			
			.950	.054	.716	.990	-.073	.683			
			.990	.099	.728						
					LOWER SURFACE						
.100	-.236	.640	.025	.158	.743	.025	.290	.777	.100	-.551	.558
.300	-.517	.565	.050	-.182	.654	.050	-.262	.633	.300	-.559	.555
.600	-.256	.635	.100	-.340	.613	.100	-.390	.600	.600	-.302	.623
.800	.139	.754	.200	-.489	.574	.200	-.488	.574	.800	.268	.772
			.300	-.573	.552	.300	-.583	.549			
			.400	-.589	.548	.400	-.605	.543			
			.500	-.577	.551	.500	-.524	.564			
			.600	-.230	.641	.600	-.244	.637			
			.700	.120	.733	.700	.097	.727			
			.800	.281	.775	.800	.360	.796			
			.900	.388	.803	.900	.392	.804			
			.950	.364	.797	.950	.393	.804			
			1.000	.104	.729						
CN=				.6117			.6440				
CM=				-.1047			-.1153				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 3^o$; $\alpha = 2.40^o$; $C_L = 0.651$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.349	.349	0.000	1.083	.985	0.000	.098	.727	.050	-1.292	.364
.150	-1.497	.310	.012	-.397	.598	.012	-.482	.576	.150	-1.583	.287
.300	-1.420	.330	.025	-.913	.463	.025	-.704	.517	.300	-1.560	.293
.450	-.909	.464	.050	-1.270	.369	.050	-1.244	.376	.450	-.662	.528
.600	-.505	.570	.100	-1.513	.306	.100	-1.427	.328	.600	-.584	.549
.800	-.329	.615	.150	-1.457	.320	.150	-1.448	.323	.800	-.318	.618
.990	.087	.724	.200	-1.489	.312	.200	-1.427	.329			
			.300	-1.506	.307	.300	-1.460	.320			
			.350	-1.491	.311	.350	-1.468	.318			
			.400	-1.504	.308	.400	-1.462	.319			
			.450	-1.313	.358	.450	-1.488	.312			
			.500	-.920	.461	.500	-.940	.456			
			.550	-.816	.488	.550	-.746	.506			
			.600	-.696	.519	.600	-.654	.531			
			.650	-.578	.550	.700	-.441	.586			
			.700	-.417	.592	.800	-.294	.625			
			.800	-.228	.642	.900	-.100	.676			
			.900	-.066	.684	.950	-.053	.688			
			.950	.007	.703	.990	-.027	.695			
			.990	.060	.717						
					LOWER SURFACE						
.100	-.153	.662	.025	.228	.761	.025	.365	.797	.100	-.480	.576
.300	-.469	.579	.050	-.066	.684	.050	-.152	.662	.300	-.521	.565
.600	-.265	.632	.100	-.276	.629	.100	-.309	.621	.600	-.302	.623
.800	.197	.753	.200	-.408	.595	.200	-.430	.589	.800	.264	.771
			.300	-.526	.564	.300	-.537	.561			
			.400	-.548	.558	.400	-.573	.552			
			.500	-.566	.553	.500	-.582	.570			
			.600	-.220	.644	.600	-.244	.638			
			.700	.105	.729	.700	.088	.725			
			.800	.280	.775	.800	.361	.796			
			.900	.385	.802	.900	.394	.805			
			.950	.363	.797	.950	.406	.808			
			1.000	.071	.720						
CN=				.6895			.7275				
CM=				-.1054			-.1187				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 6^o$; $\alpha = -4.76^o$; $C_L = -0.221$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.343	.612	0.000	1.099	.989	0.000	.087	.724	.050	-.281	.628
.150	-.439	.573	.012	.473	.825	.012	.424	.813	.150	-.460	.581
.300	-.533	.562	.025	.057	.716	.025	.137	.736	.300	-.543	.559
.450	-.459	.581	.050	-.282	.628	.050	-.244	.637	.450	-.532	.562
.600	-.552	.557	.100	-.380	.602	.100	-.397	.597	.600	-.586	.548
.800	-.399	.597	.150	-.467	.579	.150	-.393	.598	.800	-.369	.605
.990	.078	.722	.200	-.528	.563	.200	-.493	.572			
			.300	-.544	.559	.300	-.563	.554			
			.350	-.556	.556	.350	-.547	.558			
			.400	-.563	.554	.400	-.547	.558			
			.450	-.544	.559	.450	-.601	.544			
			.500	-.666	.527	.500	-.665	.527			
			.550	-.661	.528	.550	-.662	.528			
			.600	-.590	.547	.600	-.641	.534			
			.650	-.648	.532	.700	-.435	.588			
			.700	-.600	.544	.800	-.187	.654			
			.800	-.371	.604	.900	-.150	.662			
			.900	-.057	.686	.950	-.150	.662			
			.950	.040	.712	.990	-.149	.662			
			.990	.093	.726						
					LOWER SURFACE						
.100	-1.136	.404	.025	-.558	.555	.025	-.495	.572	.100	-1.473	.316
.300	-1.268	.369	.050	-1.150	.400	.050	-1.094	.415	.300	-1.324	.355
.600	-.233	.640	.100	-1.305	.360	.100	-1.353	.347	.600	-.267	.631
.800	.058	.717	.200	-1.350	.348	.200	-1.413	.331	.800	.224	.760
			.300	-1.416	.331	.300	-1.485	.313			
			.400	-.989	.442	.400	-.866	.475			
			.500	-.484	.575	.500	-.484	.575			
			.600	-.235	.640	.600	-.170	.657			
			.700	.061	.717	.700	.087	.724			
			.800	.242	.765	.800	.256	.768			
			.900	.340	.790	.900	.275	.773			
			.950	.324	.786	.950	.267	.771			
			1.000	.102	.728						
CN=				-.1398			-.1282				
CM=				-.1346			-.1292				

(f) M = 0.73. Continued.

$\delta_a = 6^o$; $\alpha = -3.02^o$; $C_L = -0.022$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.606	.543	0.000	1.109	.992	0.000	.088	.725	.050	-.528	.563
.150	-.720	.513	.012	.257	.769	.012	.204	.755	.150	-.643	.533
.300	-.654	.530	.025	-.142	.664	.025	-.066	.684	.300	-.656	.530
.450	-.556	.556	.050	-.532	.562	.050	-.495	.572	.450	-.591	.547
.600	-.573	.552	.100	-.631	.537	.100	-.591	.547	.600	-.620	.539
.800	-.336	.601	.150	-.644	.533	.150	-.548	.558	.800	-.378	.603
.990	.073	.721	.200	-.723	.512	.200	-.644	.533			
			.300	-.684	.523	.300	-.697	.519			
			.350	-.668	.527	.350	-.653	.531			
			.400	-.668	.527	.400	-.623	.538			
			.450	-.644	.533	.450	-.670	.526			
			.500	-.758	.503	.500	-.736	.509			
			.550	-.742	.507	.550	-.729	.511			
			.600	-.660	.529	.600	-.671	.526			
			.650	-.670	.526	.700	-.445	.585			
			.700	-.601	.544	.800	-.201	.649			
			.800	-.343	.612	.900	-.166	.658			
			.900	-.047	.689	.950	-.165	.658			
			.950	.044	.713	.990	-.164	.659			
			.990	.074	.721						
					LOWER SURFACE						
.100	-.908	.464	.025	-.415	.593	.025	-.278	.629	.100	-1.317	.357
.300	-.850	.479	.050	-.910	.464	.050	-.865	.475	.300	-.596	.546
.600	-.230	.641	.100	-1.090	.416	.100	-1.176	.394	.600	-.261	.633
.800	.090	.725	.200	-1.114	.410	.200	-1.146	.402	.800	.245	.766
			.300	-1.176	.394	.300	-1.183	.392			
			.400	-.667	.527	.400	-.590	.547			
			.500	-.684	.523	.500	-.524	.564			
			.600	-.269	.631	.600	-.200	.649			
			.700	.050	.715	.700	.100	.728			
			.800	.218	.759	.800	.291	.778			
			.900	.331	.788	.900	.332	.788			
			.950	.342	.791	.950	.339	.790			
			1.000	.082	.723						
CN=				.0347			.0766				
CM=				-.1247			-.1365				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

$\delta_a = 6^o$; $\alpha = 1.27^o$; $C_L = 0.185$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.877	.472	0.000	1.122	.995	0.000	.094	.726	.050	-.822	.486
.150	-1.022	.436	.012	.061	.717	.012	-.024	.695	.150	-.958	.450
.300	-.780	.497	.025	-.413	.593	.025	-.328	.615	.300	-.810	.489
.450	-.617	.540	.050	-.818	.487	.050	-.807	.490	.450	-.633	.536
.600	-.600	.544	.100	-1.068	.422	.100	-.948	.453	.600	-.634	.535
.800	-.361	.607	.150	-.967	.448	.150	-.882	.470	.800	-.363	.606
.990	.053	.715	.200	-.903	.465	.200	-.818	.487			
			.300	-.862	.476	.300	-.909	.463			
			.350	-.785	.496	.350	-.856	.477			
			.400	-.734	.509	.400	-.673	.525			
			.450	-.732	.510	.450	-.722	.512			
			.500	-.821	.486	.500	-.787	.495			
			.550	-.789	.495	.550	-.777	.498			
			.600	-.687	.521	.600	-.677	.524			
			.650	-.669	.526	.700	-.438	.587			
			.700	-.578	.550	.800	-.204	.648			
			.800	-.327	.616	.900	-.170	.657			
			.900	-.041	.691	.950	-.169	.657			
			.550	.028	.709	.990	-.173	.656			
			.990	.059	.717						
					LOWER SURFACE						
.100	-.611	.541	.025	-.195	.650	.025	-.089	.678	.100	-1.060	.424
.300	-.724	.512	.050	-.608	.542	.050	-.689	.521	.300	-.655	.530
.600	-.274	.630	.100	-.787	.495	.100	-.765	.501	.600	-.233	.640
.800	.098	.727	.200	-.836	.482	.200	-.855	.477	.800	.193	.762
			.300	-.808	.490	.300	-.891	.468			
			.400	-.731	.510	.400	-.685	.522			
			.500	-.675	.525	.500	-.538	.560			
			.600	-.267	.631	.600	-.196	.650			
			.700	.060	.717	.700	.101	.728			
			.800	.216	.758	.800	.288	.777			
			.900	.338	.790	.900	.349	.793			
			.550	.348	.792	.950	.353	.794			
			1.000	.071	.720						
CN=				.2420			.2755				
CM=				-.1121			-.1234				

(f) M = 0.73. Continued.

$\delta_a = 6^o$; $\alpha = 0.73^o$; $C_L = 0.460$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.171	.395	0.000	1.118	.994	0.000	.095	.726	.050	-1.112	.410
.150	-1.360	.346	.012	-.202	.649	.012	-.311	.670	.150	-1.412	.332
.300	-1.223	.381	.025	-.702	.518	.025	-.564	.554	.300	-1.234	.379
.450	-.612	.541	.050	-1.092	.416	.050	-1.059	.424	.450	-.630	.537
.600	-.587	.548	.100	-1.335	.352	.100	-1.245	.376	.600	-.634	.535
.800	-.381	.602	.150	-1.306	.360	.150	-1.291	.364	.800	-.363	.606
.990	.071	.720	.200	-1.338	.351	.200	-1.249	.375			
			.300	-1.327	.354	.300	-1.268	.370			
			.350	-1.320	.356	.350	-1.274	.368			
			.400	-1.293	.363	.400	-1.254	.373			
			.450	-1.099	.414	.450	-1.173	.394			
			.500	-.594	.546	.500	-.685	.522			
			.550	-.579	.550	.550	-.630	.537			
			.600	-.636	.535	.600	-.616	.540			
			.650	-.624	.538	.700	-.460	.581			
			.700	-.577	.550	.800	-.226	.642			
			.800	-.354	.609	.900	-.158	.660			
			.900	-.053	.688	.950	-.160	.660			
			.550	.042	.712	.990	-.159	.661			
			.990	.081	.723						
					LOWER SURFACE						
.100	-.355	.609	.025	.044	.713	.025	.186	.750	.100	-.697	.519
.300	-.556	.556	.050	-.299	.623	.050	-.375	.603	.300	-.589	.547
.600	-.274	.630	.100	-.462	.581	.100	-.490	.573	.600	-.261	.636
.800	.190	.751	.200	-.580	.550	.200	-.573	.552	.800	.300	.780
			.300	-.628	.537	.300	-.639	.534			
			.400	-.622	.539	.400	-.612	.541			
			.500	-.616	.540	.500	-.496	.572			
			.600	-.239	.639	.600	-.186	.653			
			.700	.097	.727	.700	.142	.739			
			.800	.294	.778	.800	.350	.793			
			.900	.383	.802	.900	.385	.802			
			.550	.369	.798	.950	.381	.801			
			1.000	.089	.725						
CN=				.5236			.5718				
CM=				-.1095			-.1248				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(f) M = 0.73. Concluded.

$\delta_a = 6^o$; $\alpha = 2.49^o$; $C_L = 0.678$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.354	.345	0.000	1.068	.581	0.000	.097	.727	.050	-1.327	.354
.150	-1.519	.304	.012	-.390	.599	.012	-.495	.572	.150	-1.583	.287
.300	-1.434	.326	.025	-.933	.457	.025	-.739	.508	.300	-1.596	.284
.450	-1.032	.431	.050	-1.285	.365	.050	-1.254	.373	.450	-.680	.524
.600	-.500	.571	.100	-1.504	.308	.100	-1.448	.323	.600	-.612	.541
.800	-.334	.614	.150	-1.453	.321	.150	-1.470	.317	.800	-.344	.612
.990	.091	.725	.200	-1.503	.308	.200	-1.479	.327			
			.300	-1.497	.310	.300	-1.490	.312			
			.350	-1.504	.308	.350	-1.478	.315			
			.400	-1.505	.308	.400	-1.481	.314			
			.450	-1.316	.357	.450	-1.505	.308			
			.500	-.950	.453	.500	-1.083	.418			
			.550	-.823	.486	.550	-.812	.489			
			.600	-.681	.523	.600	-.702	.518			
			.650	-.567	.553	.700	-.473	.578			
			.700	-.435	.588	.800	-.294	.625			
			.800	-.231	.641	.900	-.155	.661			
			.900	-.054	.687	.950	-.130	.668			
			.950	.019	.706	.950	-.126	.669			
			.990	.056	.716						
					LOWER SURFACE						
.100	-.152	.659	.025	.273	.773	.025	.375	.800	.100	-.438	.587
.300	-.443	.586	.050	-.073	.682	.050	-.128	.668	.300	-.521	.565
.600	-.262	.633	.100	-.239	.639	.100	-.270	.631	.600	-.246	.637
.800	.211	.757	.200	-.408	.595	.200	-.406	.595	.800	.324	.786
			.300	-.495	.572	.300	-.498	.571			
			.400	-.529	.563	.400	-.535	.562			
			.500	-.575	.551	.500	-.441	.586			
			.600	-.217	.645	.600	-.174	.656			
			.700	.117	.732	.700	.162	.744			
			.800	.309	.782	.800	.410	.809			
			.900	.401	.807	.900	.419	.811			
			.550	.376	.800	.950	.405	.808			
			1.000	.076	.708						
CN=				.7055			.8054				
CM=				-.1088			-.1423				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(g) M = 0.75

$\delta_a = 0^o$; $\alpha = -4.88^o$; $C_L = -0.259$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.280	.613	0.000	1.101	.987	0.000	.087	.712	.050	-.247	.622
.150	-.514	.549	.012	.500	.824	.012	.444	.809	.150	-.443	.569
.300	-.543	.542	.025	.084	.712	.025	.165	.733	.300	-.571	.534
.450	-.491	.556	.050	-.248	.621	.050	-.203	.634	.450	-.554	.539
.600	-.545	.541	.100	-.376	.587	.100	-.332	.599	.600	-.613	.522
.800	-.368	.589	.150	-.444	.568	.150	-.367	.589	.800	-.337	.597
.990	.082	.711	.200	-.547	.540	.200	-.479	.559			
			.300	-.564	.536	.300	-.561	.537			
			.350	-.556	.538	.350	-.548	.540			
			.400	-.572	.534	.400	-.550	.540			
			.450	-.568	.535	.450	-.617	.522			
			.500	-.682	.504	.500	-.683	.504			
			.550	-.692	.501	.550	-.719	.494			
			.600	-.625	.519	.600	-.654	.512			
			.650	-.642	.515	.700	-.464	.563			
			.700	-.586	.530	.800	-.221	.629			
			.800	-.322	.601	.900	-.021	.683			
			.900	-.010	.686	.950	.000	.689			
			.950	.048	.702	.990	.018	.694			
			.990	.080	.710						
					LOWER SURFACE						
.100	-.986	.421	.025	-.520	.548	.025	-.452	.566	.100	-1.419	.304
.300	-1.320	.331	.050	-1.087	.394	.050	-1.032	.409	.300	-1.438	.299
.600	-.745	.622	.100	-1.238	.353	.100	-1.278	.342	.600	-.338	.597
.800	-.017	.686	.200	-1.310	.334	.200	-1.330	.328	.800	.119	.721
			.300	-1.391	.312	.300	-1.063	.401			
			.400	-.819	.467	.400	-.730	.491			
			.500	-.474	.560	.500	-.651	.512			
			.600	-.280	.613	.600	-.514	.549			
			.700	-.147	.649	.700	-.230	.626			
			.800	-.012	.685	.800	-.074	.669			
			.900	.139	.726	.900	.040	.699			
			.950	.109	.718	.950	.101	.716			
			1.000	.089	.713						
CN=				-.1935			-.2187				
CM=				-.0860			-.0543				

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = -3.26^o$; $C_L = -0.094$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.482	.558	0.000	1.121	.992	0.000	.088	.713	.050	-.500	.553
.150	-.686	.503	.012	.284	.766	.012	.271	.762	.150	-.625	.520
.300	-.627	.520	.025	-.094	.663	.025	-.026	.682	.300	-.651	.512
.450	-.542	.542	.050	-.455	.566	.050	-.476	.560	.450	-.557	.538
.600	-.556	.538	.100	-.582	.531	.100	-.548	.540	.600	-.589	.529
.800	-.326	.601	.150	-.581	.531	.150	-.523	.547	.800	-.302	.607
.950	.077	.710	.200	-.737	.489	.200	-.615	.522			
			.300	-.741	.488	.300	-.743	.488			
			.350	-.627	.519	.350	-.617	.522			
			.400	-.639	.516	.400	-.612	.523			
			.450	-.615	.522	.450	-.643	.515			
			.500	-.730	.491	.500	-.726	.492			
			.550	-.732	.491	.550	-.772	.480			
			.600	-.651	.513	.600	-.631	.518			
			.650	-.632	.518	.700	-.419	.575			
			.700	-.563	.536	.800	-.203	.634			
			.800	-.299	.608	.900	-.027	.681			
			.900	-.018	.684	.950	-.025	.682			
			.950	.056	.704	.990	.011	.692			
			.990	.088	.713						
					LOWER SURFACE						
.100	-.812	.469	.025	-.363	.590	.025	-.283	.612	.100	-1.275	.343
.300	-1.174	.384	.050	-.909	.443	.050	-.852	.458	.300	-1.306	.335
.600	-.728	.627	.100	-1.069	.399	.100	-1.146	.378	.600	-.365	.590
.800	.042	.700	.200	-1.131	.383	.200	-1.183	.368	.800	.193	.741
			.300	-1.263	.347	.300	-1.258	.348			
			.400	-1.278	.343	.400	-1.328	.329			
			.500	-.540	.543	.500	-.563	.536			
			.600	-.223	.629	.600	-.278	.614			
			.700	.019	.694	.700	-.028	.681			
			.800	.167	.734	.800	.052	.703			
			.900	.302	.771	.900	.192	.741			
			.950	.319	.775	.950	.273	.763			
			1.000	.106	.718						
CN=				-.0516			-.1049				
CM=				-.1067			-.0763				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = -1.46^o$; $C_L = 0.123$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.775	.479	0.000	1.121	.993	0.000	.105	.717	.050	-.771	.480
.150	-.965	.428	.012	.089	.713	.012	-.010	.686	.150	-.936	.435
.300	-.730	.491	.025	-.337	.598	.025	-.241	.624	.300	-.875	.452
.450	-.623	.520	.050	-.717	.495	.050	-.712	.496	.450	-.617	.522
.600	-.577	.533	.100	-.995	.419	.100	-.843	.461	.600	-.588	.530
.800	-.316	.603	.150	-.893	.447	.150	-.812	.469	.800	-.278	.614
.950	.053	.703	.200	-.957	.430	.200	-.783	.477			
			.300	-.975	.425	.300	-.920	.440			
			.350	-.957	.430	.350	-.891	.447			
			.400	-.816	.468	.400	-.840	.461			
			.450	-.672	.507	.450	-.675	.506			
			.500	-.758	.484	.500	-.717	.495			
			.550	-.777	.478	.550	-.766	.482			
			.600	-.647	.514	.600	-.646	.514			
			.650	-.614	.523	.700	-.417	.576			
			.700	-.551	.540	.800	-.215	.631			
			.800	-.272	.615	.900	-.063	.672			
			.900	-.024	.683	.950	-.042	.677			
			.950	.030	.697	.990	-.029	.681			
			.990	.064	.706						
					LOWER SURFACE						
.100	-.542	.542	.025	-.186	.639	.025	-.076	.668	.100	-1.061	.402
.300	-.937	.437	.050	-.637	.517	.050	-.677	.505	.300	-.738	.489
.600	-.222	.629	.100	-.845	.460	.100	-.913	.442	.600	-.379	.586
.800	.076	.710	.200	-.809	.470	.200	-.877	.451	.800	.169	.735
			.300	-.964	.428	.300	-1.055	.403			
			.400	-.578	.424	.400	-1.126	.384			
			.500	-.633	.518	.500	-.569	.535			
			.600	-.251	.621	.600	-.308	.605			
			.700	.050	.702	.700	.006	.690			
			.800	.177	.737	.800	.181	.738			
			.900	.291	.768	.900	.251	.757			
			.950	.316	.775	.950	.303	.771			
			1.000	.073	.709						
CN=				.1860			.1248				
CM=				-.0999			-.0853				

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = 0.66^o$; $C_L = 0.425$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.006	.416	0.000	1.122	.993	0.000	.108	.718	.050	-1.041	.407
.150	-1.235	.354	.012	-.146	.649	.012	-.210	.632	.150	-1.313	.333
.300	-1.210	.361	.025	-.605	.525	.025	-.466	.563	.300	-1.250	.350
.450	-1.065	.400	.050	-.985	.422	.050	-.951	.431	.450	-.663	.509
.600	-.517	.549	.100	-1.244	.352	.100	-1.165	.373	.600	-.575	.533
.800	-.309	.605	.150	-1.176	.370	.150	-1.172	.371	.800	-.274	.615
.950	.079	.710	.200	-1.232	.355	.200	-1.143	.379			
			.300	-1.263	.347	.300	-1.204	.363			
			.350	-1.242	.353	.350	-1.208	.362			
			.400	-1.228	.356	.400	-1.215	.360			
			.450	-1.235	.354	.450	-1.255	.349			
			.500	-1.295	.338	.500	-1.284	.341			
			.550	-.801	.472	.550	-.764	.482			
			.600	-.613	.523	.600	-.574	.533			
			.650	-.530	.545	.700	-.382	.586			
			.700	-.444	.569	.800	-.237	.625			
			.800	-.265	.617	.900	-.043	.677			
			.900	-.020	.683	.950	.000	.689			
			.950	.069	.707	.990	.026	.696			
			.990	.106	.718						
					LOWER SURFACE						
.100	-.247	.622	.025	.039	.699	.025	.203	.744	.100	-.752	.485
.300	-.598	.527	.050	-.332	.599	.050	-.412	.577	.300	-.696	.500
.600	-.255	.620	.100	-.517	.549	.100	-.535	.544	.600	-.377	.587
.800	.138	.726	.200	-.637	.516	.200	-.626	.519	.800	.222	.749
			.300	-.692	.501	.300	-.841	.461			
			.400	-.706	.498	.400	-.702	.499			
			.500	-.653	.512	.500	-.642	.515			
			.600	-.236	.625	.600	-.293	.609			
			.700	.085	.712	.700	.020	.694			
			.800	.242	.755	.800	.270	.762			
			.900	.336	.780	.900	.338	.781			
			.950	.357	.785	.950	.357	.786			
			1.000	.094	.714						
CN=				.4802			.4556				
CM=				-.1071			-.0965				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = 1.40^o$; $C_L = 0.500$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.127	.383	0.000	1.116	.991	0.000	.113	.719	.050	-1.108	.389
.150	-1.297	.337	.012	-.226	.627	.012	-.276	.614	.150	-1.402	.309
.300	-1.279	.342	.025	-.689	.502	.025	-.546	.541	.300	-1.393	.311
.450	-1.188	.367	.050	-1.054	.403	.050	-1.056	.403	.450	-.682	.504
.600	-.501	.553	.100	-1.304	.335	.100	-1.230	.355	.600	-.534	.544
.800	-.311	.605	.150	-1.277	.343	.150	-1.251	.350	.800	-.259	.619
.950	.082	.711	.200	-1.299	.337	.200	-1.223	.357			
			.300	-1.319	.331	.300	-1.255	.349			
			.350	-1.309	.334	.350	-1.279	.342			
			.400	-1.319	.331	.400	-1.289	.339			
			.450	-1.319	.331	.450	-1.322	.331			
			.500	-1.285	.340	.500	-1.344	.325			
			.550	-.779	.478	.550	-.764	.482			
			.600	-.657	.511	.600	-.599	.527			
			.650	-.570	.534	.700	-.391	.583			
			.700	-.447	.568	.800	-.245	.622			
			.800	-.236	.625	.900	-.052	.675			
			.900	-.044	.677	.950	.003	.690			
			.950	-.010	.686	.990	.036	.699			
			.990	.051	.703						
					LOWER SURFACE						
.100	-.240	.624	.025	.109	.718	.025	.246	.756	.100	-.658	.511
.300	-.562	.536	.050	-.220	.629	.050	-.318	.603	.300	-.652	.512
.600	-.242	.623	.100	-.405	.579	.100	-.476	.560	.600	-.380	.586
.800	.165	.733	.200	-.542	.542	.200	-.571	.534	.800	.230	.751
			.300	-.646	.514	.300	-.761	.483			
			.400	-.656	.511	.400	-.718	.494			
			.500	-.647	.513	.500	-.626	.519			
			.600	-.264	.617	.600	-.298	.608			
			.700	.085	.712	.700	.035	.698			
			.800	.246	.755	.800	.278	.764			
			.900	.351	.784	.900	.340	.781			
			.950	.335	.780	.950	.382	.792			
			1.000	.077	.710						
CN=				.5517			.5249				
CM=				-.1070			-.0996				

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = 1.99^o$; $C_L = 0.534$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.175	.371	0.000	1.110	.990	0.000	.099	.716	.050	-1.179	.370
.150	-1.353	.323	.012	-.275	.614	.012	-.351	.594	.150	-1.432	.301
.300	-1.319	.332	.025	-.752	.485	.025	-.573	.534	.300	-1.446	.297
.450	-1.132	.382	.050	-1.107	.389	.050	-1.086	.395	.450	-.679	.505
.600	-.481	.559	.100	-1.357	.322	.100	-1.281	.342	.600	-.536	.544
.800	-.298	.608	.150	-1.318	.332	.150	-1.303	.336	.800	-.275	.615
.950	-.003	.688	.200	-1.365	.319	.200	-1.311	.334			
			.300	-1.377	.316	.300	-1.330	.329			
			.350	-1.365	.319	.350	-1.326	.330			
			.400	-1.289	.340	.400	-1.336	.327			
			.450	-1.010	.415	.450	-1.389	.313			
			.500	-.782	.477	.500	-1.160	.375			
			.550	-.705	.498	.550	-.765	.482			
			.600	-.668	.508	.600	-.656	.511			
			.650	-.532	.545	.700	-.407	.579			
			.700	-.442	.569	.800	-.275	.615			
			.800	-.279	.613	.900	-.061	.672			
			.900	-.109	.660	.950	-.004	.688			
			.950	-.064	.672	.990	.017	.694			
			.990	-.040	.678						
					LOWER SURFACE						
.100	-.191	.637	.025	.186	.739	.025	.278	.764	.100	-.584	.531
.300	-.546	.541	.050	-.152	.648	.050	-.267	.617	.300	-.615	.523
.600	-.265	.617	.100	-.327	.600	.100	-.389	.584	.600	-.381	.586
.800	.145	.728	.200	-.502	.553	.200	-.530	.545	.800	.218	.748
			.300	-.608	.524	.300	-.728	.492			
			.400	-.637	.517	.400	-.690	.502			
			.500	-.666	.509	.500	-.605	.525			
			.600	-.249	.622	.600	-.295	.609			
			.700	.079	.710	.700	.027	.696			
			.800	.250	.757	.800	.281	.765			
			.900	.313	.774	.900	.346	.783			
			.950	.331	.779	.950	.379	.792			
			1.000	-.084	.666						
CN=				.5558			.5762				
CM=				-.0988			-.1013				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = 3.09^o$; $C_L = 0.580$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.293	.339	0.000	1.088	.584	0.000	.084	.712	.050	-1.250	.350
.150	-1.448	.297	.012	-.388	.584	.012	-.478	.559	.150	-1.530	.274
.300	-1.399	.310	.025	-.850	.458	.025	-.691	.502	.300	-1.551	.269
.450	-.793	.474	.050	-1.213	.360	.050	-1.167	.373	.450	-.696	.500
.600	-.454	.566	.100	-1.452	.295	.100	-1.376	.316	.600	-.512	.550
.800	-.294	.609	.150	-1.408	.307	.150	-1.395	.311	.800	-.270	.616
.990	-.039	.678	.200	-1.447	.297	.200	-1.336	.327			
			.300	-1.420	.304	.300	-1.403	.309			
			.350	-.924	.439	.350	-1.420	.304			
			.400	-.767	.481	.400	-1.416	.305			
			.450	-.803	.471	.450	-.943	.433			
			.500	-.718	.494	.500	-.824	.466			
			.550	-.685	.503	.550	-.734	.490			
			.600	-.620	.521	.600	-.643	.515			
			.650	-.627	.519	.700	-.436	.571			
			.700	-.471	.561	.800	-.316	.603			
			.800	-.334	.598	.900	-.150	.648			
			.900	-.197	.635	.950	-.129	.654			
			.950	-.256	.619	.990	-.129	.654			
			.990	-.180	.640						
					LOWER SURFACE						
.100	-.107	.660	.025	.261	.760	.025	.391	.795	.100	-.478	.559
.300	-.501	.553	.050	-.035	.679	.050	-.139	.651	.300	-.589	.529
.600	-.348	.595	.100	-.246	.622	.100	-.304	.607	.600	-.379	.586
.800	.172	.735	.200	-.413	.577	.200	-.440	.570	.800	.237	.753
			.300	-.559	.537	.300	-.576	.533			
			.400	-.614	.522	.400	-.646	.514			
			.500	-.691	.501	.500	-.626	.519			
			.600	-.290	.610	.600	-.317	.603			
			.700	.050	.702	.700	.011	.692			
			.800	.252	.757	.800	.276	.764			
			.900	.364	.787	.900	.333	.779			
			.950	.305	.772	.950	.362	.787			
			1.000	-.151	.648						
CN=				.5658			.6268				
CM=				-.1024			-.0996				

(g) M = 0.75. Continued.

$\delta_a = 0^o$; $\alpha = 4.22^o$; $C_L = 0.639$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.421	.304	0.000	1.056	.575	0.000	.074	.709	.050	-1.353	.322
.150	-1.532	.274	.012	-.495	.555	.012	-.563	.536	.150	-1.590	.258
.300	-1.239	.353	.025	-.981	.423	.025	-.757	.484	.300	-1.613	.252
.450	-.785	.476	.050	-1.315	.333	.050	-1.243	.352	.450	-.680	.505
.600	-.506	.552	.100	-1.514	.279	.100	-1.441	.298	.600	-.490	.556
.800	-.294	.609	.150	-1.504	.282	.150	-1.481	.288	.800	-.313	.604
.990	-.146	.649	.200	-1.487	.286	.200	-1.452	.296			
			.300	-1.114	.387	.300	-1.469	.291			
			.350	-.940	.434	.350	-1.370	.318			
			.400	-.910	.442	.400	-.907	.443			
			.450	-.850	.459	.450	-.827	.465			
			.500	-.745	.487	.500	-.794	.474			
			.550	-.740	.488	.550	-.742	.488			
			.600	-.619	.521	.600	-.635	.517			
			.650	-.599	.527	.700	-.470	.562			
			.700	-.622	.521	.800	-.318	.603			
			.800	-.417	.576	.900	-.261	.618			
			.900	-.291	.610	.950	-.235	.625			
			.950	-.226	.628	.990	-.164	.644			
			.990	-.222	.629						
					LOWER SURFACE						
.100	.016	.693	.025	.376	.791	.025	.499	.824	.100	-.354	.593
.300	-.450	.567	.050	.050	.702	.050	-.027	.682	.300	-.553	.539
.600	-.319	.602	.100	-.155	.647	.100	-.149	.648	.600	-.399	.581
.800	.160	.732	.200	-.360	.591	.200	-.347	.595	.800	.239	.754
			.300	-.504	.552	.300	-.521	.548			
			.400	-.573	.534	.400	-.597	.527			
			.500	-.694	.501	.500	-.616	.522			
			.600	-.310	.605	.600	-.330	.600			
			.700	.036	.699	.700	-.014	.685			
			.800	.242	.755	.800	.270	.762			
			.900	.353	.784	.900	.343	.782			
			.950	.307	.772	.950	.337	.780			
			1.000	-.175	.641						
CN=				.6315			.6690				
CM=				-.1115			-.0961				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(g) M = 0.75. Concluded.

$\delta_a = 0^o$; $\alpha = 5.38^o$; $C_L = 0.707$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.542	.272	0.000	1.015	.964	0.000	.049	.702	.050	-1.480	.288
.150	-1.128	.386	.012	-.602	.526	.012	-.738	.489	.150	-1.723	.223
.300	-.834	.463	.025	-1.075	.398	.025	-.928	.438	.300	-1.694	.231
.450	-.709	.497	.050	-1.408	.308	.050	-1.338	.327	.450	-.877	.452
.600	-.575	.533	.100	-1.599	.256	.100	-1.546	.270	.600	-.518	.549
.800	-.236	.625	.150	-1.569	.264	.150	-1.555	.268	.800	-.335	.598
.950	-.231	.626	.200	-1.608	.254	.200	-1.557	.268			
			.300	-1.091	.394	.300	-1.395	.311			
			.350	-1.031	.410	.350	-1.111	.388			
			.400	-.973	.426	.400	-.965	.428			
			.450	-.899	.446	.450	-.935	.436			
			.500	-.788	.476	.500	-.809	.470			
			.550	-.663	.510	.550	-.700	.499			
			.600	-.745	.488	.600	-.663	.510			
			.650	-.485	.558	.700	-.480	.559			
			.700	-.405	.579	.800	-.401	.580			
			.800	-.371	.589	.900	-.303	.607			
			.900	-.265	.617	.950	-.262	.618			
			.950	-.249	.622	.990	-.232	.626			
			.990	-.209	.633						
					LOWER SURFACE						
.100	.068	.707	.025	.443	.809	.025	.581	.846	.100	-.261	.618
.300	-.400	.581	.050	.177	.737	.050	.086	.712	.300	-.479	.559
.600	-.359	.592	.100	-.030	.681	.100	-.104	.661	.600	-.405	.580
.800	.169	.735	.200	-.263	.618	.200	-.294	.610	.800	.239	.754
			.300	-.450	.567	.300	-.473	.561			
			.400	-.540	.543	.400	-.588	.530			
			.500	-.681	.505	.500	-.601	.526			
			.600	-.317	.603	.600	-.343	.596			
			.700	.062	.706	.700	-.023	.683			
			.800	.259	.759	.800	.274	.763			
			.900	.346	.783	.900	.318	.775			
			.950	.315	.774	.950	.333	.779			
			1.000	-.201	.635						
CN=				.6716			.7235				
CM=				-.0942			-.0996				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76

$\delta_a = -6^o$; $\alpha = -4.78^o$; $C_L = -0.254$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.287	.602	0.000	1.113	.989	0.000	.089	.705	.050	-.260	.610
.150	-.500	.544	.012	.490	.817	.012	.427	.800	.150	-.483	.548
.300	-.562	.526	.025	.083	.704	.025	.147	.722	.300	-.583	.521
.450	-.451	.557	.050	-.265	.608	.050	-.239	.616	.450	-.555	.528
.600	-.566	.525	.100	-.396	.575	.100	-.361	.582	.600	-.552	.529
.800	-.382	.576	.150	-.468	.552	.150	-.399	.571	.800	-.256	.611
.950	.068	.700	.200	-.543	.532	.200	-.496	.545			
			.300	-.582	.521	.300	-.594	.518			
			.350	-.595	.517	.350	-.571	.524			
			.400	-.587	.519	.400	-.556	.528			
			.450	-.554	.529	.450	-.614	.512			
			.500	-.736	.478	.500	-.690	.491			
			.550	-.780	.466	.550	-.775	.468			
			.600	-.839	.505	.600	-.674	.496			
			.650	-.675	.495	.700	-.385	.575			
			.700	-.647	.503	.800	-.281	.604			
			.800	-.329	.591	.900	-.129	.646			
			.900	-.015	.672	.950	-.029	.674			
			.950	.031	.690	.990	.044	.694			
			.990	.078	.703						
					LOWER SURFACE						
.100	-.941	.422	.025	-.478	.550	.025	-.375	.578	.100	-1.345	.310
.300	-1.282	.328	.050	-1.026	.398	.050	-.965	.415	.300	-1.399	.295
.600	-.299	.593	.100	-1.207	.348	.100	-1.220	.345	.600	-.413	.568
.800	-.028	.674	.200	-1.262	.333	.200	-1.297	.324	.800	-.050	.668
			.300	-1.333	.314	.300	-1.384	.299			
			.400	-.805	.459	.400	-1.163	.360			
			.500	-.625	.509	.500	-.611	.513			
			.600	-.438	.561	.600	-.384	.576			
			.700	-.199	.627	.700	-.210	.624			
			.800	-.014	.678	.800	-.060	.665			
			.900	.079	.704	.900	.030	.690			
			.950	.108	.712	.950	.102	.710			
			1.000	.089	.706						
CN=				-.1999			-.2383				
CM=				-.0792			-.0581				

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = -3.36^o$; $C_L = -0.140$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.493	.546	0.000	1.126	.993	0.000	.096	.709	.050	-.435	.562
.150	-.698	.499	.012	.345	.777	.012	.277	.758	.150	-.605	.515
.300	-.647	.503	.025	-.076	.661	.025	.000	.682	.300	-.760	.472
.450	-.510	.541	.050	-.424	.565	.050	-.416	.567	.450	-.572	.524
.600	-.564	.526	.100	-.553	.528	.100	-.545	.531	.600	-.531	.535
.800	-.339	.598	.150	-.582	.521	.150	-.522	.538	.800	-.219	.621
.950	.071	.701	.200	-.729	.481	.200	-.616	.512			
			.300	-.763	.471	.300	-.740	.478			
			.350	-.645	.504	.350	-.694	.490			
			.400	-.620	.511	.400	-.587	.520			
			.450	-.583	.521	.450	-.646	.504			
			.500	-.774	.468	.500	-.713	.485			
			.550	-.812	.458	.550	-.761	.472			
			.600	-.628	.508	.600	-.597	.517			
			.650	-.614	.512	.700	-.324	.592			
			.700	-.522	.538	.800	-.218	.622			
			.800	-.279	.605	.900	-.051	.668			
			.900	.004	.683	.950	.052	.696			
			.950	.064	.699	.990	.126	.717			
			.990	.086	.705						
					LOWER SURFACE						
.100	-.800	.461	.025	-.354	.534	.025	-.252	.612	.100	-1.246	.338
.300	-1.118	.373	.050	-.890	.436	.050	-.827	.453	.300	-1.330	.315
.600	-.265	.609	.100	-1.050	.392	.100	-1.131	.370	.600	-.434	.562
.800	.031	.690	.200	-1.150	.364	.200	-1.176	.357	.800	.057	.697
			.300	-1.203	.350	.300	-1.261	.334			
			.400	-.851	.447	.400	-.872	.441			
			.500	-.497	.545	.500	-.653	.501			
			.600	-.361	.582	.600	-.433	.548			
			.700	-.233	.617	.700	-.272	.607			
			.800	-.067	.663	.800	-.071	.662			
			.900	.029	.690	.900	.055	.697			
			.950	.151	.724	.950	.141	.721			
			1.000	.091	.707						
CN=				-.0956			-.1589				
CM=				-.0620			-.0346				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = -1.66^o$; $C_L = 0.063$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.717	.496	0.000	1.139	.956	0.000	.100	.709	.050	-.656	.501
.150	-.931	.425	.012	.176	.730	.012	.081	.704	.150	-.584	.410
.300	-.746	.476	.025	-.299	.599	.025	-.210	.624	.300	-.819	.456
.450	-.583	.521	.050	-.642	.504	.050	-.662	.499	.450	-.612	.513
.600	-.562	.527	.100	-.538	.423	.100	-.811	.458	.600	-.514	.540
.800	-.313	.595	.150	-.821	.455	.150	-.771	.469	.800	-.187	.630
.950	.078	.703	.200	-.846	.448	.200	-.740	.478			
			.300	-.905	.432	.300	-.685	.437			
			.350	-.898	.434	.350	-.901	.433			
			.400	-.835	.451	.400	-.856	.445			
			.450	-.657	.489	.450	-.776	.468			
			.500	-.687	.492	.500	-.674	.496			
			.550	-.706	.497	.550	-.637	.506			
			.600	-.602	.516	.600	-.546	.531			
			.650	-.605	.515	.700	-.288	.602			
			.700	-.503	.543	.800	-.184	.631			
			.800	-.248	.613	.900	-.008	.680			
			.900	.002	.682	.950	.091	.707			
			.950	.063	.659	.990	.154	.724			
			.990	.091	.707						
					LOWER SURFACE						
.100	-.616	.512	.025	-.205	.625	.025	-.099	.555	.100	-1.090	.381
.300	-.938	.423	.050	-.688	.492	.050	-.664	.498	.300	-1.134	.369
.600	-.242	.615	.100	-.869	.442	.100	-.975	.413	.600	-.454	.556
.800	.054	.697	.200	-.909	.431	.200	-.885	.437	.800	.064	.699
			.300	-1.030	.398	.300	-1.067	.387			
			.400	-1.093	.380	.400	-1.187	.354			
			.500	-.573	.524	.500	-.940	.422			
			.600	-.202	.626	.600	-.368	.580			
			.700	-.068	.663	.700	-.102	.654			
			.800	.045	.694	.800	.141	.721			
			.900	.197	.736	.900	.221	.743			
			.950	.252	.751	.950	.303	.765			
			1.000	.110	.712						
CN=				.0801			-.0028				
CM=				-.0745			-.0449				

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = -0.32^o$; $C_L = 0.336$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.947	.424	0.000	1.133	.995	0.000	.105	.711	.050	-.699	.434
.150	-1.171	.359	.012	-.014	.678	.012	-.129	.647	.150	-1.228	.344
.300	-1.127	.371	.025	-.525	.537	.025	-.398	.572	.300	-1.224	.345
.450	-.994	.408	.050	-.911	.431	.050	-.891	.437	.450	-.615	.513
.600	-.698	.545	.100	-1.149	.365	.100	-1.067	.383	.600	-.497	.545
.800	-.336	.589	.150	-1.118	.374	.150	-1.080	.384	.800	-.180	.633
.950	.089	.707	.200	-1.164	.361	.200	-1.062	.389			
			.300	-1.192	.353	.300	-1.146	.366			
			.350	-1.179	.357	.350	-1.154	.364			
			.400	-1.176	.358	.400	-1.134	.369			
			.450	-1.123	.373	.450	-1.186	.355			
			.500	-1.236	.341	.500	-1.190	.354			
			.550	-.889	.437	.550	-.629	.509			
			.600	-.551	.530	.600	-.478	.550			
			.650	-.474	.551	.700	-.262	.610			
			.700	-.412	.569	.800	-.170	.635			
			.800	-.241	.616	.900	-.008	.680			
			.900	-.006	.680	.950	.087	.706			
			.950	.064	.700	.990	.156	.725			
			.990	.092	.707						
					LOWER SURFACE						
.100	-.355	.584	.025	.010	.685	.025	.114	.714	.100	-.828	.454
.300	-.690	.492	.050	-.408	.570	.050	-.440	.561	.300	-.758	.473
.600	-.236	.617	.100	-.528	.537	.100	-.601	.517	.600	-.460	.555
.800	.099	.709	.200	-.708	.487	.200	-.721	.483	.800	.054	.697
			.300	-.747	.476	.300	-.882	.439			
			.400	-.861	.445	.400	-.993	.408			
			.500	-.766	.471	.500	-.743	.477			
			.600	-.217	.622	.600	-.399	.572			
			.700	.054	.697	.700	-.101	.654			
			.800	.159	.726	.800	.168	.729			
			.900	.257	.764	.900	.256	.753			
			.950	.324	.771	.950	.330	.773			
			1.000	.122	.716						
CN=				.3850			.2719				
CM=				-.0914			-.0511				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = 1.69^o$; $C_L = 0.450$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.106	.378	0.000	1.121	.551	0.000	.099	.710	.050	-1.034	.397
.150	-1.408	.322	.012	-.177	.634	.012	-.285	.604	.150	-1.362	.307
.300	-1.254	.337	.025	-.667	.498	.025	-.532	.536	.300	-1.401	.296
.450	-1.014	.403	.050	-1.039	.396	.050	-1.022	.401	.450	-.712	.486
.600	-.458	.556	.100	-1.288	.327	.100	-1.229	.344	.600	-.458	.556
.800	-.422	.594	.150	-1.263	.334	.150	-1.225	.345	.800	-.172	.635
.950	.058	.634	.200	-1.290	.327	.200	-1.210	.349			
			.300	-1.317	.319	.300	-1.264	.334			
			.350	-1.307	.322	.350	-1.277	.330			
			.400	-1.290	.327	.400	-1.266	.333			
			.450	-1.167	.361	.450	-1.318	.319			
			.500	-.810	.459	.500	-1.043	.355			
			.550	-.711	.486	.550	-.694	.491			
			.600	-.638	.506	.600	-.588	.520			
			.650	-.548	.531	.700	-.323	.593			
			.700	-.448	.559	.800	-.162	.638			
			.800	-.204	.626	.900	-.013	.679			
			.900	-.097	.656	.950	.073	.703			
			.950	-.078	.661	.990	.144	.722			
			.990	-.014	.679						
					LOWER SURFACE						
.100	-.239	.616	.025	.131	.718	.025	.262	.755	.100	-.638	.507
.300	-.613	.513	.050	-.213	.624	.050	-.279	.605	.300	-.753	.475
.600	-.276	.606	.100	-.403	.571	.100	-.447	.559	.600	-.440	.550
.800	.134	.719	.200	-.586	.521	.200	-.588	.520	.800	.058	.709
			.300	-.677	.496	.300	-.807	.460			
			.400	-.799	.467	.400	-.897	.435			
			.500	-.819	.457	.500	-.782	.467			
			.600	-.266	.609	.600	-.418	.567			
			.700	.055	.693	.700	-.111	.652			
			.800	.204	.739	.800	.184	.733			
			.900	.327	.773	.900	.273	.758			
			.950	.339	.776	.950	.340	.776			
			1.000	-.025	.676						
CN=				.4611			.3949				
CM=				-.0855			-.0521				

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = 2.82^o$; $C_L = 0.511$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.221	.346	0.000	1.100	.586	0.000	.090	.707	.050	-1.138	.369
.150	-1.386	.300	.012	-.277	.606	.012	-.375	.579	.150	-1.426	.289
.300	-1.435	.314	.025	-.771	.470	.025	-.601	.517	.300	-1.480	.274
.450	-.868	.443	.050	-1.131	.370	.050	-1.115	.375	.450	-.744	.477
.600	-.435	.562	.100	-1.332	.299	.100	-1.299	.324	.600	-.436	.562
.800	-.259	.611	.150	-1.343	.312	.150	-1.333	.315	.800	-.174	.634
.950	-.087	.658	.200	-1.365	.306	.200	-1.307	.324			
			.300	-1.287	.328	.300	-1.321	.318			
			.350	-1.175	.358	.350	-1.362	.307			
			.400	-.776	.468	.400	-1.205	.350			
			.450	-.716	.485	.450	-.808	.460			
			.500	-.694	.491	.500	-.758	.473			
			.550	-.690	.492	.550	-.707	.487			
			.600	-.638	.506	.600	-.633	.508			
			.650	-.546	.532	.700	-.412	.571			
			.700	-.541	.533	.800	-.256	.612			
			.800	-.352	.585	.900	-.102	.654			
			.900	-.211	.624	.950	-.011	.679			
			.950	-.200	.627	.990	.027	.690			
			.990	-.198	.628						
					LOWER SURFACE						
.100	-.393	.657	.025	.220	.743	.025	.349	.779	.100	-.533	.535
.300	-.536	.535	.050	-.096	.656	.050	-.185	.631	.300	-.667	.498
.600	-.291	.602	.100	-.309	.597	.100	-.348	.587	.600	-.508	.542
.800	.165	.729	.200	-.477	.551	.200	-.513	.541	.800	.088	.707
			.300	-.625	.510	.300	-.741	.478			
			.400	-.705	.488	.400	-.792	.464			
			.500	-.892	.436	.500	-.808	.459			
			.600	-.241	.605	.600	-.442	.560			
			.700	.044	.654	.700	-.141	.643			
			.800	.210	.740	.800	.171	.729			
			.900	.322	.771	.900	.262	.754			
			.950	.305	.766	.950	.315	.769			
			1.000	-.132	.646						
CN=				.4943			.4463				
CM=				-.0565			-.0536				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -6^o$; $\alpha = 4.09^o$; $C_L = 0.597$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.350	.409	0.000	1.075	.578	0.000	.079	.704	.050	-1.250	.337
.150	-1.501	.268	.012	-.406	.570	.012	-.508	.542	.150	-1.525	.261
.300	-1.430	.287	.025	-.883	.438	.025	-.713	.485	.300	-1.555	.253
.450	-.769	.470	.050	-1.275	.330	.050	-1.188	.354	.450	-.838	.451
.600	-.468	.553	.100	-1.466	.277	.100	-1.397	.297	.600	-.419	.566
.800	-.229	.619	.150	-1.416	.291	.150	-1.413	.292	.800	-.214	.623
.950	-.052	.668	.200	-1.477	.274	.200	-1.397	.297			
			.300	-1.475	.275	.300	-1.081	.384			
			.350	-1.330	.301	.350	-.917	.429			
			.400	-.914	.430	.400	-.835	.451			
			.450	-.823	.455	.450	-.795	.463			
			.500	-.711	.486	.500	-.769	.470			
			.550	-.714	.485	.550	-.751	.475			
			.600	-.680	.494	.600	-.679	.494			
			.650	-.535	.534	.700	-.572	.524			
			.700	-.516	.539	.800	-.415	.567			
			.800	-.391	.574	.900	-.242	.615			
			.900	-.274	.606	.950	-.182	.632			
			.950	-.226	.603	.990	-.105	.653			
			.990	-.132	.632						
					LOWER SURFACE						
.100	-.021	.676	.025	.347	.778	.025	.444	.804	.100	-.397	.572
.300	-.470	.552	.050	.020	.687	.050	-.027	.674	.300	-.595	.518
.600	-.342	.588	.100	-.194	.628	.100	-.233	.618	.500	-.570	.525
.800	.140	.721	.200	-.376	.578	.200	-.409	.569	.800	.064	.700
			.300	-.531	.535	.300	-.414	.513			
			.400	-.641	.505	.400	-.712	.486			
			.500	-.903	.433	.500	-.802	.461			
			.600	-.314	.595	.600	-.494	.546			
			.700	.041	.693	.700	-.173	.633			
			.800	.227	.744	.800	.142	.721			
			.900	.337	.775	.900	.249	.751			
			.950	.308	.767	.950	.282	.760			
			1.000	-.177	.633						
CN=				.6084			.5049				
CM=				-.1061			-.0681				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = -4.73^o$; $C_L = -0.236$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.327	.592	0.000	1.115	.989	0.000	.091	.707	.050	-.265	.609
.150	-.524	.537	.012	.434	.815	.012	.416	.796	.150	-.484	.548
.300	-.560	.527	.025	.059	.761	.025	.146	.722	.300	-.590	.519
.450	-.489	.547	.050	-.233	.617	.050	-.241	.615	.450	-.559	.527
.600	-.572	.524	.100	-.415	.566	.100	-.380	.577	.600	-.616	.512
.800	-.362	.582	.150	-.438	.549	.150	-.399	.572	.900	-.330	.591
.950	.052	.696	.200	-.550	.530	.200	-.493	.546			
			.300	-.587	.520	.300	-.603	.515			
			.350	-.574	.522	.350	-.586	.520			
			.400	-.564	.519	.400	-.570	.525			
			.450	-.555	.528	.450	-.629	.508			
			.500	-.742	.477	.500	-.706	.487			
			.550	-.777	.467	.550	-.811	.459			
			.600	-.652	.502	.600	-.813	.457			
			.650	-.700	.488	.700	-.475	.551			
			.700	-.605	.515	.800	-.336	.589			
			.800	-.329	.591	.900	-.109	.652			
			.900	-.035	.672	.950	-.023	.675			
			.950	.049	.695	.990	.024	.689			
			.990	.090	.706						
					LOWER SURFACE						
.100	-.934	.423	.025	-.473	.551	.025	-.381	.577	.100	-1.338	.313
.300	-1.275	.338	.050	-1.016	.491	.050	-.943	.420	.300	-1.410	.293
.600	-.340	.591	.100	-1.174	.358	.100	-1.227	.343	.600	-.382	.576
.800	-.014	.678	.200	-1.276	.330	.200	-1.287	.327	.800	.033	.691
			.300	-1.180	.356	.300	-.945	.421			
			.400	-.735	.479	.400	-.677	.495			
			.500	-.575	.523	.500	-.604	.515			
			.600	-.359	.583	.600	-.503	.543			
			.700	-.243	.616	.700	-.369	.580			
			.800	-.045	.672	.800	-.186	.631			
			.900	.151	.723	.900	-.066	.664			
			.950	.115	.719	.950	.015	.686			
			1.000	.114	.713						
CN=				-.1904			-.1691				
CM=				-.0846			-.0508				

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = -3.29^o$; $C_L = -0.117$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.481	.549	0.000	1.136	.995	0.000	.094	.708	.050	-.465	.554
.150	-.654	.501	.012	.340	.776	.012	.286	.761	.150	-.628	.509
.300	-.641	.505	.025	-.037	.666	.025	-.007	.680	.300	-.774	.468
.450	-.527	.534	.050	-.476	.551	.050	-.445	.559	.450	-.590	.519
.600	-.566	.526	.100	-.579	.522	.100	-.544	.532	.600	-.589	.519
.800	-.343	.587	.150	-.571	.524	.150	-.529	.536	.800	-.281	.604
.950	.065	.703	.200	-.743	.478	.200	-.634	.515			
			.300	-.750	.475	.300	-.765	.471			
			.350	-.753	.474	.350	-.738	.478			
			.400	-.678	.495	.400	-.595	.518			
			.450	-.576	.523	.450	-.645	.504			
			.500	-.774	.469	.500	-.725	.482			
			.550	-.834	.452	.550	-.830	.453			
			.600	-.687	.492	.600	-.732	.480			
			.650	-.639	.506	.700	-.397	.572			
			.700	-.535	.534	.800	-.245	.614			
			.800	-.265	.609	.900	-.020	.676			
			.900	-.091	.682	.950	.063	.699			
			.950	.066	.700	.990	.095	.709			
			.990	.062	.699						
					LOWER SURFACE						
.100	-.803	.460	.025	-.341	.598	.025	-.242	.615	.100	-1.232	.342
.300	-1.143	.367	.050	-.331	.439	.050	-.801	.461	.300	-1.312	.320
.600	-.261	.610	.100	-1.045	.394	.100	-1.108	.376	.600	-.409	.569
.800	-.004	.681	.200	-1.106	.377	.200	-1.175	.358	.800	.101	.710
			.300	-1.133	.353	.300	-1.247	.333			
			.400	-1.276	.330	.400	-.677	.495			
			.500	-.530	.536	.500	-.562	.527			
			.600	-.283	.604	.600	-.422	.565			
			.700	-.084	.659	.700	-.251	.613			
			.800	.024	.688	.800	-.080	.660			
			.900	.183	.732	.900	.040	.693			
			.950	.258	.753	.950	.117	.714			
			1.000	.102	.710						
CN=				-.0675			-.0942				
CM=				-.0944			-.0484				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = -1.60^o$; $C_L = 0.092$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.722	.482	0.000	1.138	.996	0.000	.099	.709	.050	-.685	.492
.150	-.923	.427	.012	.173	.729	.012	.679	.703	.150	-1.023	.399
.300	-.705	.487	.025	-.309	.596	.025	-.183	.631	.300	-.697	.489
.450	-.703	.487	.050	-.678	.494	.050	-.657	.500	.450	-.629	.508
.600	-.562	.526	.100	-.954	.417	.100	-.852	.446	.600	-.564	.526
.800	-.319	.594	.150	-.841	.449	.150	-.786	.465	.800	-.240	.615
.950	.065	.700	.200	-.909	.431	.200	-.794	.462			
			.300	-.915	.429	.300	-.902	.432			
			.350	-.925	.426	.350	-.894	.435			
			.400	-.880	.439	.400	-.880	.434			
			.450	-.785	.465	.450	-.882	.433			
			.500	-.855	.445	.500	-.790	.463			
			.550	-.692	.490	.550	-.697	.489			
			.600	-.597	.517	.600	-.591	.518			
			.650	-.610	.513	.700	-.353	.584			
			.700	-.539	.533	.800	-.214	.623			
			.800	-.261	.610	.900	-.003	.681			
			.900	-.001	.681	.950	.055	.697			
			.950	.058	.698	.990	.087	.706			
			.990	.088	.706						
					LOWER SURFACE						
.100	-.558	.528	.025	-.193	.628	.025	-.068	.663	.100	-1.080	.383
.300	-.962	.416	.050	-.641	.504	.050	-.653	.500	.300	-1.091	.380
.600	-.232	.618	.100	-.840	.450	.100	-.937	.423	.600	-.422	.565
.800	.040	.690	.200	-.921	.427	.200	-.901	.433	.900	.109	.712
			.300	-1.026	.398	.300	-1.038	.395			
			.400	-1.092	.383	.400	-1.169	.359			
			.500	-.596	.517	.500	-.670	.496			
			.600	-.199	.628	.600	-.304	.598			
			.700	.001	.682	.700	-.101	.654			
			.800	.106	.711	.800	.122	.715			
			.900	.275	.758	.900	.234	.745			
			.950	.293	.764	.950	.286	.760			
			1.000	.107	.711						
CN=				.1357			.0722				
CM=				-.0916			-.0622				

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 0.04^o$; $C_L = 0.326$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.941	.422	0.000	1.137	.996	0.000	.103	.710	.050	-.880	.438
.150	-1.159	.362	.012	-.016	.677	.012	-.104	.653	.150	-1.205	.349
.300	-1.085	.382	.025	-.457	.544	.025	-.376	.578	.300	-1.177	.356
.450	-.974	.413	.050	-.858	.442	.050	-.870	.441	.450	-.648	.503
.600	-.517	.540	.100	-1.145	.365	.100	-1.041	.394	.600	-.560	.527
.800	-.336	.589	.150	-1.092	.380	.150	-1.066	.387	.800	-.242	.615
.950	.074	.702	.200	-1.131	.369	.200	-1.026	.398			
			.300	-1.145	.365	.300	-1.136	.368			
			.350	-1.134	.369	.350	-1.136	.368			
			.400	-1.126	.371	.400	-1.143	.366			
			.450	-1.118	.373	.450	-1.173	.358			
			.500	-1.204	.349	.500	-1.191	.353			
			.550	-1.104	.377	.550	-.843	.449			
			.600	-.572	.524	.600	-.561	.527			
			.650	-.485	.548	.700	-.435	.589			
			.700	-.425	.564	.800	-.224	.623			
			.800	-.273	.606	.900	-.016	.677			
			.900	-.020	.676	.950	.061	.698			
			.950	.063	.699	.990	.101	.709			
			.990	.093	.707						
					LOWER SURFACE						
.100	-.349	.585	.025	-.026	.674	.025	.087	.706	.100	-.877	.439
.300	-.701	.484	.050	-.457	.555	.050	-.491	.546	.300	-.821	.455
.600	-.227	.619	.100	-.535	.517	.100	-.614	.512	.600	-.418	.566
.800	.126	.716	.200	-.709	.436	.200	-.750	.474	.300	.110	.717
			.300	-.836	.451	.300	-.921	.427			
			.400	-.951	.447	.400	-1.024	.399			
			.500	-.708	.486	.500	-.632	.507			
			.600	-.216	.622	.600	-.340	.534			
			.700	.034	.691	.700	-.032	.673			
			.800	.209	.739	.800	.215	.741			
			.900	.322	.770	.900	.300	.765			
			.950	.359	.781	.950	.348	.778			
			1.000	.120	.715						
CN=				.3847			.3145				
CM=				-.1062			-.0792				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 0.43^o$; $C_L = 0.366$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.957	.417	0.000	1.125	.992	0.000	.102	.710	.050	-.931	.425
.150	-1.161	.361	.012	-.052	.667	.012	-.132	.645	.150	-1.270	.331
.300	-1.137	.364	.025	-.527	.536	.025	-.412	.564	.300	-1.212	.347
.450	-1.036	.396	.050	-.904	.432	.050	-.894	.435	.450	-.673	.496
.600	-.438	.544	.100	-1.177	.357	.100	-1.079	.334	.600	-.556	.528
.800	-.409	.536	.150	-1.106	.376	.150	-1.086	.382	.800	-.237	.616
.950	.071	.701	.200	-1.167	.359	.200	-1.075	.385			
			.300	-1.191	.353	.300	-1.152	.364			
			.350	-1.166	.360	.350	-1.148	.365			
			.400	-1.175	.357	.400	-1.159	.362			
			.450	-1.180	.356	.450	-1.216	.346			
			.500	-1.233	.341	.500	-1.263	.333			
			.550	-1.129	.370	.550	-.852	.444			
			.600	-.631	.507	.600	-.575	.523			
			.650	-.519	.538	.700	-.335	.589			
			.700	-.403	.569	.800	-.224	.620			
			.800	-.235	.617	.900	-.019	.676			
			.900	-.009	.674	.950	.062	.699			
			.950	.046	.694	.990	.106	.711			
			.990	.077	.703						
					LOWER SURFACE						
.100	-.339	.588	.025	.035	.691	.025	.125	.716	.100	-.807	.459
.300	-.695	.490	.050	-.352	.584	.050	-.450	.657	.300	-.708	.486
.600	-.249	.618	.100	-.541	.532	.100	-.570	.624	.500	-.413	.569
.800	.101	.709	.200	-.707	.486	.200	-.703	.587	.900	.108	.711
			.300	-.748	.475	.300	-.886	.537			
			.400	-.869	.442	.400	-.987	.509			
			.500	-.701	.488	.500	-.671	.496			
			.600	-.214	.627	.600	-.346	.586			
			.700	.062	.699	.700	-.035	.672			
			.800	.185	.733	.800	.218	.742			
			.900	.305	.766	.900	.300	.764			
			.950	.340	.776	.950	.356	.780			
			1.000	.117	.714						
CN=				.4165			.3475				
CM=				-.1032			-.0790				

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 1.11^o$; $C_L = 0.425$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.082	.383	0.000	1.130	.994	0.000	.101	.709	.050	-.981	.411
.150	-1.226	.343	.012	-.111	.651	.012	-.179	.632	.150	-1.313	.319
.300	-1.187	.354	.025	-.533	.518	.025	-.462	.554	.300	-1.315	.319
.450	-1.041	.388	.050	-.928	.410	.050	-.975	.413	.450	-.705	.487
.600	-.479	.543	.100	-1.239	.340	.100	-1.157	.362	.600	-.528	.536
.800	-.298	.599	.150	-1.181	.356	.150	-1.140	.366	.800	-.234	.617
.990	.046	.694	.200	-1.254	.335	.200	-1.150	.364			
			.300	-1.269	.331	.300	-1.211	.347			
			.350	-1.245	.338	.350	-1.237	.340			
			.400	-1.271	.331	.400	-1.224	.344			
			.450	-1.239	.340	.450	-1.274	.329			
			.500	-1.270	.331	.500	-1.300	.323			
			.550	-.808	.459	.550	-.791	.463			
			.600	-.659	.500	.600	-.614	.512			
			.650	-.535	.534	.700	-.371	.579			
			.700	-.425	.564	.800	-.231	.618			
			.800	-.136	.628	.900	-.033	.673			
			.900	-.036	.672	.950	.055	.697			
			.950	.007	.684	.990	.113	.713			
			.990	.034	.693						
					LOWER SURFACE						
.100	-.261	.613	.025	.069	.700	.025	.196	.736	.100	-.704	.487
.300	-.623	.513	.050	-.271	.607	.050	-.351	.585	.300	-.752	.474
.600	-.277	.605	.100	-.449	.558	.100	-.507	.542	.600	-.425	.564
.800	.085	.705	.200	-.627	.505	.200	-.667	.498	.800	.141	.721
			.300	-.693	.490	.300	-.861	.444			
			.400	-.772	.469	.400	-.938	.423			
			.500	-.761	.472	.500	-.707	.487			
			.600	-.236	.617	.600	-.353	.584			
			.700	.039	.705	.700	-.038	.671			
			.800	.225	.744	.900	.233	.746			
			.900	.343	.773	.900	.316	.769			
			.950	.362	.782	.950	.361	.781			
			1.000	-.021	.676						
CN=				.4759			.4094				
CM=				-.1328			-.0807				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 1.69^o$; $C_L = 0.455$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.123	.372	0.000	1.119	.591	0.000	.097	.708	.050	-1.053	.391
.150	-1.304	.322	.012	-.155	.638	.012	-.268	.603	.150	-1.356	.308
.300	-1.255	.335	.025	-.650	.502	.025	-.521	.538	.300	-1.394	.297
.450	-1.028	.394	.050	-1.030	.397	.050	-1.019	.401	.450	-.769	.469
.600	-.447	.558	.100	-1.275	.330	.100	-1.212	.347	.600	-.505	.542
.800	-.281	.604	.150	-1.223	.343	.150	-1.227	.342	.800	-.232	.618
.950	-.011	.679	.200	-1.230	.328	.200	-1.207	.349			
			.300	-1.295	.324	.300	-1.256	.335			
			.350	-1.290	.326	.350	-1.267	.332			
			.400	-1.304	.322	.400	-1.262	.334			
			.450	-.760	.472	.450	-1.326	.316			
			.500	-.913	.430	.500	-1.209	.348			
			.550	-.679	.494	.550	-.724	.482			
			.600	-.531	.521	.600	-.627	.509			
			.650	-.547	.531	.700	-.399	.572			
			.700	-.455	.556	.800	-.242	.615			
			.800	-.354	.584	.900	-.057	.666			
			.900	-.273	.605	.950	.025	.689			
			.950	-.072	.662	.990	.084	.705			
			.990	-.030	.673						
					LOWER SURFACE						
.100	-.231	.618	.025	.118	.714	.025	.246	.753	.100	-.672	.496
.300	-.600	.516	.050	-.236	.617	.050	-.298	.600	.300	-.743	.477
.600	-.266	.608	.100	-.411	.568	.100	-.452	.557	.600	-.426	.564
.800	.143	.721	.200	-.535	.520	.200	-.589	.519	.800	.143	.721
			.300	-.666	.498	.300	-.806	.459			
			.400	-.793	.463	.400	-.924	.454			
			.500	-.757	.462	.500	-.776	.469			
			.600	-.267	.608	.600	-.365	.581			
			.700	.050	.655	.700	-.050	.663			
			.800	.193	.735	.800	.225	.744			
			.900	.343	.777	.900	.309	.767			
			.950	.307	.766	.950	.356	.780			
			1.000	-.085	.658						
CN=				.4900			.4549				
CM=				-.1078			-.0792				

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 2.08^o$; $C_L = 0.486$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.143	.366	0.000	1.110	.588	0.000	.097	.708	.050	-1.083	.383
.150	-1.365	.305	.012	-.207	.625	.012	-.315	.595	.150	-1.393	.297
.300	-1.290	.324	.025	-.727	.487	.025	-.560	.527	.300	-1.430	.287
.450	-.967	.415	.050	-1.064	.388	.050	-1.058	.390	.450	-.774	.468
.600	-.451	.557	.100	-1.310	.320	.100	-1.233	.341	.600	-.497	.545
.800	-.272	.607	.150	-1.273	.330	.150	-1.259	.334	.800	-.235	.617
.950	-.058	.666	.200	-1.322	.317	.200	-1.250	.337			
			.300	-1.347	.310	.300	-1.303	.322			
			.350	-1.315	.319	.350	-1.320	.317			
			.400	-1.312	.320	.400	-1.295	.324			
			.450	-.834	.451	.450	-1.334	.313			
			.500	-.735	.479	.500	-.924	.427			
			.550	-.668	.497	.550	-.722	.492			
			.600	-.633	.506	.600	-.639	.505			
			.650	-.526	.537	.700	-.437	.561			
			.700	-.435	.562	.800	-.260	.610			
			.800	-.307	.597	.900	-.111	.651			
			.900	-.191	.629	.950	-.031	.673			
			.950	-.098	.655	.990	.048	.695			
			.990	-.116	.650						
					LOWER SURFACE						
.100	-.179	.642	.025	.170	.729	.025	.293	.763	.100	-.596	.520
.300	-.565	.526	.050	-.153	.639	.050	-.254	.612	.300	-.692	.491
.600	-.279	.605	.100	-.361	.582	.100	-.413	.568	.600	-.431	.563
.800	.142	.721	.200	-.525	.537	.200	-.541	.532	.800	.153	.724
			.300	-.653	.501	.300	-.777	.467			
			.400	-.718	.483	.400	-.736	.478			
			.500	-.820	.455	.500	-.783	.465			
			.600	-.287	.602	.600	-.371	.579			
			.700	.074	.702	.700	-.059	.665			
			.800	.230	.745	.800	.232	.746			
			.900	.343	.776	.900	.316	.769			
			.950	.348	.778	.950	.354	.780			
			1.000	-.093	.656						
CN=				.5084			.4933				
CM=				-.1016			-.0831				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 2.84^o$; $C_L = 0.521$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.206	.349	0.000	1.099	.585	0.000	.085	.705	.050	-1.136	.368
.150	-1.391	.293	.012	-.274	.606	.012	-.370	.580	.150	-1.444	.283
.300	-1.343	.311	.025	-.773	.468	.025	-.614	.512	.300	-1.472	.275
.450	-.652	.502	.050	-1.114	.374	.050	-1.095	.379	.450	-.739	.478
.600	-.429	.563	.100	-1.361	.306	.100	-1.298	.323	.600	-.466	.553
.800	-.211	.623	.150	-1.332	.314	.150	-1.332	.314	.800	-.240	.615
.950	-.094	.654	.200	-1.385	.299	.200	-1.319	.320			
			.300	-1.212	.347	.300	-1.356	.307			
			.350	-.928	.426	.350	-1.354	.308			
			.400	-.742	.477	.400	-1.319	.319			
			.450	-.683	.493	.450	-.835	.435			
			.500	-.696	.488	.500	-.747	.476			
			.550	-.616	.512	.550	-.677	.495			
			.600	-.539	.519	.600	-.609	.513			
			.650	-.550	.530	.700	-.437	.561			
			.700	-.506	.542	.800	-.279	.605			
			.800	-.394	.573	.900	-.158	.638			
			.900	-.259	.610	.950	-.105	.653			
			.950	-.192	.629	.990	-.039	.671			
			.990	-.223	.620						
					LOWER SURFACE						
.100	-.129	.646	.025	.230	.745	.025	.146	.777	.100	-.542	.532
.300	-.543	.532	.050	-.102	.653	.050	-.187	.630	.300	-.675	.495
.600	-.320	.594	.100	-.233	.601	.100	-.367	.580	.600	-.437	.561
.800	.126	.717	.200	-.471	.552	.200	-.499	.544	.900	.139	.720
			.300	-.601	.516	.300	-.740	.478			
			.400	-.705	.486	.400	-.773	.469			
			.500	-.901	.433	.500	-.796	.462			
			.600	-.279	.605	.600	-.388	.574			
			.700	.033	.691	.700	-.076	.661			
			.800	.219	.742	.800	.214	.741			
			.900	.345	.777	.900	.297	.764			
			.950	.332	.765	.950	.331	.773			
			1.000	-.162	.637						
CN=				.4759			.4934				
CM=				-.0571			-.0745				

(h) M = 0.76. Continued.

$\delta_a = -3^o$; $\alpha = 4.12^o$; $C_L = 0.619$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.373	.302	0.000	1.077	.979	0.000	.073	.702	.050	-1.262	.333
.150	-1.483	.270	.012	-.398	.572	.012	-.488	.547	.150	-1.531	.259
.300	-1.432	.286	.025	-.908	.431	.025	-.729	.480	.300	-1.570	.248
.450	-.757	.473	.050	-1.256	.335	.050	-1.196	.351	.450	-.822	.454
.600	-.487	.547	.100	-1.463	.277	.100	-1.395	.296	.600	-.506	.542
.800	-.272	.606	.150	-1.437	.285	.150	-1.412	.292	.800	-.277	.605
.950	-.104	.653	.200	-1.473	.275	.200	-1.396	.295			
			.300	-1.137	.368	.300	-1.449	.281			
			.350	-1.028	.400	.350	-1.306	.321			
			.400	-.851	.446	.400	-.943	.421			
			.450	-.855	.445	.450	-.816	.456			
			.500	-.739	.477	.500	-.758	.472			
			.550	-.720	.483	.550	-.708	.486			
			.600	-.671	.496	.600	-.651	.502			
			.650	-.617	.511	.700	-.521	.538			
			.700	-.534	.534	.800	-.402	.570			
			.800	-.440	.560	.900	-.272	.606			
			.900	-.342	.587	.950	-.220	.621			
			.950	-.233	.617	.990	-.175	.633			
			.990	-.242	.615						
					LOWER SURFACE						
.100	-.034	.672	.025	.337	.775	.025	.458	.808	.100	-.383	.576
.300	-.467	.553	.050	.024	.688	.050	-.043	.670	.300	-.564	.526
.600	-.426	.571	.100	-.175	.633	.100	-.230	.613	.600	-.457	.555
.800	.136	.719	.200	-.377	.577	.200	-.390	.574	.900	.132	.719
			.300	-.528	.536	.300	-.507	.514			
			.400	-.637	.506	.400	-.671	.496			
			.500	-.830	.459	.500	-.784	.465			
			.600	-.332	.598	.600	-.417	.567			
			.700	.035	.691	.700	-.109	.651			
			.800	.232	.745	.800	.202	.737			
			.900	.328	.772	.900	.299	.761			
			.950	.288	.761	.950	.300	.764			
			1.000	-.155	.639						
CN=				.5847			.5867				
CM=				-.1069			-.0847				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = -4.79^o$; $C_L = -0.246$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.247	.614	0.000	1.113	.989	0.000	.080	.704	.050	-.285	.604
.150	-.483	.549	.012	.458	.809	.012	.448	.806	.150	-.484	.549
.300	-.591	.519	.025	.109	.712	.025	.141	.721	.300	-.579	.523
.450	-.505	.543	.050	-.241	.616	.050	-.215	.623	.450	-.557	.529
.600	-.567	.526	.100	-.367	.581	.100	-.364	.582	.600	-.607	.515
.800	-.364	.582	.150	-.438	.561	.150	-.410	.569	.800	-.301	.599
.950	.058	.698	.200	-.542	.533	.200	-.497	.545			
			.300	-.581	.522	.300	-.575	.524			
			.350	-.560	.528	.350	-.562	.527			
			.400	-.578	.523	.400	-.570	.525			
			.450	-.562	.527	.450	-.610	.514			
			.500	-.728	.481	.500	-.698	.490			
			.550	-.773	.469	.550	-.823	.455			
			.600	-.677	.496	.600	-.812	.458			
			.650	-.699	.490	.700	-.452	.558			
			.700	-.575	.524	.800	-.227	.620			
			.800	-.333	.590	.900	-.034	.673			
			.900	-.047	.669	.950	-.001	.682			
			.950	.052	.697	.990	-.004	.681			
			.990	.075	.703						
					LOWER SURFACE						
.100	-.953	.413	.025	-.463	.555	.025	-.410	.569	.100	-1.369	.305
.300	-1.292	.326	.050	-1.033	.398	.050	-.990	.409	.300	-1.358	.308
.600	-.289	.603	.100	-1.192	.354	.100	-1.238	.341	.600	-.391	.575
.800	-.088	.658	.200	-1.291	.326	.200	-1.293	.326	.800	-.010	.680
			.300	-1.337	.314	.300	-1.369	.305			
			.400	-.999	.407	.400	-.855	.446			
			.500	-.564	.527	.500	-.607	.515			
			.600	-.376	.579	.600	-.425	.565			
			.700	-.222	.621	.700	-.224	.620			
			.800	-.104	.654	.800	-.142	.643			
			.900	.032	.691	.900	.097	.709			
			.950	.150	.723	.950	.141	.721			
			1.000	.105	.711						
CN=				-.2197			-.2157				
CM=				-.0720			-.0585				

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = -3.29^o$; $C_L = -0.106$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.527	.537	0.000	1.131	.954	0.000	.097	.709	.050	-.535	.535
.150	-.703	.498	.012	.328	.773	.012	.278	.759	.150	-.610	.514
.300	-.705	.488	.025	-.093	.656	.025	-.041	.671	.300	-.793	.464
.450	-.573	.524	.050	-.451	.558	.050	-.435	.562	.450	-.583	.522
.600	-.565	.526	.100	-.566	.526	.100	-.529	.536	.600	-.608	.515
.800	-.315	.595	.150	-.569	.525	.150	-.542	.533	.800	-.297	.600
.950	.061	.699	.200	-.726	.482	.200	-.626	.510			
			.300	-.757	.473	.300	-.785	.466			
			.350	-.661	.500	.350	-.755	.474			
			.400	-.691	.492	.400	-.580	.522			
			.450	-.608	.515	.450	-.648	.503			
			.500	-.758	.473	.500	-.726	.482			
			.550	-.811	.459	.550	-.835	.452			
			.600	-.678	.495	.600	-.667	.498			
			.650	-.610	.514	.700	-.413	.568			
			.700	-.535	.535	.800	-.173	.634			
			.800	-.236	.612	.900	-.025	.675			
			.900	.005	.684	.950	-.017	.677			
			.950	.055	.697	.990	.009	.685			
			.990	.089	.707						
					LOWER SURFACE						
.100	-.781	.467	.025	-.349	.586	.025	-.272	.607	.100	-1.244	.339
.300	-1.147	.366	.050	-.888	.437	.050	-.805	.460	.300	-1.304	.323
.600	-.257	.611	.100	-1.054	.392	.100	-1.120	.373	.600	-.361	.583
.800	-.043	.670	.200	-1.130	.371	.200	-1.131	.371	.800	.172	.730
			.300	-1.212	.348	.300	-1.263	.334			
			.400	-1.154	.364	.400	-.869	.443			
			.500	-.516	.540	.500	-.570	.525			
			.600	-.246	.614	.600	-.388	.575			
			.700	-.187	.631	.700	-.185	.631			
			.800	-.018	.677	.800	.044	.694			
			.900	.136	.720	.900	.096	.709			
			.950	.191	.735	.950	.198	.737			
			1.000	.091	.707						
CN=				-.0910			-.0769				
CM=				-.0724			-.0652				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = -1.38^o$; $C_L = 0.139$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.773	.469	0.000	1.137	.596	0.000	.107	.712	.050	-.746	.476
.150	-.917	.429	.012	.135	.719	.012	.063	.700	.150	-1.020	.401
.300	-.871	.442	.025	-.343	.588	.025	-.221	.621	.300	-.765	.471
.450	-.747	.476	.050	-.722	.483	.050	-.772	.483	.450	-.641	.505
.600	-.572	.524	.100	-.991	.409	.100	-.852	.447	.600	-.629	.509
.800	-.315	.595	.150	-.868	.443	.150	-.852	.447	.800	-.284	.604
.950	.053	.697	.200	-.955	.419	.200	-.843	.450			
			.300	-.944	.422	.300	-.912	.431			
			.350	-.972	.414	.350	-.917	.429			
			.400	-.907	.432	.400	-.939	.423			
			.450	-.830	.453	.450	-.907	.432			
			.500	-.814	.458	.500	-.881	.439			
			.550	-.726	.432	.550	-.714	.485			
			.600	-.609	.514	.600	-.607	.515			
			.650	-.584	.521	.700	-.396	.573			
			.700	-.536	.534	.800	-.213	.623			
			.800	-.264	.609	.900	-.051	.668			
			.900	-.006	.680	.950	-.040	.671			
			.950	.054	.697	.990	-.032	.673			
			.990	.062	.699						
					LOWER SURFACE						
.100	-.534	.535	.025	-.174	.634	.025	-.045	.670	.100	-1.074	.386
.300	-.927	.426	.050	-.647	.504	.050	-.643	.505	.300	-1.056	.391
.600	-.258	.611	.100	-.852	.447	.100	-.916	.430	.600	-.363	.582
.800	.036	.692	.200	-.846	.449	.200	-.851	.447	.800	.191	.735
			.300	-.953	.419	.300	-1.005	.405			
			.400	-1.035	.397	.400	-1.146	.366			
			.500	-.618	.512	.500	-.550	.530			
			.600	-.212	.624	.600	-.248	.614			
			.700	.048	.695	.700	.007	.684			
			.800	.178	.731	.800	.221	.743			
			.900	.285	.761	.900	.290	.762			
			.950	.310	.768	.950	.312	.768			
			1.000	.086	.706						
CN=				.1781			.1692				
CM=				-.0983			-.0925				

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 0.54^o$; $C_L = 0.393$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.964	.417	0.000	1.130	.594	0.000	.101	.710	.050	-.944	.422
.150	-1.209	.349	.012	-.094	.656	.012	-.183	.632	.150	-1.263	.334
.300	-1.132	.370	.025	-.560	.528	.025	-.429	.564	.300	-1.261	.335
.450	-1.065	.389	.050	-.926	.427	.050	-.895	.436	.450	-.710	.487
.600	-.505	.543	.100	-1.181	.357	.100	-1.088	.383	.600	-.579	.523
.800	-.309	.597	.150	-1.147	.366	.150	-1.111	.376	.800	-.248	.614
.950	.084	.706	.200	-1.166	.361	.200	-1.086	.383			
			.300	-1.201	.351	.300	-1.170	.360			
			.350	-1.231	.351	.350	-1.176	.358			
			.400	-1.227	.344	.400	-1.168	.361			
			.450	-1.205	.350	.450	-1.238	.341			
			.500	-1.267	.333	.500	-1.255	.337			
			.550	-1.113	.376	.550	-.966	.416			
			.600	-.645	.505	.600	-.612	.514			
			.650	-.506	.543	.700	-.376	.579			
			.700	-.410	.569	.800	-.228	.619			
			.800	-.251	.613	.900	-.049	.669			
			.900	-.025	.675	.950	-.026	.675			
			.950	.003	.683	.990	.032	.691			
			.990	.018	.687						
					LOWER SURFACE						
.100	-.313	.596	.025	.049	.696	.025	.180	.732	.100	-.770	.470
.300	-.643	.505	.050	-.376	.579	.050	-.403	.571	.300	-.745	.477
.600	-.225	.620	.100	-.510	.542	.100	-.552	.530	.600	-.370	.580
.800	.107	.712	.200	-.674	.497	.200	-.692	.492	.800	.200	.738
			.300	-.751	.475	.300	-.865	.444			
			.400	-.780	.467	.400	-.745	.477			
			.500	-.700	.439	.500	-.660	.500			
			.600	-.235	.618	.600	-.283	.604			
			.700	.082	.705	.700	.021	.688			
			.800	.242	.749	.800	.263	.755			
			.900	.339	.776	.900	.323	.771			
			.950	.354	.780	.950	.362	.782			
			1.000	.083	.705						
CN=				.4603			.4293				
CM=				-.1138			-.1011				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 1.18^o$; $C_L = 0.439$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.066	.388	0.000	1.123	.992	0.000	.111	.713	.050	-1.046	.394
.150	-1.229	.343	.012	-.171	.635	.012	-.229	.619	.150	-1.314	.320
.300	-1.211	.348	.025	-.624	.510	.025	-.484	.549	.300	-1.350	.310
.450	-1.105	.377	.050	-1.002	.406	.050	-.989	.409	.450	-.719	.484
.600	-.495	.546	.100	-1.237	.341	.100	-1.168	.360	.600	-.577	.523
.800	-.277	.606	.150	-1.204	.350	.150	-1.187	.355	.800	-.255	.612
.990	.065	.700	.200	-1.261	.334	.200	-1.183	.356			
			.300	-1.274	.331	.300	-1.222	.345			
			.350	-1.254	.336	.350	-1.245	.339			
			.400	-1.260	.335	.400	-1.246	.339			
			.450	-1.254	.336	.450	-1.275	.330			
			.500	-1.136	.369	.500	-1.301	.323			
			.550	-.763	.472	.550	-.773	.469			
			.600	-.602	.516	.600	-.638	.506			
			.650	-.514	.540	.700	-.420	.566			
			.700	-.440	.561	.800	-.268	.608			
			.800	-.223	.621	.900	-.108	.652			
			.900	-.149	.641	.950	-.042	.671			
			.950	-.034	.673	.990	.003	.683			
			.990	-.011	.679						
					LOWER SURFACE						
.100	-.239	.616	.025	.092	.707	.025	.208	.740	.100	-.683	.494
.300	-.611	.514	.050	-.281	.605	.050	-.353	.585	.300	-.752	.475
.600	-.276	.606	.100	-.451	.558	.100	-.504	.543	.600	-.376	.578
.800	.146	.723	.200	-.604	.515	.200	-.634	.507	.800	.225	.744
			.300	-.704	.488	.300	-.822	.455			
			.400	-.772	.469	.400	-.782	.466			
			.500	-.735	.479	.500	-.689	.492			
			.600	-.256	.611	.600	-.307	.598			
			.700	.076	.703	.700	.025	.689			
			.800	.217	.747	.800	.273	.757			
			.900	.335	.774	.900	.349	.778			
			.950	.334	.774	.950	.364	.783			
			1.000	.046	.695						
CN=				.4758			.4812				
CM=				-.1038			-.1043				

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 1.80^o$; $C_L = 0.478$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.115	.375	0.000	1.123	.992	0.000	.098	.709	.050	-1.119	.374
.150	-1.294	.326	.012	-.190	.630	.012	-.301	.599	.150	-1.384	.301
.300	-1.261	.335	.025	-.675	.496	.025	-.530	.536	.300	-1.400	.296
.450	-1.132	.370	.050	-1.031	.398	.050	-1.019	.401	.450	-.768	.471
.600	-.470	.553	.100	-1.275	.331	.100	-1.239	.341	.600	-.543	.533
.800	-.280	.605	.150	-1.259	.336	.150	-1.236	.342	.800	-.275	.607
.990	-.036	.672	.200	-1.313	.320	.200	-1.219	.346			
			.300	-1.322	.318	.300	-1.269	.333			
			.350	-1.316	.320	.350	-1.291	.327			
			.400	-1.319	.319	.400	-1.291	.327			
			.450	-1.063	.389	.450	-1.342	.313			
			.500	-.782	.467	.500	-1.119	.374			
			.550	-.686	.493	.550	-.730	.481			
			.600	-.633	.508	.600	-.630	.509			
			.650	-.556	.529	.700	-.442	.561			
			.700	-.413	.568	.800	-.280	.605			
			.800	-.231	.619	.900	-.097	.656			
			.900	-.146	.642	.950	-.035	.673			
			.950	-.082	.660	.990	-.001	.682			
			.990	-.099	.655						
					LOWER SURFACE						
.100	-.186	.631	.025	.142	.722	.025	.269	.756	.100	-.622	.511
.300	-.571	.525	.050	-.184	.632	.050	-.766	.609	.300	-.706	.488
.600	-.273	.607	.100	-.389	.575	.100	-.422	.566	.600	-.384	.576
.800	.109	.712	.200	-.555	.529	.200	-.566	.526	.800	.238	.748
			.300	-.673	.497	.300	-.801	.462			
			.400	-.743	.478	.400	-.737	.479			
			.500	-.800	.462	.500	-.717	.485			
			.600	-.256	.612	.600	-.298	.600			
			.700	.070	.702	.700	.019	.688			
			.800	.217	.742	.800	.286	.761			
			.900	.354	.780	.900	.347	.778			
			.950	.318	.770	.950	.373	.785			
			1.000	-.027	.675						
CN=				.4854			.5208				
CM=				-.0966			-.1014				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 2.92^o$; $C_L = 0.537$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.233	.344	0.000	1.058	.585	0.000	.093	.708	.050	-1.214	.348
.150	-1.405	.295	.012	-.325	.593	.012	-.392	.574	.150	-1.443	.285
.300	-1.340	.313	.025	-.777	.468	.025	-.610	.514	.300	-1.488	.272
.450	-.788	.465	.050	-1.122	.373	.050	-1.102	.379	.450	-.800	.462
.600	-.461	.555	.100	-1.365	.306	.100	-1.305	.323	.600	-.503	.544
.800	-.254	.617	.150	-1.334	.313	.150	-1.311	.321	.800	-.283	.604
.950	-.013	.679	.200	-1.330	.307	.200	-1.305	.323			
			.300	-1.371	.304	.300	-1.376	.303			
			.350	-.834	.453	.350	-1.359	.308			
			.400	-1.074	.386	.400	-1.349	.311			
			.450	-.800	.462	.450	-1.040	.396			
			.500	-.732	.431	.500	-.762	.472			
			.550	-.711	.488	.550	-.713	.486			
			.600	-.692	.492	.600	-.652	.503			
			.650	-.620	.517	.700	-.482	.550			
			.700	-.478	.551	.800	-.290	.602			
			.800	-.375	.579	.900	-.225	.620			
			.900	-.229	.619	.950	-.184	.632			
			.950	-.216	.623	.990	-.166	.637			
			.990	-.165	.637						
					LOWER SURFACE						
.100	-.135	.645	.025	.236	.747	.025	.374	.786	.100	-.506	.543
.300	-.522	.539	.050	-.103	.654	.050	-.180	.633	.300	-.628	.509
.600	-.277	.606	.100	-.273	.607	.100	-.307	.598	.600	-.397	.573
.800	.161	.727	.200	-.451	.558	.200	-.490	.547	.800	.236	.747
			.300	-.598	.517	.300	-.704	.484			
			.400	-.652	.503	.400	-.760	.473			
			.500	-.816	.457	.500	-.691	.492			
			.600	-.285	.604	.600	-.327	.592			
			.700	.039	.693	.700	-.005	.681			
			.800	.219	.743	.800	.276	.759			
			.900	.333	.774	.900	.323	.771			
			.950	.298	.764	.950	.336	.775			
			1.000	-.114	.651						
CN=					.5382			.5718			
CM=					-.1039			-.1017			

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 4.11^o$; $C_L = 0.603$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.353	.309	0.000	1.088	.982	0.000	.070	.701	.050	-1.312	.320
.150	-1.498	.269	.012	-.443	.560	.012	-.524	.538	.150	-1.551	.255
.300	-1.166	.361	.025	-.908	.432	.025	-.721	.483	.300	-1.567	.250
.450	-.758	.473	.050	-1.227	.344	.050	-1.187	.355	.450	-.854	.447
.600	-.520	.539	.100	-1.433	.287	.100	-1.392	.299	.600	-.531	.544
.800	-.248	.614	.150	-1.423	.290	.150	-1.422	.290	.800	-.321	.594
.990	-.143	.643	.200	-1.434	.287	.200	-1.405	.295			
			.300	-1.082	.334	.300	-1.447	.283			
			.350	-1.232	.343	.350	-1.334	.315			
			.400	-.838	.451	.400	-.972	.414			
			.450	-.849	.448	.450	-.831	.453			
			.500	-.776	.468	.500	-.756	.474			
			.550	-.742	.478	.550	-.688	.493			
			.600	-.648	.503	.600	-.666	.499			
			.650	-.500	.544	.700	-.477	.551			
			.700	-.480	.550	.800	-.374	.579			
			.800	-.348	.586	.900	-.273	.607			
			.900	-.372	.580	.950	-.247	.614			
			.950	-.232	.618	.990	-.221	.621			
			.990	-.193	.629						
					LOWER SURFACE						
.100	-.080	.660	.025	.348	.778	.025	.449	.806	.100	-.403	.571
.300	-.468	.553	.050	.047	.695	.050	-.074	.662	.300	-.583	.522
.600	-.356	.584	.100	-.186	.631	.100	-.207	.625	.600	-.400	.572
.800	.147	.720	.200	-.368	.581	.200	-.378	.578	.800	.218	.742
			.300	-.525	.538	.300	-.562	.527			
			.400	-.637	.507	.400	-.651	.503			
			.500	-.816	.457	.500	-.731	.481			
			.600	-.288	.603	.600	-.340	.588			
			.700	.027	.690	.700	-.022	.676			
			.800	.236	.747	.800	.277	.759			
			.900	.330	.773	.900	.310	.768			
			.950	.294	.763	.950	.340	.776			
			1.000	-.154	.640						
CN=					.5754			.6312			
CM=					-.1019			-.1008			

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 0^o$; $\alpha = 5.13^o$; $C_L = 0.664$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.489	.272	0.000	1.025	.965	0.000	.066	.700	.050	-1.384	.301
.150	-1.449	.283	.012	-.539	.534	.012	-.671	.497	.150	-1.607	.239
.300	-1.062	.389	.025	-.969	.415	.025	-.820	.456	.300	-1.613	.237
.450	-.779	.467	.050	-1.326	.317	.050	-1.272	.331	.450	-.887	.438
.600	-.582	.522	.100	-1.532	.260	.100	-1.487	.272	.600	-.592	.519
.800	-.398	.572	.150	-1.483	.273	.150	-1.506	.267	.800	-.332	.591
.950	-.272	.607	.200	-1.545	.256	.200	-1.494	.270			
			.300	-1.100	.379	.300	-1.372	.304			
			.350	-.903	.433	.350	-1.054	.392			
			.400	-.952	.420	.400	-.916	.429			
			.450	-.866	.443	.450	-.859	.445			
			.500	-.824	.455	.500	-.816	.457			
			.550	-.690	.492	.550	-.720	.484			
			.600	-.532	.536	.600	-.634	.507			
			.650	-.527	.537	.700	-.495	.546			
			.700	-.447	.559	.800	-.400	.572			
			.800	-.314	.596	.900	-.295	.601			
			.900	-.269	.608	.950	-.289	.603			
			.950	-.271	.607	.990	-.255	.612			
			.990	-.189	.630						
					LOWER SURFACE						
.100	.052	.697	.025	.434	.802	.025	.567	.838	.100	-.308	.597
.300	-.419	.567	.050	.119	.715	.050	.034	.692	.300	-.522	.538
.600	-.361	.583	.100	-.108	.652	.100	-.132	.646	.600	-.408	.570
.800	.157	.725	.200	-.309	.597	.200	-.354	.585	.800	.204	.738
			.300	-.474	.552	.300	-.505	.543			
			.400	-.571	.525	.400	-.643	.505			
			.500	-.786	.465	.500	-.740	.478			
			.600	-.322	.593	.600	-.356	.584			
			.700	.047	.695	.700	-.052	.668			
			.800	.254	.752	.800	.255	.752			
			.900	.321	.771	.900	.305	.766			
			.950	.288	.762	.950	.329	.773			
			1.000	-.198	.628						
CN=				.6131			.6581				
CM=				-.0922			-.0946				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = -4.73^o$; $C_L = -0.257$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.332	.601	0.000	1.116	.990	0.000	.088	.706	.050	-.265	.668
.150	-.483	.546	.012	.469	.811	.012	.424	.799	.150	-.483	.648
.300	-.568	.524	.025	.068	.708	.025	.154	.724	.300	-.596	.617
.450	-.476	.550	.050	-.240	.615	.050	-.248	.613	.450	-.568	.625
.600	-.564	.526	.100	-.410	.568	.100	-.384	.575	.600	-.624	.609
.800	-.355	.583	.150	-.461	.557	.150	-.402	.570	.800	-.301	.658
.990	.063	.699	.200	-.521	.538	.200	-.508	.561			
			.300	-.578	.522	.300	-.620	.510			
			.350	-.574	.523	.350	-.579	.521			
			.400	-.571	.524	.400	-.564	.526			
			.450	-.560	.527	.450	-.624	.509			
			.500	-.737	.478	.500	-.702	.487			
			.550	-.780	.466	.550	-.811	.458			
			.600	-.617	.511	.600	-.756	.473			
			.650	-.638	.505	.700	-.418	.566			
			.700	-.572	.523	.800	-.139	.643			
			.800	-.310	.596	.900	-.084	.658			
			.900	-.046	.669	.950	-.082	.659			
			.950	.032	.690	.990	-.075	.661			
			.990	.073	.702						
					LOWER SURFACE						
.100	-.945	.420	.025	-.449	.557	.025	-.371	.579	.100	-1.350	.308
.300	-1.230	.325	.050	-1.032	.396	.050	-.968	.414	.300	-1.474	.274
.600	-.297	.599	.100	-1.180	.356	.100	-1.226	.343	.600	-.335	.589
.800	-.033	.656	.200	-1.245	.337	.200	-1.293	.324	.800	.122	.715
			.300	-1.342	.311	.300	-1.325	.315			
			.400	-.865	.442	.400	-.814	.457			
			.500	-.579	.522	.500	-.738	.478			
			.600	-.376	.578	.600	-.497	.544			
			.700	-.195	.628	.700	-.254	.611			
			.800	-.023	.675	.800	-.066	.663			
			.900	-.020	.676	.900	.053	.696			
			.950	.107	.711	.950	.120	.715			
			1.000	.083	.704						
CN=				-.2023			-.2190				
CM=				-.0714			-.0541				

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = -3.24^o$; $C_L = -0.099$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.524	.536	0.000	1.131	.994	0.000	.091	.707	.050	-.472	.651
.150	-.723	.482	.012	.359	.781	.012	.265	.755	.150	-.635	.606
.300	-.705	.487	.025	-.071	.662	.025	-.030	.673	.300	-.776	.566
.450	-.553	.533	.050	-.462	.554	.050	-.471	.552	.450	-.591	.618
.600	-.558	.525	.100	-.612	.513	.100	-.545	.531	.600	-.638	.605
.800	-.320	.593	.150	-.621	.510	.150	-.563	.526	.800	-.311	.596
.990	.067	.667	.200	-.742	.477	.200	-.645	.503			
			.300	-.771	.468	.300	-.791	.463			
			.350	-.766	.470	.350	-.795	.462			
			.400	-.690	.491	.400	-.617	.511			
			.450	-.591	.521	.450	-.637	.505			
			.500	-.755	.473	.500	-.722	.482			
			.550	-.831	.452	.550	-.837	.450			
			.600	-.699	.488	.600	-.783	.465			
			.650	-.598	.516	.700	-.400	.571			
			.700	-.521	.538	.800	-.162	.637			
			.800	-.249	.613	.900	-.101	.654			
			.900	-.010	.679	.950	-.100	.654			
			.950	.051	.695	.990	-.099	.654			
			.990	.065	.700						
					LOWER SURFACE						
.100	-.796	.462	.025	-.344	.587	.025	-.240	.615	.100	-1.221	.344
.300	-1.114	.374	.050	-.880	.439	.050	-.796	.462	.300	-1.322	.316
.600	-.263	.609	.100	-1.051	.391	.100	-1.101	.377	.600	-.316	.594
.800	-.004	.680	.200	-1.123	.371	.200	-1.145	.365	.800	.225	.744
			.300	-1.230	.342	.300	-1.236	.339			
			.400	-1.324	.316	.400	-1.287	.326			
			.500	-.539	.533	.500	-.625	.509			
			.600	-.254	.611	.600	-.314	.595			
			.700	-.049	.668	.700	-.087	.657			
			.800	.110	.712	.800	.089	.706			
			.900	.253	.751	.900	.203	.738			
			.950	.295	.744	.950	.249	.750			
			1.000	.077	.703						
CN=				-.0615			-.0640				
CM=				-.0502			-.0819				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = -1.33^o$; $C_L = 0.154$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.733	.480	0.000	1.134	.695	0.000	.100	.709	.050	-.706	.487
.150	-.955	.416	.012	.118	.714	.012	.030	.690	.150	-1.059	.390
.300	-.876	.440	.025	-.354	.684	.025	-.233	.618	.300	-.658	.500
.450	-.737	.479	.050	-.715	.485	.050	-.747	.476	.450	-.660	.500
.600	-.539	.525	.100	-1.032	.397	.100	-.895	.435	.600	-.656	.501
.800	-.321	.593	.150	-.920	.428	.150	-.866	.443	.800	-.305	.658
.990	.050	.698	.200	-.842	.422	.200	-.873	.441			
			.300	-.939	.423	.300	-.956	.418			
			.350	-.931	.425	.350	-.984	.410			
			.400	-.956	.418	.400	-.943	.422			
			.450	-.911	.431	.450	-.901	.433			
			.500	-.943	.422	.500	-.867	.443			
			.550	-.995	.407	.550	-.795	.461			
			.600	-.610	.514	.600	-.632	.508			
			.650	-.562	.527	.700	-.398	.572			
			.700	-.478	.550	.800	-.184	.631			
			.800	-.241	.616	.900	-.121	.649			
			.900	-.014	.678	.950	-.119	.649			
			.950	.042	.693	.990	-.122	.648			
			.990	.043	.694						
					LOWER SURFACE						
.100	-.516	.540	.025	-.156	.639	.025	-.064	.664	.100	-1.041	.395
.300	-.909	.431	.050	-.610	.514	.050	-.630	.508	.300	-.956	.418
.600	-.216	.622	.100	-.807	.459	.100	-.862	.436	.600	-.301	.599
.800	.029	.690	.200	-.867	.443	.200	-.865	.443	.800	.209	.740
			.300	-.917	.429	.300	-1.034	.397			
			.400	-1.026	.395	.400	-1.157	.363			
			.500	-.594	.518	.500	-.522	.538			
			.600	-.231	.618	.600	-.206	.625			
			.700	.045	.694	.700	.065	.700			
			.800	.184	.733	.800	.265	.755			
			.900	.309	.767	.900	.319	.770			
			.950	.372	.771	.950	.316	.769			
			1.000	.056	.697						
CN=				.2191			.2128				
CM=				-.1051			-.1084				

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 0.21^o$; $C_L = 0.375$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.695	.410	0.000	1.124	.693	0.000	.099	.710	.050	-.908	.434
.150	-1.155	.365	.012	-.045	.671	.012	-.130	.647	.150	-1.234	.344
.300	-1.107	.379	.025	-.534	.536	.025	-.398	.574	.300	-1.206	.352
.450	-1.027	.401	.050	-.902	.435	.050	-.905	.433	.450	-.675	.498
.600	-.510	.543	.100	-1.155	.365	.100	-1.102	.380	.600	-.621	.512
.800	-.306	.598	.150	-1.124	.374	.150	-1.103	.380	.800	-.305	.598
.990	.077	.704	.200	-1.159	.365	.200	-1.099	.381			
			.300	-1.165	.363	.300	-1.157	.365			
			.350	-1.211	.350	.350	-1.175	.359			
			.400	-1.197	.354	.400	-1.161	.364			
			.450	-1.166	.362	.450	-1.204	.352			
			.500	-1.251	.339	.500	-1.227	.346			
			.550	-1.110	.378	.550	-1.003	.407			
			.600	-.619	.513	.600	-.616	.514			
			.650	-.497	.549	.700	-.396	.577			
			.700	-.382	.578	.800	-.210	.626			
			.800	-.211	.625	.900	-.108	.653			
			.900	-.096	.657	.950	-.100	.656			
			.950	-.020	.678	.990	-.096	.657			
			.990	.003	.684						
					LOWER SURFACE						
.100	-.332	.592	.025	.006	.685	.025	.136	.721	.100	-.763	.473
.300	-.679	.497	.050	-.388	.577	.050	-.444	.561	.300	-.699	.491
.600	-.220	.623	.100	-.564	.528	.100	-.576	.525	.600	-.307	.599
.800	.133	.717	.200	-.697	.491	.200	-.689	.494	.800	.206	.740
			.300	-.732	.482	.300	-.880	.441			
			.400	-.734	.481	.400	-.877	.442			
			.500	-.658	.502	.500	-.592	.520			
			.600	-.233	.619	.600	-.250	.615			
			.700	.081	.705	.700	.072	.703			
			.800	.223	.744	.800	.299	.765			
			.900	.342	.777	.900	.358	.782			
			.950	.315	.770	.950	.367	.784			
			1.000	.034	.692						
CN=				.4442			.4394				
CM=				-.1148			-.1157				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 0.51^o$; $C_L = 0.394$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.034	.405	0.000	1.130	.594	0.000	.102	.710	.050	-.945	.422
.150	-1.156	.360	.012	-.069	.663	.012	-.154	.640	.150	-1.260	.336
.300	-1.133	.368	.025	-.551	.530	.025	-.425	.565	.300	-1.209	.340
.450	-1.054	.391	.050	-.950	.420	.050	-.919	.429	.450	-.703	.488
.600	-.531	.544	.100	-1.213	.348	.100	-1.110	.376	.600	-.614	.513
.800	-.322	.593	.150	-1.149	.365	.150	-1.124	.372	.900	-.311	.566
.990	.076	.703	.200	-1.137	.352	.200	-1.111	.376			
			.300	-1.272	.345	.300	-1.140	.365			
			.350	-1.200	.351	.350	-1.188	.354			
			.400	-1.222	.345	.400	-1.174	.358			
			.450	-1.192	.353	.450	-1.214	.347			
			.500	-1.242	.339	.500	-1.237	.341			
			.550	-.870	.442	.550	-.927	.426			
			.600	-.692	.502	.600	-.611	.513			
			.650	-.493	.557	.700	-.393	.574			
			.700	-.386	.575	.800	-.230	.618			
			.800	-.235	.617	.900	-.130	.646			
			.900	-.095	.659	.950	-.115	.650			
			.550	-.102	.654	.990	-.111	.651			
			.990	-.037	.672						
					LOWER SURFACE						
.100	-.343	.587	.025	.044	.654	.025	.145	.722	.100	-.778	.468
.300	-.669	.501	.050	-.350	.586	.050	-.418	.567	.300	-.712	.486
.600	-.738	.611	.100	-.551	.530	.100	-.557	.528	.600	-.304	.598
.800	.114	.714	.200	-.645	.499	.200	-.689	.492	.800	.222	.743
			.300	-.712	.486	.300	-.872	.441			
			.400	-.758	.462	.400	-.969	.415			
			.500	-.699	.489	.500	-.586	.520			
			.600	-.238	.616	.600	-.248	.614			
			.700	.090	.704	.700	.071	.702			
			.800	.230	.746	.800	.300	.745			
			.900	.338	.775	.900	.360	.781			
			.550	.323	.771	.950	.366	.783			
			1.000	.011	.685						
CN=				.4422			.4411				
CM=				-.1100			-.1161				

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 1.15^o$; $C_L = 0.446$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.045	.393	0.000	1.127	.993	0.000	.097	.709	.050	-1.015	.402
.150	-1.244	.337	.012	-.176	.644	.012	-.225	.620	.150	-1.328	.315
.300	-1.131	.353	.025	-.635	.507	.025	-.473	.551	.300	-1.343	.311
.450	-1.131	.379	.050	-1.000	.406	.050	-.975	.413	.450	-.770	.469
.600	-.482	.543	.100	-1.256	.335	.100	-1.161	.361	.600	-.592	.518
.800	-.331	.595	.150	-1.219	.345	.150	-1.189	.354	.900	-.306	.567
.990	.067	.709	.200	-1.249	.337	.200	-1.169	.359			
			.300	-1.271	.331	.300	-1.217	.346			
			.350	-1.272	.331	.350	-1.248	.337			
			.400	-1.262	.333	.400	-1.223	.344			
			.450	-1.246	.338	.450	-1.280	.328			
			.500	-.783	.466	.500	-1.305	.322			
			.550	-.657	.500	.550	-.776	.468			
			.600	-.591	.521	.600	-.651	.502			
			.650	-.499	.547	.700	-.436	.561			
			.700	-.415	.567	.800	-.282	.604			
			.800	-.240	.615	.900	-.172	.634			
			.900	-.174	.633	.550	-.135	.645			
			.550	-.147	.636	.990	-.119	.649			
			.990	-.090	.657						
					LOWER SURFACE						
.100	-.373	.505	.025	.099	.709	.025	.204	.738	.100	-.657	.489
.300	-.693	.510	.050	-.253	.612	.050	-.351	.585	.300	-.708	.486
.600	-.740	.510	.100	-.441	.560	.100	-.489	.547	.600	-.310	.596
.800	.118	.714	.200	-.607	.514	.200	-.608	.514	.800	.236	.747
			.300	-.690	.491	.300	-.802	.460			
			.400	-.756	.470	.400	-.702	.488			
			.500	-.758	.473	.500	-.630	.508			
			.600	-.264	.609	.600	-.256	.611			
			.700	.050	.696	.700	.075	.702			
			.800	.217	.742	.800	.322	.771			
			.900	.337	.775	.900	.368	.783			
			.550	.310	.767	.950	.374	.785			
			1.000	-.031	.673						
CN=				.4467			.5327				
CM=				-.0582			-.1263				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 1.76^o$; $C_L = 0.479$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.135	.369	0.000	1.129	.993	0.000	.092	.709	.050	-1.075	.396
.150	-1.331	.315	.012	-.175	.634	.012	-.296	.600	.150	-1.388	.299
.300	-1.249	.332	.025	-.673	.496	.025	-.538	.534	.300	-1.406	.294
.450	-1.083	.404	.050	-1.054	.392	.050	-1.021	.400	.450	-.767	.471
.600	-.450	.555	.100	-1.323	.317	.100	-1.210	.348	.600	-.566	.526
.800	-.223	.593	.150	-1.275	.331	.150	-1.224	.345	.800	-.319	.554
.990	-.039	.680	.200	-1.286	.327	.200	-1.214	.347			
			.300	-1.305	.322	.300	-1.267	.333			
			.350	-1.304	.323	.350	-1.287	.327			
			.400	-1.277	.330	.400	-1.284	.328			
			.450	-.724	.482	.450	-1.328	.316			
			.500	-.669	.498	.500	-1.036	.396			
			.550	-.632	.508	.550	-.732	.480			
			.600	-.570	.525	.600	-.652	.502			
			.650	-.513	.541	.700	-.455	.557			
			.700	-.369	.572	.800	-.303	.599			
			.800	-.283	.604	.900	-.183	.632			
			.900	-.240	.616	.950	-.153	.640			
			.950	-.193	.629	.990	-.124	.648			
			.990	-.095	.656						
					LOWER SURFACE						
.100	-.216	.623	.025	.131	.718	.025	.265	.755	.100	-.634	.607
.300	-.577	.523	.050	-.173	.635	.050	-.310	.597	.300	-.664	.599
.600	-.338	.597	.100	-.357	.584	.100	-.445	.558	.600	-.318	.564
.800	.125	.717	.200	-.532	.535	.200	-.591	.519	.800	.239	.748
			.300	-.652	.502	.300	-.765	.463			
			.400	-.735	.480	.400	-.762	.472			
			.500	-.803	.461	.500	-.661	.500			
			.600	-.279	.605	.600	-.263	.609			
			.700	.052	.696	.700	.076	.703			
			.800	.223	.744	.800	.330	.773			
			.900	.325	.772	.900	.372	.785			
			.950	.289	.762	.950	.381	.787			
			1.000	-.103	.654						
CN=				.4844			.5474				
CM=				-.0964			-.1231				

(h) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 3.00^o$; $C_L = 0.564$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.274	.331	0.000	1.091	.583	0.000	.083	.705	.050	-1.171	.356
.150	-1.334	.301	.012	-.320	.594	.012	-.402	.571	.150	-1.449	.282
.300	-1.358	.309	.025	-.790	.464	.025	-.622	.511	.300	-1.489	.269
.450	-.768	.470	.050	-1.159	.363	.050	-1.131	.370	.450	-.756	.473
.600	-.448	.553	.100	-1.388	.299	.100	-1.219	.318	.600	-.530	.536
.800	-.271	.607	.150	-1.367	.305	.150	-1.237	.313	.800	-.362	.582
.990	-.041	.660	.200	-1.403	.295	.200	-1.328	.316			
			.300	-1.130	.371	.300	-1.372	.304			
			.350	-.976	.413	.350	-1.333	.315			
			.400	-.914	.430	.400	-1.188	.354			
			.450	-.774	.469	.450	-.791	.464			
			.500	-.754	.474	.500	-.749	.476			
			.550	-.664	.499	.550	-.713	.486			
			.600	-.653	.502	.600	-.671	.497			
			.650	-.547	.531	.700	-.503	.544			
			.700	-.477	.551	.800	-.373	.579			
			.800	-.359	.583	.900	-.314	.596			
			.900	-.385	.576	.950	-.267	.608			
			.950	-.334	.590	.990	-.227	.620			
			.990	-.324	.593						
					LOWER SURFACE						
.100	-.104	.653	.025	.237	.747	.025	.359	.781	.100	-.469	.653
.300	-.495	.545	.050	-.052	.665	.050	-.151	.641	.300	-.586	.621
.600	-.314	.595	.100	-.263	.610	.100	-.314	.595	.600	-.324	.593
.800	.146	.722	.200	-.439	.561	.200	-.478	.550	.800	.243	.749
			.300	-.584	.521	.300	-.687	.493			
			.400	-.659	.500	.400	-.712	.486			
			.500	-.823	.455	.500	-.674	.496			
			.600	-.293	.601	.600	-.237	.603			
			.700	.065	.700	.700	.053	.657			
			.800	.218	.747	.800	.322	.771			
			.900	.321	.771	.900	.362	.782			
			.950	.289	.761	.950	.354	.780			
			1.000	-.218	.622						
CN=				.5367			.6056				
CM=				-.1113			-.1213				

[redacted]

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(*h*) M = 0.76. Continued.

$\delta_a = 3^o$; $\alpha = 3.89^o$; $C_L = 0.622$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.329	.314	0.000	1.087	.682	0.000	.077	.703	.050	-1.250	.336
.150	-1.466	.276	.012	-.393	.573	.012	-.482	.548	.150	-1.520	.262
.300	-1.474	.287	.025	-.880	.438	.025	-.693	.490	.300	-1.553	.252
.450	-.770	.469	.050	-1.204	.349	.050	-1.178	.356	.450	-.814	.457
.600	-.516	.539	.100	-1.458	.278	.100	-1.366	.304	.600	-.537	.533
.800	-.251	.612	.150	-1.422	.289	.150	-1.419	.289	.800	-.386	.575
.990	-.144	.642	.200	-1.455	.279	.200	-1.391	.297			
			.300	-1.051	.391	.300	-1.313	.319			
			.350	-1.049	.392	.350	-1.058	.389			
			.400	-.825	.453	.400	-.865	.442			
			.450	-.799	.461	.450	-.800	.460			
			.500	-.764	.470	.500	-.760	.472			
			.550	-.720	.482	.550	-.737	.478			
			.600	-.653	.501	.600	-.677	.494			
			.650	-.635	.506	.700	-.533	.534			
			.700	-.556	.528	.800	-.425	.564			
			.800	-.455	.556	.900	-.344	.586			
			.900	-.332	.590	.950	-.314	.595			
			.950	-.358	.583	.990	-.264	.608			
			.990	-.228	.618						
					LOWER SURFACE						
.100	-.034	.672	.025	.326	.771	.025	.430	.800	.100	-.392	.573
.300	-.444	.553	.050	.023	.688	.050	-.054	.667	.300	-.555	.528
.600	-.334	.589	.100	-.137	.630	.100	-.221	.620	.600	-.338	.588
.800	.120	.715	.200	-.387	.575	.200	-.388	.574	.800	.240	.748
			.300	-.527	.536	.300	-.598	.519			
			.400	-.614	.512	.400	-.640	.505			
			.500	-.813	.457	.500	-.660	.499			
			.600	-.303	.598	.600	-.308	.599			
			.700	.045	.694	.700	.040	.693			
			.800	.238	.747	.800	.320	.770			
			.900	.339	.775	.900	.353	.779			
			.950	.274	.757	.950	.347	.777			
			1.000	-.247	.613						
CN=				.5913			.6409				
CM=				-.1158			-.1215				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 6^o$; $\alpha = -4.74^o$; $C_L = -0.236$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.325	.592	0.000	1.120	.591	0.000	.085	.704	.050	-.260	.610
.150	-.504	.543	.012	.473	.812	.012	.422	.798	.150	-.484	.549
.300	-.559	.528	.025	.079	.704	.025	.141	.721	.300	-.593	.519
.450	-.475	.551	.050	-.267	.608	.050	-.259	.611	.450	-.562	.527
.600	-.568	.525	.100	-.394	.574	.100	-.394	.573	.600	-.632	.508
.800	-.368	.581	.150	-.469	.553	.150	-.486	.570	.800	-.388	.603
.990	.074	.702	.200	-.545	.532	.200	-.525	.537			
			.300	-.592	.519	.300	-.615	.512			
			.350	-.585	.521	.350	-.580	.522			
			.400	-.579	.522	.400	-.572	.524			
			.450	-.564	.527	.450	-.632	.508			
			.500	-.736	.479	.500	-.707	.487			
			.550	-.796	.463	.550	-.913	.457			
			.600	-.625	.510	.600	-.737	.479			
			.650	-.667	.498	.700	-.407	.570			
			.700	-.597	.517	.800	-.147	.641			
			.800	-.323	.593	.900	-.127	.647			
			.900	-.028	.674	.950	-.131	.646			
			.950	.051	.696	.990	-.121	.649			
			.990	.095	.708						
					LOWER SURFACE						
.100	-1.037	.395	.025	-.501	.544	.025	-.375	.579	.100	-1.346	.311
.300	-1.273	.331	.050	-1.020	.401	.050	-.961	.417	.300	-1.613	.292
.600	-.318	.594	.100	-1.181	.356	.100	-1.226	.344	.600	-.285	.603
.800	-.019	.677	.200	-1.270	.332	.200	-1.268	.324	.800	.160	.726
			.300	-1.347	.311	.300	-1.342	.312			
			.400	-.735	.479	.400	-.750	.475			
			.500	-.653	.502	.500	-.632	.508			
			.600	-.436	.562	.600	-.499	.545			
			.700	-.105	.653	.700	-.313	.596			
			.800	-.000	.682	.800	-.094	.656			
			.900	.112	.713	.900	.046	.695			
			.950	.245	.750	.950	.135	.719			
			1.000	.087	.706						
CN=				-.1653			-.2035				
CM=				-.0892			-.0582				

(h) M = 0.76. Continued.

$\delta_a = 6^o$; $\alpha = -3.13^o$; $C_L = -0.066$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.536	.534	0.000	1.130	.994	0.000	.096	.709	.050	-.523	.538
.150	-.720	.484	.012	.281	.760	.012	.246	.750	.150	-.475	.496
.300	-.712	.486	.025	-.112	.651	.025	-.051	.668	.300	-.780	.467
.450	-.564	.527	.050	-.409	.544	.050	-.476	.551	.450	-.594	.518
.600	-.589	.520	.100	-.509	.517	.100	-.503	.519	.600	-.651	.503
.800	-.362	.582	.150	-.610	.514	.150	-.556	.529	.800	-.315	.595
.990	.053	.699	.200	-.753	.474	.200	-.661	.500			
			.300	-.726	.482	.300	-.784	.466			
			.350	-.751	.475	.350	-.776	.468			
			.400	-.628	.509	.400	-.648	.503			
			.450	-.619	.511	.450	-.641	.505			
			.500	-.710	.486	.500	-.727	.482			
			.550	-.856	.446	.550	-.847	.448			
			.600	-.769	.470	.600	-.854	.447			
			.650	-.595	.518	.700	-.388	.575			
			.700	-.573	.524	.800	-.163	.637			
			.800	-.303	.598	.900	-.143	.643			
			.900	-.039	.671	.950	-.146	.642			
			.950	.038	.692	.990	-.138	.644			
			.990	.061	.699						
					LOWER SURFACE						
.100	-.940	.423	.025	-.305	.598	.025	-.230	.619	.100	-1.194	.353
.300	-1.144	.367	.050	-.833	.452	.050	-.791	.464	.300	-1.270	.332
.600	-.277	.606	.100	-1.056	.391	.100	-1.085	.383	.600	-.270	.608
.800	.008	.684	.200	-1.122	.373	.200	-1.123	.372	.800	.253	.752
			.300	-1.174	.358	.300	-1.241	.340			
			.400	-1.302	.323	.400	-.793	.464			
			.500	-.597	.518	.500	-.496	.545			
			.600	-.222	.621	.600	-.316	.595			
			.700	.054	.697	.700	-.134	.645			
			.800	.246	.750	.800	.093	.708			
			.900	.325	.772	.900	.180	.732			
			.950	.325	.772	.950	.261	.754			
			1.000	.085	.705						
CN=				-.0150			.0147				
CM=				-.1161			-.0966				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 6^o$; $\alpha = -1.21^o$; $C_L = 0.193$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.733	.464	0.000	1.137	.996	0.000	.101	.710	.050	-.770	.470
.150	-.563	.476	.012	.099	.710	.012	.035	.692	.150	-1.102	.378
.300	-.341	.423	.025	-.352	.582	.025	-.248	.608	.300	-.867	.443
.450	-.717	.420	.050	-.739	.478	.050	-.729	.481	.450	-.656	.501
.600	-.534	.521	.100	-1.002	.406	.100	-.924	.427	.600	-.686	.493
.800	-.733	.560	.150	-.934	.425	.150	-.903	.433	.800	-.344	.587
.990	.047	.701	.200	-.960	.417	.200	-.880	.439			
			.300	-.970	.415	.300	-.969	.415			
			.350	-1.014	.402	.350	-.993	.408			
			.400	-1.013	.403	.400	-.974	.413			
			.450	-.954	.419	.450	-1.008	.404			
			.500	-.937	.424	.500	-.925	.427			
			.550	-.974	.413	.550	-.884	.438			
			.600	-.614	.513	.600	-.659	.489			
			.650	-.582	.522	.700	-.387	.575			
			.700	-.550	.530	.800	-.185	.631			
			.800	-.299	.600	.900	-.159	.638			
			.900	-.036	.672	.950	-.159	.638			
			.950	.031	.691	.990	-.161	.638			
			.990	.068	.701						
					LOWER SURFACE						
.100	-.615	.513	.025	-.112	.651	.025	-.023	.676	.100	-1.041	.395
.300	-.916	.436	.050	-.549	.525	.050	-.608	.514	.300	-.972	.414
.600	-.735	.517	.100	-.772	.490	.100	-.869	.442	.600	-.253	.612
.830	.033	.707	.200	-.778	.468	.200	-.843	.450	.800	.262	.754
			.300	-.930	.426	.300	-1.004	.405			
			.400	-1.018	.401	.400	-1.109	.376			
			.500	-.593	.519	.500	-.461	.555			
			.600	-.240	.616	.600	-.155	.639			
			.700	.079	.704	.700	.102	.710			
			.800	.241	.749	.800	.299	.764			
			.900	.347	.778	.900	.357	.781			
			.950	.357	.780	.950	.366	.783			
			1.000	.047	.700						
CN=				.2773			.2810				
CM=				-.1186			-.1281				

(h) M = 0.76. Continued.

$\delta_a = 6^o$; $\alpha = 0.61^o$; $C_L = 0.421$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.005	.405	0.000	1.129	.993	0.000	.100	.710	.050	-.973	.414
.150	-1.131	.387	.012	-.082	.660	.012	-.148	.641	.150	-1.283	.328
.300	-1.158	.383	.025	-.563	.527	.025	-.435	.562	.300	-1.270	.332
.450	-1.064	.399	.050	-.950	.420	.050	-.817	.429	.450	-.706	.487
.630	-.535	.543	.100	-1.190	.354	.100	-1.110	.376	.600	-.625	.510
.800	-.340	.588	.150	-1.129	.371	.150	-1.136	.369	.800	-.356	.593
.990	.069	.701	.200	-1.201	.351	.200	-1.105	.377			
			.300	-1.216	.347	.300	-1.193	.353			
			.350	-1.211	.348	.350	-1.181	.356			
			.400	-1.220	.346	.400	-1.197	.352			
			.450	-1.220	.346	.450	-1.245	.339			
			.500	-1.247	.338	.500	-1.274	.331			
			.550	-.911	.431	.550	-.856	.446			
			.600	-.651	.502	.600	-.627	.509			
			.650	-.473	.552	.700	-.421	.566			
			.700	-.403	.571	.800	-.258	.611			
			.800	-.229	.619	.900	-.197	.628			
			.900	-.111	.652	.950	-.196	.628			
			.950	-.044	.670	.990	-.193	.629			
			.990	-.004	.681						
					LOWER SURFACE						
.100	-.408	.570	.025	.053	.697	.025	.165	.729	.100	-.773	.449
.300	-.549	.503	.050	-.324	.593	.050	-.408	.569	.300	-.694	.491
.600	-.757	.611	.100	-.500	.544	.100	-.525	.537	.600	-.245	.614
.800	.149	.723	.200	-.687	.493	.200	-.645	.504	.800	.261	.754
			.300	-.703	.488	.300	-.847	.448			
			.400	-.747	.476	.400	-.668	.498			
			.500	-.732	.480	.500	-.538	.534			
			.600	-.243	.615	.600	-.173	.634			
			.700	.093	.705	.700	.126	.717			
			.800	.256	.753	.800	.336	.775			
			.900	.355	.780	.900	.387	.789			
			.950	.363	.782	.950	.387	.789			
			1.000	-.003	.681						
CN=				.4594			.5289				
CM=				-.1139			-.1413				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\delta_a = 6^o$; $\alpha = 1.84^o$; $C_L = 0.503$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.109	.376	0.000	1.127	.593	0.000	.098	.709	.050	-1.091	.381
.150	-1.309	.321	.012	-.217	.622	.012	-.283	.604	.150	-1.380	.302
.300	-1.246	.327	.025	-.694	.491	.025	-.552	.530	.300	-1.412	.293
.450	-1.126	.372	.050	-1.060	.390	.050	-1.044	.394	.450	-.846	.469
.600	-.476	.551	.100	-1.309	.321	.100	-1.227	.344	.600	-.588	.520
.800	-.316	.595	.150	-1.287	.327	.150	-1.246	.338	.800	-.386	.576
.990	-.031	.674	.200	-1.304	.323	.200	-1.251	.337			
			.300	-1.316	.319	.300	-1.279	.330			
			.350	-1.321	.318	.350	-1.286	.327			
			.400	-1.319	.318	.400	-1.297	.324			
			.450	-.994	.408	.450	-1.326	.316			
			.500	-.774	.469	.500	-.987	.410			
			.550	-.649	.503	.550	-.707	.487			
			.600	-.624	.510	.600	-.634	.507			
			.650	-.516	.540	.700	-.475	.551			
			.700	-.404	.571	.800	-.343	.588			
			.800	-.281	.605	.900	-.284	.604			
			.900	-.137	.628	.950	-.261	.610			
			.950	-.160	.638	.990	-.228	.619			
			.990	-.158	.639						
					LOWER SURFACE						
.100	-.321	.594	.025	.153	.724	.025	.287	.761	.100	-.611	.514
.300	-.574	.524	.050	-.211	.624	.050	-.265	.609	.300	-.632	.508
.600	-.312	.596	.100	-.374	.575	.100	-.408	.570	.600	-.254	.612
.800	.116	.714	.200	-.554	.529	.200	-.536	.534	.800	.262	.763
			.300	-.664	.499	.300	-.750	.475			
			.400	-.730	.481	.400	-.665	.499			
			.500	-.824	.455	.500	-.557	.529			
			.600	-.271	.607	.600	-.190	.630			
			.700	.041	.699	.700	.131	.718			
			.800	.247	.750	.800	.347	.778			
			.900	.353	.779	.900	.388	.789			
			.950	.321	.771	.950	.377	.786			
			1.000	-.118	.650						
CN=				.4993			.6214				
CM=				-.1024			-.1440				

(h) M = 0.76. Concluded.

$\delta_a = 6^o$; $\alpha = 3.13^o$; $C_L = 0.590$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.249	.338	0.000	1.088	.582	0.000	.085	.706	.050	-1.210	.349
.150	-1.419	.291	.012	-.311	.597	.012	-.400	.572	.150	-1.478	.275
.300	-1.374	.303	.025	-.809	.459	.025	-.647	.504	.300	-1.528	.261
.450	-.852	.447	.050	-1.159	.363	.050	-1.133	.370	.450	-.838	.451
.600	-.443	.549	.100	-1.400	.296	.100	-1.332	.315	.600	-.554	.529
.800	-.277	.606	.150	-1.395	.298	.150	-1.343	.306	.800	-.416	.567
.990	-.039	.673	.200	-1.415	.292	.200	-1.335	.314			
			.300	-1.425	.289	.300	-1.337	.297			
			.350	-1.290	.327	.350	-1.382	.298			
			.400	-1.170	.360	.400	-1.329	.316			
			.450	-.834	.452	.450	-1.057	.391			
			.500	-.744	.466	.500	-.788	.465			
			.550	-.723	.483	.550	-.717	.485			
			.600	-.623	.510	.600	-.650	.503			
			.650	-.552	.530	.700	-.498	.545			
			.700	-.443	.560	.800	-.379	.578			
			.800	-.390	.575	.900	-.327	.592			
			.900	-.359	.583	.950	-.305	.598			
			.950	-.217	.622	.990	-.274	.607			
			.990	-.234	.618						
					LOWER SURFACE						
.100	-.142	.632	.025	.231	.763	.025	.383	.788	.100	-.458	.556
.300	-.492	.546	.050	-.041	.671	.050	-.133	.646	.300	-.572	.524
.600	-.311	.597	.100	-.237	.617	.100	-.289	.602	.600	-.263	.610
.800	.150	.726	.200	-.428	.564	.200	-.441	.560	.900	.300	.765
			.300	-.540	.528	.300	-.608	.514			
			.400	-.618	.512	.400	-.631	.508			
			.500	-.747	.471	.500	-.659	.528			
			.600	-.287	.603	.600	-.211	.624			
			.700	.059	.698	.700	.126	.717			
			.800	.260	.754	.800	.365	.783			
			.900	.359	.781	.900	.389	.789			
			.950	.324	.772	.950	.370	.784			
			1.000	-.171	.635						
CN=				.6214			.6957				
CM=				-.1199			-.1422				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(i) M = 0.80

$\delta_a = 0^o$; $\alpha = -4.50^o$; $C_L = -0.206$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.273	.576	0.000	1.139	.551	0.000	.085	.681	.050	-.302	.567
.150	-.555	.493	.012	.463	.752	.012	.400	.774	.150	-.542	.497
.300	-.617	.475	.025	.097	.685	.025	.131	.695	.300	-.688	.454
.450	-.616	.475	.050	-.263	.579	.050	-.240	.585	.450	-.636	.469
.600	-.729	.442	.100	-.436	.528	.100	-.391	.541	.600	-.771	.429
.800	-.378	.545	.150	-.458	.521	.150	-.426	.531	.800	-.314	.564
.990	-.099	.627	.200	-.555	.481	.200	-.523	.502			
			.300	-.616	.475	.300	-.663	.459			
			.350	-.645	.466	.350	-.697	.451			
			.400	-.653	.465	.400	-.698	.451			
			.450	-.634	.470	.450	-.710	.447			
			.500	-.792	.423	.500	-.766	.431			
			.550	-.861	.403	.550	-.865	.402			
			.600	-.850	.406	.600	-.921	.385			
			.650	-.911	.388	.700	-.560	.491			
			.700	-.490	.515	.800	-.267	.577			
			.800	-.213	.593	.900	-.164	.608			
			.900	-.144	.614	.950	-.155	.610			
			.950	-.101	.626	.990	-.127	.619			
			.990	-.084	.631						
					LOWER SURFACE						
.100	-.916	.387	.025	-.378	.545	.025	-.231	.588	.100	-1.199	.303
.300	-1.121	.326	.050	-.873	.399	.050	-.816	.416	.300	-1.231	.294
.600	-.328	.560	.100	-1.018	.357	.100	-1.049	.348	.600	-.524	.502
.800	-.286	.572	.200	-1.114	.329	.200	-1.116	.328	.800	-.253	.582
			.300	-1.214	.299	.300	-1.130	.324			
			.400	-1.116	.328	.400	-.657	.463			
			.500	-.667	.460	.500	-.552	.494			
			.600	-.500	.505	.600	-.534	.499			
			.700	-.411	.535	.700	-.490	.512			
			.800	-.144	.614	.800	-.334	.558			
			.900	-.041	.644	.900	-.211	.594			
			.950	.013	.660	.950	-.144	.614			
			1.000	-.041	.644						
CN=				-.1881			-.1371				
CM=				-.0509			-.0329				

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = -3.16^o$; $C_L = -0.114$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.411	.535	0.000	1.141	.551	0.000	.105	.687	.050	-.444	.525
.150	-.681	.486	.012	.354	.760	.012	.287	.740	.150	-.791	.423
.300	-.647	.486	.025	-.044	.643	.025	.016	.661	.300	-.645	.466
.450	-.722	.444	.050	-.426	.531	.050	-.457	.521	.450	-.732	.441
.600	-.791	.423	.100	-.614	.475	.100	-.527	.501	.600	-.820	.415
.800	-.336	.557	.150	-.575	.487	.150	-.553	.493	.800	-.243	.584
.990	-.054	.640	.200	-.694	.452	.200	-.575	.487			
			.300	-.785	.425	.300	-.756	.433			
			.350	-.763	.431	.350	-.785	.425			
			.400	-.738	.439	.400	-.776	.428			
			.450	-.679	.456	.450	-.827	.413			
			.500	-.855	.404	.500	-.849	.406			
			.550	-.930	.382	.550	-.937	.380			
			.600	-.518	.386	.600	-.994	.364			
			.650	-.542	.497	.700	-.366	.548			
			.700	-.312	.564	.800	-.211	.594			
			.800	-.200	.597	.900	-.155	.610			
			.900	-.125	.619	.950	-.144	.614			
			.950	-.117	.622	.990	-.094	.628			
			.990	-.114	.622						
					LOWER SURFACE						
.100	-.821	.415	.025	-.256	.581	.025	-.117	.621	.100	-1.076	.339
.300	-1.053	.346	.050	-.747	.436	.050	-.674	.458	.300	-1.235	.293
.600	-.314	.564	.100	-.915	.387	.100	-.962	.373	.600	-.501	.509
.800	-.271	.576	.200	-.997	.363	.200	-1.022	.355	.800	-.262	.579
			.300	-1.116	.328	.300	-1.133	.323			
			.400	-1.209	.301	.400	-.716	.445			
			.500	-.608	.477	.500	-.587	.483			
			.600	-.446	.525	.600	-.551	.494			
			.700	-.354	.552	.700	-.364	.549			
			.800	-.179	.603	.800	-.290	.571			
			.900	-.012	.652	.900	-.148	.612			
			.950	.036	.666	.950	-.087	.630			
			1.000	-.064	.637						
CN=				-.1164			-.0616				
CM=				-.0368			-.0293				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Continued

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = -1.85^o$; $C_L = -0.029$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.585	.484	0.000	1.146	.993	0.000	.086	.681	.050	-.624	.473
.150	-.823	.414	.012	.246	.728	.012	.164	.704	.150	-.932	.387
.300	-.808	.419	.025	-.185	.602	.025	-.101	.626	.300	-.936	.381
.450	-.752	.435	.050	-.529	.501	.050	-.558	.492	.450	-.742	.438
.600	-.655	.464	.100	-.815	.416	.100	-.711	.447	.600	-.829	.413
.800	-.279	.574	.150	-.757	.434	.150	-.732	.441	.800	-.247	.584
.990	.007	.658	.200	-.813	.417	.200	-.717	.445			
			.300	-.850	.406	.300	-.818	.416			
			.350	-.854	.405	.350	-.857	.404			
			.400	-.865	.402	.400	-.875	.399			
			.450	-.824	.414	.450	-.934	.382			
			.500	-.927	.384	.500	-.980	.368			
			.550	-.979	.368	.550	-1.051	.347			
			.600	-.651	.465	.600	-.826	.413			
			.650	-.415	.534	.700	-.358	.551			
			.700	-.297	.569	.800	-.239	.586			
			.800	-.168	.607	.900	-.138	.616			
			.900	-.117	.622	.950	-.110	.624			
			.950	-.102	.626	.990	-.087	.630			
			.990	-.068	.636						
					LOWER SURFACE						
.100	-.678	.457	.025	-.158	.610	.025	-.026	.648	.100	-.996	.363
.300	-.979	.368	.050	-.625	.472	.050	-.597	.481	.300	-1.179	.310
.600	-.335	.558	.100	-.803	.420	.100	-.887	.395	.600	-.409	.536
.800	-.246	.584	.200	-.893	.394	.200	-.921	.385	.800	.028	.664
			.300	-1.023	.355	.300	-1.038	.351			
			.400	-1.119	.327	.400	-.899	.392			
			.500	-.587	.484	.500	-.467	.519			
			.600	-.415	.534	.600	-.471	.518			
			.700	-.328	.560	.700	-.409	.534			
			.800	-.162	.609	.800	-.344	.555			
			.900	-.026	.649	.900	-.150	.612			
			.950	.056	.673	.950	-.095	.629			
			1.000	-.041	.644						
CN=				-.0126			.0129				
CM=				-.0317			-.0193				

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = -0.57^o$; $C_L = 0.062$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.699	.451	0.000	1.155	.996	0.000	.085	.681	.050	-.721	.444
.150	-.918	.386	.012	.126	.693	.012	.048	.670	.150	-1.017	.357
.300	-.927	.384	.025	-.331	.559	.025	-.196	.598	.300	-1.040	.350
.450	-.871	.400	.050	-.658	.463	.050	-.648	.466	.450	-.824	.414
.600	-.451	.523	.100	-.914	.387	.100	-.930	.412	.600	-.599	.480
.800	-.235	.587	.150	-.869	.401	.150	-.855	.405	.800	-.254	.581
.990	-.014	.652	.200	-.959	.374	.200	-.846	.407			
			.300	-.966	.372	.300	-.942	.379			
			.350	-.956	.375	.350	-.964	.373			
			.400	-.977	.369	.400	-.991	.365			
			.450	-.932	.382	.450	-1.026	.355			
			.500	-1.018	.357	.500	-1.045	.349			
			.550	-.577	.486	.550	-.764	.431			
			.600	-.415	.534	.600	-.473	.517			
			.650	-.383	.544	.700	-.353	.552			
			.700	-.306	.566	.800	-.270	.577			
			.800	-.175	.605	.900	-.155	.611			
			.900	-.136	.616	.950	-.156	.610			
			.950	-.081	.632	.990	-.070	.636			
			.990	-.086	.631						
					LOWER SURFACE						
.100	-.592	.482	.025	-.061	.638	.025	.059	.673	.100	-.910	.389
.300	-.863	.402	.050	-.486	.513	.050	-.497	.510	.300	-1.066	.343
.600	-.311	.565	.100	-.676	.457	.100	-.782	.426	.600	-.466	.519
.800	-.196	.598	.200	-.775	.428	.200	-.757	.434	.800	.111	.689
			.300	-.898	.392	.300	-.928	.383			
			.400	-.998	.363	.400	-1.083	.338			
			.500	-.987	.366	.500	-.473	.517			
			.600	-.405	.537	.600	-.454	.523			
			.700	-.302	.567	.700	-.392	.541			
			.800	-.207	.595	.800	-.290	.571			
			.900	-.041	.644	.900	-.137	.616			
			.950	.081	.680	.950	-.016	.651			
			1.000	-.067	.636						
CN=				.0327			.0779				
CM=				-.0115			-.0150				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(i) $M = 0.80$. Continued.

$\delta_a = 0^o$; $\alpha = 0.08^o$; $C_L = 0.109$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.727	.442	0.000	1.142	.992	0.000	.085	.681	.050	-.753	.435
.150	-.976	.369	.012	.072	.677	.012	.033	.666	.150	-1.084	.337
.300	-.994	.364	.025	-.359	.550	.025	-.260	.580	.300	-1.087	.336
.450	-.951	.376	.050	-.724	.443	.050	-.708	.448	.450	-.870	.400
.600	-.429	.530	.100	-.965	.372	.100	-.920	.385	.600	-.535	.499
.800	-.219	.591	.150	-.927	.383	.150	-.916	.387	.900	-.260	.580
.950	-.019	.650	.200	-.980	.368	.200	-.895	.393			
			.300	-1.045	.349	.300	-1.009	.359			
			.350	-1.035	.352	.350	-.985	.366			
			.400	-1.040	.350	.400	-1.016	.357			
			.450	-1.037	.351	.450	-1.071	.341			
			.500	-.719	.445	.500	-1.057	.345			
			.550	-.493	.511	.550	-.541	.497			
			.600	-.432	.529	.600	-.452	.523			
			.650	-.381	.544	.700	-.380	.544			
			.700	-.317	.563	.800	-.299	.568			
			.800	-.234	.587	.900	-.217	.592			
			.900	-.143	.612	.950	-.177	.604			
			.950	-.147	.613	.990	-.121	.620			
			.990	-.135	.616						
					LOWER SURFACE						
.100	-.497	.510	.025	-.024	.649	.025	.131	.694	.100	-.848	.407
.300	-.843	.408	.050	-.408	.536	.050	-.453	.523	.300	-1.010	.359
.600	-.371	.547	.100	-.557	.481	.100	-.589	.483	.600	-.445	.525
.800	-.204	.596	.200	-.722	.444	.200	-.727	.442	.800	.119	.691
			.300	-.849	.407	.300	-.886	.395			
			.400	-.976	.369	.400	-1.054	.346			
			.500	-1.117	.328	.500	-.546	.496			
			.600	-.409	.536	.600	-.445	.525			
			.700	-.297	.569	.700	-.382	.544			
			.800	-.190	.600	.800	-.255	.581			
			.900	.005	.659	.900	-.140	.615			
			.950	.126	.693	.950	-.018	.651			
			1.000	-.070	.635						
CN=				.0619			.1312				
CM=				-.0122			-.0167				

(i) $M = 0.80$. Continued.

$\delta_a = 0^o$; $\alpha = 0.70^o$; $C_L = 0.153$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.800	.421	0.000	1.145	.993	0.000	.089	.682	.050	-.817	.416
.150	-1.031	.353	.012	.032	.665	.012	-.049	.642	.150	-1.121	.327
.300	-1.047	.348	.025	-.403	.538	.025	-.311	.565	.300	-1.186	.307
.450	-.966	.372	.050	-.767	.431	.050	-.763	.432	.450	-.935	.381
.600	-.417	.534	.100	-1.000	.362	.100	-.933	.382	.600	-.458	.521
.800	-.227	.589	.150	-1.010	.359	.150	-.990	.365	.800	-.285	.572
.950	-.015	.652	.200	-1.049	.348	.200	-.955	.375			
			.300	-1.075	.340	.300	-1.040	.350			
			.350	-1.066	.343	.350	-1.060	.345			
			.400	-1.092	.335	.400	-1.067	.342			
			.450	-1.042	.350	.450	-1.121	.327			
			.500	-.592	.432	.500	-.668	.460			
			.550	-.491	.517	.550	-.521	.503			
			.600	-.445	.525	.600	-.483	.514			
			.650	-.391	.541	.700	-.399	.539			
			.700	-.342	.556	.800	-.344	.555			
			.800	-.258	.580	.900	-.266	.578			
			.900	-.197	.598	.950	-.241	.585			
			.950	-.168	.607	.990	-.136	.616			
			.990	-.159	.609						
					LOWER SURFACE						
.100	-.436	.528	.025	.045	.669	.025	.162	.704	.100	-.780	.427
.300	-.796	.422	.050	-.331	.559	.050	-.392	.541	.300	-.589	.365
.600	-.362	.550	.100	-.517	.504	.100	-.517	.504	.600	-.400	.538
.800	-.201	.597	.200	-.660	.462	.200	-.692	.453	.900	.058	.673
			.300	-.820	.415	.300	-.868	.401			
			.400	-.944	.379	.400	-1.010	.359			
			.500	-1.131	.324	.500	-.724	.443			
			.600	-.405	.537	.600	-.448	.524			
			.700	-.279	.574	.700	-.386	.543			
			.800	-.149	.613	.800	-.269	.577			
			.900	.075	.678	.900	-.037	.645			
			.950	.146	.699	.950	.020	.662			
			1.000	-.103	.626						
CN=				.1202			.1535				
CM=				-.0207			-.0164				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF;

AILERON UNSEALED - Continued

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = 1.99^o$; $C_L = 0.253$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.927	.384	0.000	1.145	.992	0.000	.085	.681	.050	-.957	.375
.150	-1.144	.320	.012	-.085	.631	.012	-.157	.610	.150	-1.218	.298
.300	-1.119	.327	.025	-.523	.502	.025	-.376	.546	.300	-1.280	.280
.450	-.762	.432	.050	-.880	.398	.050	-.863	.403	.450	-.997	.363
.600	-.434	.529	.100	-1.120	.327	.100	-1.074	.341	.600	-.531	.500
.800	-.193	.600	.150	-1.102	.333	.150	-1.084	.338	.800	-.325	.561
.950	-.023	.649	.200	-1.130	.324	.200	-1.072	.341			
			.300	-1.167	.313	.300	-1.139	.321			
			.350	-1.116	.328	.350	-1.128	.325			
			.400	-.836	.410	.400	-1.115	.328			
			.450	-.600	.480	.450	-.699	.451			
			.500	-.561	.491	.500	-.565	.490			
			.550	-.534	.499	.550	-.530	.500			
			.600	-.508	.507	.600	-.503	.508			
			.650	-.375	.546	.700	-.436	.528			
			.700	-.374	.546	.800	-.382	.544			
			.800	-.274	.576	.900	-.324	.561			
			.900	-.251	.583	.950	-.297	.569			
			.950	-.213	.594	.990	-.212	.594			
			.990	-.186	.601						
					LOWER SURFACE						
.100	-.242	.585	.025	.153	.701	.025	.276	.737	.100	-.637	.469
.300	-.754	.435	.050	-.188	.601	.050	-.259	.580	.300	-.785	.425
.600	-.398	.539	.100	-.400	.539	.100	-.432	.529	.600	-.428	.530
.800	-.166	.607	.200	-.593	.482	.200	-.573	.488	.800	-.013	.652
			.300	-.698	.451	.300	-.773	.429			
			.400	-.825	.414	.400	-.947	.378			
			.500	-1.058	.345	.500	-1.021	.356			
			.600	-.385	.543	.600	-.418	.533			
			.700	-.250	.583	.700	-.348	.554			
			.800	-.062	.638	.800	-.190	.600			
			.900	.103	.687	.900	-.037	.645			
			.950	.122	.652	.950	.088	.682			
			1.000	-.162	.609						
CN=				.2157			.2254				
CM=				-.0295			-.0237				

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = 3.27^o$; $C_L = 0.352$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.076	.340	0.000	1.129	.588	0.000	.061	.674	.050	-1.062	.344
.150	-1.243	.291	.012	-.198	.598	.012	-.288	.572	.150	-1.310	.271
.300	-.956	.375	.025	-.650	.465	.025	-.479	.515	.300	-1.365	.255
.450	-.577	.487	.050	-.986	.366	.050	-.961	.374	.450	-.729	.442
.600	-.474	.517	.100	-1.215	.299	.100	-1.139	.321	.600	-.611	.476
.800	-.302	.567	.150	-1.181	.309	.150	-1.184	.308	.800	-.404	.537
.950	-.211	.594	.200	-1.232	.294	.200	-1.168	.313			
			.300	-1.214	.299	.300	-1.254	.288			
			.350	-.768	.430	.350	-1.175	.311			
			.400	-.731	.441	.400	-.761	.432			
			.450	-.663	.461	.450	-.618	.474			
			.500	-.659	.462	.500	-.594	.481			
			.550	-.631	.471	.550	-.566	.490			
			.600	-.478	.516	.600	-.540	.497			
			.650	-.514	.505	.700	-.473	.517			
			.700	-.393	.540	.800	-.438	.527			
			.800	-.375	.546	.900	-.341	.556			
			.900	-.281	.573	.950	-.321	.562			
			.950	-.233	.588	.990	-.286	.572			
			.990	-.249	.583						
					LOWER SURFACE						
.100	-.169	.607	.025	.267	.734	.025	.406	.776	.100	-.538	.498
.300	-.608	.477	.050	-.064	.637	.050	-.161	.609	.300	-.727	.442
.600	-.376	.546	.100	-.263	.579	.100	-.311	.565	.600	-.469	.518
.800	-.127	.619	.200	-.485	.514	.200	-.482	.514	.800	-.006	.654
			.300	-.615	.475	.300	-.704	.449			
			.400	-.772	.429	.400	-.878	.398			
			.500	-1.001	.362	.500	-.948	.377			
			.600	-.412	.535	.600	-.377	.545			
			.700	-.267	.578	.700	-.309	.565			
			.800	-.047	.642	.800	-.114	.622			
			.900	.148	.699	.900	.058	.673			
			.950	.189	.712	.950	.071	.677			
			1.000	-.170	.606						
CN=				.3164			.3223				
CM=				-.0452			-.0348				

TABLE IV.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED - Concluded

(i) M = 0.80. Continued.

$\delta_a = 0^o$; $\alpha = 4.68^o$; $C_L = 0.481$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.204	.403	0.000	1.098	.979	0.000	.036	.667	.050	-1.147	.319
.150	-1.347	.261	.012	-.315	.563	.012	-.391	.541	.150	-1.397	.246
.300	-.944	.167	.025	-.763	.432	.025	-.573	.488	.300	-1.405	.244
.450	-.574	.493	.050	-1.119	.327	.050	-1.046	.349	.450	-.795	.423
.600	-.515	.505	.100	-1.308	.272	.100	-1.238	.293	.600	-.659	.463
.800	-.382	.544	.150	-1.296	.276	.150	-1.277	.281	.800	-.475	.517
.950	-.284	.571	.200	-1.340	.263	.200	-1.280	.280			
			.300	-1.068	.342	.300	-1.035	.352			
			.350	-.884	.397	.350	-1.041	.351			
			.400	-.850	.407	.400	-.767	.431			
			.450	-.791	.424	.450	-.707	.449			
			.500	-.763	.432	.500	-.666	.461			
			.550	-.640	.468	.550	-.615	.476			
			.600	-.576	.487	.600	-.558	.492			
			.650	-.552	.494	.700	-.509	.507			
			.700	-.557	.493	.800	-.478	.516			
			.800	-.331	.544	.900	-.435	.528			
			.900	-.326	.561	.950	-.339	.557			
			.950	-.300	.568	.990	-.294	.570			
			.990	-.256	.581						
					LOWER SURFACE						
.100	-.013	.653	.025	.383	.769	.025	.501	.803	.100	-.367	.548
.300	-.453	.523	.050	.084	.675	.050	-.004	.655	.300	-.664	.461
.600	-.404	.537	.100	-.152	.612	.100	-.211	.594	.600	-.554	.493
.800	-.069	.636	.200	-.374	.547	.200	-.378	.545	.800	.017	.661
			.300	-.542	.497	.300	-.642	.468			
			.400	-.661	.462	.400	-.749	.436			
			.500	-.939	.380	.500	-.847	.408			
			.600	-.371	.547	.600	-.360	.551			
			.700	-.135	.617	.700	-.267	.578			
			.800	.003	.657	.800	-.019	.651			
			.900	.256	.732	.900	.075	.678			
			.950	.246	.728	.950	.190	.712			
			1.000	-.226	.590						
CN=				.4662			.4408				
CM=				-.0754			-.0626				

(i) M = 0.80. Concluded.

$\delta_a = 0^o$; $\alpha = 5.33^o$; $C_L = 0.533$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.275	.282	0.000	1.083	.974	0.000	.008	.659	.050	-1.184	.308
.150	-1.319	.269	.012	-.359	.551	.012	-.439	.527	.150	-1.435	.235
.300	-.793	.423	.025	-.815	.416	.025	-.653	.464	.300	-1.373	.253
.450	-.493	.511	.050	-1.144	.320	.050	-1.093	.335	.450	-.807	.419
.600	-.529	.501	.100	-1.357	.258	.100	-1.285	.279	.600	-.680	.456
.800	-.411	.536	.150	-1.322	.268	.150	-1.325	.267	.800	-.490	.512
.990	-.338	.557	.200	-1.377	.252	.200	-1.318	.269			
			.300	-1.003	.362	.300	-1.064	.344			
			.350	-.958	.375	.350	-.951	.377			
			.400	-.840	.409	.400	-.808	.419			
			.450	-.813	.416	.450	-.731	.441			
			.500	-.761	.433	.500	-.699	.451			
			.550	-.666	.460	.550	-.626	.472			
			.600	-.543	.497	.600	-.569	.489			
			.650	-.513	.505	.700	-.536	.499			
			.700	-.488	.513	.800	-.417	.534			
			.800	-.392	.541	.900	-.391	.541			
			.900	-.277	.575	.950	-.378	.545			
			.950	-.290	.571	.990	-.322	.562			
			.990	-.290	.571						
					LOWER SURFACE						
.100	.034	.666	.025	.424	.781	.025	.527	.811	.100	-.320	.562
.300	-.437	.528	.050	.118	.691	.050	.068	.676	.300	-.636	.469
.600	-.428	.531	.100	-.066	.631	.100	-.127	.619	.600	-.547	.495
.800	-.071	.635	.200	-.323	.561	.200	-.349	.554	.800	-.010	.653
			.300	-.505	.508	.300	-.606	.478			
			.400	-.649	.466	.400	-.683	.456			
			.500	-.907	.390	.500	-.811	.418			
			.600	-.379	.545	.600	-.394	.540			
			.700	-.157	.610	.700	-.191	.600			
			.800	.071	.677	.800	.074	.678			
			.900	.276	.737	.900	.177	.708			
			.950	.249	.729	.950	.227	.723			
			1.000	-.212	.594						
CN=				.4936			.5005				
CM=				-.0729			-.0720				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED

(a) M = 0.30

$\alpha = -4.14^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.431	.914	0.000	.979	.997	0.000	.081	.944	.050	-.311	.921
.150	-.439	.913	.012	.289	.956	.012	.264	.955	.150	-.352	.918
.300	-.417	.915	.025	-.094	.934	.025	-.003	.939	.300	-.374	.917
.450	-.389	.916	.050	-.341	.919	.050	-.320	.920	.450	-.384	.916
.600	-.431	.914	.100	-.379	.917	.100	-.304	.921	.600	-.409	.915
.800	-.392	.916	.150	-.423	.914	.150	-.324	.920	.800	-.334	.919
.990	.048	.942	.200	-.407	.915	.200	-.388	.916			
			.300	-.419	.914	.300	-.408	.915			
			.350	-.418	.914	.350	-.382	.917			
			.400	-.423	.914	.400	-.403	.915			
			.450	-.406	.915	.450	-.424	.914			
			.500	-.462	.912	.500	-.455	.912			
			.550	-.475	.911	.550	-.440	.913			
			.600	-.435	.913	.600	-.463	.912			
			.650	-.483	.911	.700	-.401	.915			
			.700	-.461	.912	.800	-.322	.920			
			.800	-.355	.918	.900	-.083	.934			
			.900	-.123	.932	.950	.020	.940			
			.950	.009	.940	.990	.092	.945			
			.990	.087	.944						
					LOWER SURFACE						
.100	-.769	.894	.025	-.744	.895	.025	-.769	.894	.100	-.877	.887
.300	-.593	.904	.050	-.938	.884	.050	-.972	.882	.300	-.536	.907
.600	-.322	.920	.100	-.836	.890	.100	-.804	.892	.600	-.280	.923
.800	.167	.949	.200	-.666	.900	.200	-.634	.902	.800	.192	.951
			.300	-.623	.902	.300	-.592	.904			
			.400	-.557	.906	.400	-.549	.907			
			.500	-.515	.909	.500	-.447	.913			
			.600	-.259	.924	.600	-.255	.924			
			.700	.032	.941	.700	.017	.940			
			.800	.215	.952	.800	.242	.954			
			.900	.293	.957	.900	.273	.955			
			.950	.303	.957	.950	.302	.957			
			1.000	.116	.946						
CN=				.0287			.0087				
CM=				-.1052			-.1032				

(a) M = 0.30. Continued.

$\alpha = -3.05^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.586	.905	0.000	1.005	.999	0.000	.051	.942	.050	-.488	.910
.150	-.524	.908	.012	.059	.943	.012	.053	.943	.150	-.443	.913
.300	-.453	.913	.025	-.348	.919	.025	-.250	.925	.300	-.427	.914
.450	-.417	.915	.050	-.528	.908	.050	-.475	.911	.450	-.413	.915
.600	-.453	.913	.100	-.515	.909	.100	-.473	.911	.600	-.444	.913
.800	-.406	.915	.150	-.520	.909	.150	-.413	.915	.800	-.339	.919
.990	.049	.942	.200	-.499	.910	.200	-.467	.912			
			.300	-.481	.911	.300	-.468	.912			
			.350	-.467	.912	.350	-.458	.912			
			.400	-.461	.912	.400	-.435	.914			
			.450	-.444	.913	.450	-.472	.911			
			.500	-.499	.910	.500	-.494	.910			
			.550	-.506	.909	.550	-.494	.910			
			.600	-.460	.912	.600	-.493	.910			
			.650	-.505	.909	.700	-.434	.914			
			.700	-.487	.911	.800	-.338	.919			
			.800	-.358	.918	.900	-.088	.934			
			.900	-.119	.932	.950	.014	.940			
			.950	.007	.940	.990	.064	.943			
			.990	.090	.945						
					LOWER SURFACE						
.100	-.659	.900	.025	-.539	.907	.025	-.452	.913	.100	-.772	.894
.300	-.544	.907	.050	-.745	.895	.050	-.797	.892	.300	-.510	.909
.600	-.309	.921	.100	-.670	.900	.100	-.661	.900	.600	-.269	.923
.800	.208	.952	.200	-.587	.905	.200	-.563	.906	.800	.208	.952
			.300	-.566	.906	.300	-.551	.907			
			.400	-.515	.909	.400	-.519	.909			
			.500	-.491	.910	.500	-.418	.915			
			.600	-.238	.925	.600	-.255	.924			
			.700	.052	.942	.700	.026	.941			
			.800	.241	.954	.800	.252	.954			
			.900	.329	.959	.900	.283	.956			
			.950	.321	.958	.950	.314	.958			
			1.000	.116	.946						
CN=				.1378			.1174				
CM=				-.1068			-.1025				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M =0.30. Continued.

$\alpha = -2.48^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.648	.901	C.000	1.019	1.000	C.000	.072	.944	.050	-.553	.907
.150	-.571	.905	.012	-.066	.935	.012	-.083	.934	.150	-.463	.912
.300	-.494	.910	.025	-.413	.915	.025	-.297	.922	.300	-.450	.913
.450	-.425	.914	.050	-.621	.903	.050	-.549	.907	.450	-.408	.915
.600	-.460	.912	.100	-.582	.905	.100	-.493	.910	.600	-.448	.913
.800	-.397	.916	.150	-.532	.908	.150	-.458	.912	.800	-.337	.919
.990	.044	.942	.200	-.541	.907	.200	-.509	.909			
			.300	-.506	.909	.300	-.492	.910			
			.350	-.486	.911	.350	-.465	.912			
			.400	-.484	.911	.400	-.455	.912			
			.450	-.457	.912	.450	-.480	.911			
			.500	-.514	.909	.500	-.502	.910			
			.550	-.518	.909	.550	-.492	.910			
			.600	-.470	.911	.600	-.501	.910			
			.650	-.507	.909	.700	-.434	.914			
			.700	-.492	.910	.800	-.340	.919			
			.800	-.359	.918	.900	-.084	.934			
			.900	-.123	.932	.950	.012	.940			
			.950	.004	.940	.990	.082	.944			
			.990	.090	.945						
					LOWER SURFACE						
.100	-.532	.905	.025	-.418	.915	.025	-.368	.918	.100	-.700	.898
.300	-.511	.909	.050	-.651	.901	.050	-.723	.896	.300	-.484	.911
.600	-.299	.922	.100	-.608	.903	.100	-.610	.903	.600	-.260	.924
.800	.219	.952	.200	-.546	.907	.200	-.517	.909	.800	.216	.952
			.300	-.519	.909	.300	-.511	.909			
			.400	-.481	.911	.400	-.484	.911			
			.500	-.462	.912	.500	-.404	.915			
			.600	-.222	.926	.600	-.226	.926			
			.700	.060	.943	.700	.036	.942			
			.800	.259	.955	.800	.270	.955			
			.900	.340	.960	.900	.292	.957			
			.950	.327	.959	.950	.335	.959			
			1.000	.112	.946						
CN=				.1893			.1657				
CM=				-.1087			-.1042				

(a) M = 0.30. Continued.

$\alpha = -1.97^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.739	.895	C.000	1.009	.999	C.000	.071	.944	.050	-.660	.900
.150	-.633	.902	.012	-.208	.927	.012	-.187	.928	.150	-.510	.909
.300	-.531	.908	.025	-.617	.903	.025	-.480	.911	.300	-.459	.912
.450	-.452	.912	.050	-.721	.897	.050	-.675	.899	.450	-.441	.913
.600	-.480	.911	.100	-.634	.902	.100	-.585	.905	.600	-.445	.913
.800	-.409	.915	.150	-.595	.904	.150	-.516	.909	.800	-.354	.918
.990	.036	.941	.200	-.597	.904	.200	-.538	.907			
			.300	-.543	.907	.300	-.524	.908			
			.350	-.526	.908	.350	-.491	.910			
			.400	-.522	.908	.400	-.483	.911			
			.450	-.481	.911	.450	-.493	.910			
			.500	-.535	.908	.500	-.510	.909			
			.550	-.536	.908	.550	-.507	.909			
			.600	-.495	.910	.600	-.518	.909			
			.650	-.527	.908	.700	-.436	.913			
			.700	-.510	.909	.800	-.350	.919			
			.800	-.381	.917	.900	-.089	.934			
			.900	-.123	.932	.950	.010	.940			
			.950	-.004	.939	.990	.066	.943			
			.990	.082	.944						
					LOWER SURFACE						
.100	-.515	.909	.025	-.307	.921	.025	-.289	.922	.100	-.655	.900
.300	-.490	.910	.050	-.600	.904	.050	-.551	.904	.300	-.465	.912
.600	-.290	.922	.100	-.581	.905	.100	-.557	.906	.600	-.261	.924
.800	.218	.952	.200	-.524	.908	.200	-.512	.909	.800	.240	.954
			.300	-.505	.909	.300	-.481	.911			
			.400	-.476	.911	.400	-.480	.911			
			.500	-.464	.912	.500	-.380	.917			
			.600	-.224	.926	.600	-.223	.926			
			.700	.048	.942	.700	.037	.942			
			.800	.252	.954	.800	.271	.955			
			.900	.333	.959	.900	.304	.957			
			.950	.319	.958	.950	.327	.959			
			1.000	.106	.946						
CN=				.2304			.2139				
CM=				-.1076			-.1019				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\alpha = -1.38^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.964	.888	0.000	1.011	.999	0.000	.070	.943	.050	-.780	.893
.150	-.659	.900	.012	-.292	.922	.012	-.333	.920	.150	-.570	.906
.300	-.556	.906	.025	-.704	.898	.025	-.554	.906	.300	-.494	.910
.450	-.463	.912	.050	-.820	.891	.050	-.759	.894	.450	-.454	.912
.600	-.388	.910	.100	-.704	.898	.100	-.632	.902	.600	-.460	.912
.800	-.404	.915	.150	-.657	.900	.150	-.570	.906	.800	-.360	.918
.990	.040	.942	.200	-.627	.902	.200	-.571	.905			
			.250	-.574	.905	.300	-.564	.906			
			.350	-.550	.907	.350	-.522	.908			
			.400	-.548	.907	.400	-.510	.909			
			.450	-.498	.910	.450	-.518	.909			
			.500	-.551	.907	.500	-.526	.908			
			.550	-.548	.907	.550	-.519	.909			
			.600	-.511	.909	.600	-.531	.908			
			.650	-.546	.907	.700	-.451	.913			
			.700	-.504	.909	.800	-.350	.919			
			.800	-.381	.917	.900	-.102	.933			
			.900	-.140	.931	.950	-.000	.939			
			.950	-.009	.939	.990	.048	.947			
			.990	.079	.944						
					LOWER SURFACE						
.100	-.488	.910	.025	-.234	.925	.025	-.154	.930	.100	-.574	.905
.300	-.460	.912	.050	-.472	.911	.050	-.520	.908	.300	-.472	.911
.600	-.285	.922	.100	-.484	.911	.100	-.524	.908	.600	-.265	.924
.800	.225	.953	.200	-.466	.912	.200	-.466	.912	.800	.245	.954
			.300	-.477	.911	.300	-.468	.912			
			.400	-.458	.912	.400	-.455	.912			
			.500	-.446	.913	.500	-.382	.917			
			.600	-.217	.926	.600	-.721	.926			
			.700	.052	.942	.700	.045	.942			
			.800	.264	.955	.800	.273	.956			
			.900	.347	.960	.900	.296	.957			
			.950	.320	.958	.950	.327	.959			
			1.000	.101	.945						
CN=				.2866			.2614				
CM=				-.1079			-.1017				

(a) M = 0.30. Continued.

$\alpha = -0.87^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.017	.879	0.000	1.005	.999	0.000	.073	.944	.050	-.879	.888
.150	-.726	.897	.012	-.417	.915	.012	-.494	.910	.150	-.599	.904
.300	-.557	.906	.025	-.792	.893	.025	-.649	.901	.300	-.530	.908
.450	-.469	.912	.050	-.937	.884	.050	-.844	.890	.450	-.470	.912
.600	-.494	.910	.100	-.774	.894	.100	-.678	.899	.600	-.460	.912
.800	-.413	.915	.150	-.706	.898	.150	-.630	.902	.800	-.353	.919
.990	.047	.942	.200	-.675	.900	.200	-.616	.903			
			.300	-.610	.903	.300	-.582	.905			
			.350	-.576	.905	.350	-.533	.908			
			.400	-.557	.907	.400	-.531	.908			
			.450	-.518	.909	.450	-.529	.908			
			.500	-.568	.906	.500	-.552	.907			
			.550	-.566	.906	.550	-.531	.908			
			.600	-.514	.909	.600	-.534	.908			
			.650	-.548	.907	.700	-.452	.913			
			.700	-.518	.909	.800	-.346	.919			
			.800	-.380	.917	.900	-.089	.934			
			.900	-.133	.932	.950	.003	.940			
			.950	.002	.940	.990	.045	.942			
			.990	.080	.944						
					LOWER SURFACE						
.100	-.391	.916	.025	-.141	.931	.025	-.077	.935	.100	-.523	.909
.300	-.433	.914	.050	-.395	.916	.050	-.431	.914	.300	-.429	.914
.600	-.272	.923	.100	-.420	.915	.100	-.432	.914	.600	-.253	.925
.800	.232	.953	.200	-.437	.914	.200	-.421	.915	.800	.245	.954
			.300	-.446	.913	.300	-.434	.914			
			.400	-.429	.914	.400	-.442	.913			
			.500	-.427	.914	.500	-.359	.918			
			.600	-.202	.928	.600	-.214	.927			
			.700	.060	.943	.700	.040	.942			
			.800	.271	.956	.800	.273	.956			
			.900	.351	.960	.900	.305	.958			
			.950	.323	.959	.950	.330	.959			
			1.000	.099	.945						
CN=				.3356			.3073				
CM=				-.1071			-.0978				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\alpha = -0.32^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.062	.877	0.000	.994	.998	0.000	.061	.943	.050	-.920	.885
.150	-.745	.896	.012	-.524	.909	.012	-.601	.904	.150	-.664	.900
.300	-.601	.904	.025	-.931	.885	.025	-.768	.894	.300	-.554	.907
.450	-.431	.911	.050	-1.008	.880	.050	-.978	.882	.450	-.482	.911
.600	-.494	.910	.100	-.817	.891	.100	-.757	.895	.600	-.477	.911
.800	-.406	.916	.150	-.739	.896	.150	-.637	.902	.800	-.350	.919
.990	.046	.942	.200	-.697	.898	.200	-.667	.900			
			.300	-.619	.903	.300	-.594	.905			
			.350	-.602	.904	.350	-.565	.906			
			.400	-.570	.906	.400	-.536	.908			
			.450	-.531	.908	.450	-.559	.907			
			.500	-.577	.906	.500	-.560	.907			
			.550	-.572	.906	.550	-.552	.907			
			.600	-.534	.908	.600	-.536	.908			
			.650	-.556	.907	.700	-.463	.912			
			.700	-.524	.909	.800	-.349	.919			
			.800	-.386	.917	.900	-.099	.934			
			.900	-.119	.933	.950	-.005	.939			
			.550	-.000	.940	.990	.027	.941			
			.590	.080	.944						
					LOWER SURFACE						
.100	-.380	.917	.025	-.029	.938	.025	.029	.941	.100	-.500	.910
.300	-.417	.915	.050	-.322	.921	.050	-.393	.916	.300	-.415	.915
.600	-.261	.924	.100	-.358	.918	.100	-.383	.917	.600	-.253	.925
.800	.242	.954	.200	-.381	.917	.200	-.395	.916	.800	.228	.953
			.300	-.417	.915	.300	-.413	.915			
			.400	-.408	.916	.400	-.427	.914			
			.500	-.412	.915	.500	-.355	.919			
			.600	-.193	.928	.600	-.220	.927			
			.700	.081	.944	.700	.058	.943			
			.800	.271	.956	.800	.278	.956			
			.900	.347	.960	.900	.298	.957			
			.550	.329	.959	.550	.328	.959			
			1.000	.094	.945						
CN=				.3777			.3511				
CM=				-.1063			-.0972				

(a) M = 0.30. Continued.

$\alpha = 0.22^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.163	.871	0.000	.974	.997	0.000	.083	.944	.050	-1.095	.875
.150	-.773	.894	.012	-.690	.899	.012	-.730	.896	.150	-.695	.898
.300	-.623	.903	.025	-1.077	.876	.025	-.879	.887	.300	-.573	.906
.450	-.509	.909	.050	-1.107	.874	.050	-1.056	.877	.450	-.487	.911
.600	-.511	.909	.100	-.888	.887	.100	-.797	.892	.600	-.476	.911
.800	-.400	.916	.150	-.793	.893	.150	-.694	.899	.800	-.342	.919
.990	.039	.942	.200	-.741	.896	.200	-.673	.900			
			.300	-.661	.900	.300	-.632	.902			
			.350	-.623	.903	.350	-.570	.906			
			.400	-.590	.905	.400	-.566	.906			
			.450	-.553	.907	.450	-.564	.906			
			.500	-.601	.904	.500	-.563	.906			
			.550	-.589	.905	.550	-.546	.907			
			.600	-.539	.908	.600	-.548	.907			
			.650	-.558	.906	.700	-.452	.913			
			.700	-.527	.908	.800	-.338	.919			
			.800	-.381	.917	.900	-.083	.935			
			.900	-.118	.932	.950	-.013	.939			
			.550	-.003	.939	.990	.021	.941			
			.590	.074	.944						
					LOWER SURFACE						
.100	-.287	.922	.025	.044	.942	.025	.123	.947	.100	-.423	.914
.300	-.395	.916	.050	-.227	.926	.050	-.296	.923	.300	-.386	.917
.600	-.255	.924	.100	-.324	.920	.100	-.335	.920	.600	-.249	.925
.800	.240	.954	.200	-.359	.918	.200	-.332	.920	.800	.246	.954
			.300	-.385	.917	.300	-.381	.917			
			.400	-.389	.916	.400	-.406	.915			
			.500	-.403	.916	.500	-.330	.920			
			.600	-.182	.929	.600	-.193	.928			
			.700	.072	.944	.700	.053	.943			
			.800	.274	.956	.800	.280	.956			
			.900	.354	.960	.900	.300	.957			
			.550	.322	.959	.550	.340	.960			
			1.000	.082	.944						
CN=				.4193			.3955				
CM=				-.1045			-.0947				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\alpha = 1.30^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.343	.860	0.000	.892	.992	0.000	.075	.944	.050	-1.295	.863
.150	-.866	.888	.012	-1.071	.876	.012	-1.032	.878	.150	-.728	.897
.300	-.656	.900	.025	-1.375	.858	.025	-1.153	.871	.300	-.630	.902
.450	-.539	.908	.050	-1.366	.859	.050	-1.253	.866	.450	-.510	.909
.600	-.518	.909	.100	-1.043	.878	.100	-.910	.886	.600	-.490	.911
.800	-.397	.916	.150	-.882	.887	.150	-.785	.893	.800	-.344	.919
.990	.046	.942	.200	-.835	.890	.200	-.776	.894			
			.300	-.712	.897	.300	-.686	.899			
			.350	-.669	.900	.350	-.636	.902			
			.400	-.645	.901	.400	-.601	.904			
			.450	-.586	.905	.450	-.601	.904			
			.500	-.619	.903	.500	-.602	.904			
			.550	-.610	.903	.550	-.581	.905			
			.600	-.555	.907	.600	-.572	.906			
			.650	-.567	.906	.700	-.455	.913			
			.700	-.538	.908	.800	-.341	.919			
			.800	-.371	.918	.900	-.078	.935			
			.900	-.119	.933	.950	-.040	.937			
			.950	.004	.940	.990	-.001	.940			
			.990	.061	.943						
					LOWER SURFACE						
.100	-.201	.928	.025	.189	.951	.025	.304	.958	.100	-.304	.922
.300	-.347	.919	.050	-.103	.933	.050	-.156	.930	.300	-.355	.919
.600	-.237	.926	.100	-.209	.927	.100	-.236	.926	.600	-.237	.926
.800	.249	.954	.200	-.289	.922	.200	-.289	.922	.800	.241	.954
			.300	-.337	.920	.300	-.333	.920			
			.400	-.345	.919	.400	-.366	.918			
			.500	-.377	.917	.500	-.320	.921			
			.600	-.158	.930	.600	-.186	.929			
			.700	.090	.945	.700	.056	.943			
			.800	.287	.957	.800	.281	.956			
			.900	.360	.961	.900	.299	.957			
			.950	.328	.959	.950	.340	.960			
			1.000	.073	.944						
CN=				.5177			.4847				
CM=				-.1013			-.0909				

(a) M = 0.30. Continued.

$\alpha = 2.38^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.587	.846	0.000	.815	.908	0.000	.090	.945	.050	-1.427	.855
.150	-.957	.883	.012	-1.344	.860	.012	-1.430	.855	.150	-.818	.891
.300	-.742	.896	.025	-1.656	.841	.025	-1.449	.854	.300	-.637	.902
.450	-.563	.906	.050	-1.529	.849	.050	-1.436	.855	.450	-.526	.908
.600	-.544	.907	.100	-1.164	.871	.100	-1.065	.876	.600	-.485	.911
.800	-.407	.915	.150	-.972	.882	.150	-.868	.888	.800	-.336	.920
.990	.024	.941	.200	-.900	.886	.200	-.836	.890			
			.300	-.761	.894	.300	-.721	.897			
			.350	-.717	.897	.350	-.650	.901			
			.400	-.674	.900	.400	-.637	.902			
			.450	-.616	.903	.450	-.622	.903			
			.500	-.651	.901	.500	-.628	.902			
			.550	-.636	.902	.550	-.588	.905			
			.600	-.578	.905	.600	-.574	.905			
			.650	-.591	.904	.700	-.458	.912			
			.700	-.548	.907	.800	-.326	.920			
			.800	-.385	.917	.900	-.086	.934			
			.900	-.122	.932	.950	-.037	.937			
			.950	-.004	.939	.990	-.026	.938			
			.990	.049	.942						
					LOWER SURFACE						
.100	-.119	.932	.025	.308	.958	.025	.472	.967	.100	-.250	.925
.300	-.305	.921	.050	.052	.943	.050	-.018	.938	.300	-.311	.921
.600	-.225	.926	.100	-.104	.933	.100	-.153	.930	.600	-.232	.926
.800	.246	.954	.200	-.216	.927	.200	-.229	.926	.800	.253	.954
			.300	-.281	.923	.300	-.281	.923			
			.400	-.322	.920	.400	-.296	.922			
			.500	-.352	.919	.500	-.300	.922			
			.600	-.149	.931	.600	-.179	.929			
			.700	.091	.945	.700	.071	.944			
			.800	.289	.957	.800	.287	.956			
			.900	.358	.961	.900	.321	.958			
			.950	.326	.959	.950	.341	.960			
			1.000	.053	.943						
CN=				.6014			.5697				
CM=				-.0992			-.0855				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\alpha = 3.46^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.910	.832	C.000	.698	.981	0.000	.060	.943	.050	-1.668	.841
.150	-1.031	.878	.012	-1.651	.842	.012	-1.720	.837	.150	-.908	.886
.300	-.776	.893	.025	-2.000	.821	.025	-1.687	.839	.300	-.706	.898
.450	-.590	.904	.050	-1.787	.834	.050	-1.647	.842	.450	-.548	.907
.600	-.548	.907	.100	-1.278	.864	.100	-1.206	.868	.600	-.498	.910
.800	-.394	.916	.150	-1.070	.876	.150	-.978	.881	.800	-.307	.921
.990	.035	.941	.200	-.977	.882	.200	-.904	.886			
			.300	-.813	.891	.300	-.784	.893			
			.350	-.761	.894	.350	-.727	.896			
			.400	-.708	.897	.400	-.674	.899			
			.450	-.646	.901	.450	-.662	.900			
			.500	-.670	.900	.500	-.648	.901			
			.550	-.659	.900	.550	-.621	.903			
			.600	-.595	.904	.600	-.593	.904			
			.650	-.602	.904	.700	-.479	.911			
			.700	-.553	.907	.800	-.307	.921			
			.800	-.379	.917	.900	-.103	.933			
			.900	-.096	.934	.950	-.061	.936			
			.950	-.008	.939	.990	-.059	.936			
			.990	.046	.942						
					LOWER SURFACE						
.100	.012	.940	.025	.441	.966	.025	.569	.973	.100	-.147	.931
.300	-.260	.924	.050	.178	.950	.050	.120	.946	.300	-.300	.922
.600	-.205	.927	.100	-.001	.939	.100	-.026	.938	.600	-.214	.927
.800	.267	.955	.200	-.155	.930	.200	-.181	.929	.800	.226	.953
			.300	-.232	.926	.300	-.257	.924			
			.400	-.267	.924	.400	-.269	.923			
			.500	-.309	.921	.500	-.285	.923			
			.600	-.133	.931	.600	-.190	.929			
			.700	.103	.945	.700	.066	.943			
			.800	.297	.957	.800	.285	.956			
			.900	.368	.961	.900	.301	.957			
			.950	.329	.959	.950	.336	.959			
			1.000	.039	.942						
CN=				.6909			.6536				
CM=				-.0953			-.0812				

(a) M = 0.30. Continued.

$\alpha = 4.54^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.583	.822	C.000	.518	.970	C.000	.062	.943	.050	-1.879	.828
.150	-1.126	.873	.012	-2.049	.818	.012	-2.110	.814	.150	-.979	.881
.300	-.801	.892	.025	-2.330	.801	.025	-1.940	.825	.300	-.735	.896
.450	-.618	.903	.050	-2.018	.820	.050	-1.910	.826	.450	-.569	.906
.600	-.555	.907	.100	-1.400	.856	.100	-1.300	.862	.600	-.510	.909
.800	-.390	.917	.150	-1.184	.869	.150	-1.059	.877	.800	-.311	.921
.990	.029	.941	.200	-1.079	.876	.200	-.985	.881			
			.300	-.874	.888	.300	-.839	.890			
			.350	-.791	.893	.350	-.753	.895			
			.400	-.743	.895	.400	-.708	.898			
			.450	-.675	.899	.450	-.698	.898			
			.500	-.716	.897	.500	-.677	.899			
			.550	-.671	.900	.550	-.631	.902			
			.600	-.616	.903	.600	-.603	.904			
			.650	-.608	.903	.700	-.470	.912			
			.700	-.550	.907	.800	-.310	.921			
			.800	-.357	.918	.900	-.102	.933			
			.900	-.098	.934	.950	-.080	.935			
			.950	-.012	.939	.990	-.071	.935			
			.990	.032	.941						
					LOWER SURFACE						
.100	.093	.945	.025	.554	.972	.025	.663	.979	.100	-.053	.936
.300	-.208	.927	.050	.312	.958	.050	.253	.954	.300	-.241	.925
.600	-.191	.928	.100	.086	.945	.100	.049	.942	.600	-.214	.927
.800	.265	.955	.200	-.072	.935	.200	-.110	.933	.800	.232	.953
			.300	-.173	.929	.300	-.192	.928			
			.400	-.230	.926	.400	-.229	.926			
			.500	-.284	.923	.500	-.259	.924			
			.600	-.116	.933	.600	-.152	.930			
			.700	.117	.946	.700	.076	.944			
			.800	.303	.957	.800	.292	.957			
			.900	.372	.961	.900	.309	.958			
			.950	.325	.959	.950	.336	.959			
			1.000	.044	.942						
CN=				.7818			.7417				
CM=				-.0905			-.0779				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Continued.

$\alpha = 6.70^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.524	.790	0.000	.188	.951	0.000	.087	.945	.050	-2.456	.794
.150	-1.273	.864	.012	-2.875	.770	.012	-2.853	.771	.150	-1.148	.872
.300	-.881	.887	.025	-3.033	.760	.025	-2.654	.783	.300	-.808	.892
.450	-.658	.901	.050	-2.488	.792	.050	-2.422	.796	.450	-.604	.904
.600	-.563	.906	.100	-1.675	.841	.100	-1.603	.845	.600	-.511	.909
.800	-.350	.919	.150	-1.361	.859	.150	-1.262	.865	.800	-.324	.920
.990	.006	.940	.200	-1.200	.869	.200	-1.128	.873			
			.300	-.979	.882	.300	-.928	.885			
			.350	-.871	.888	.350	-.836	.890			
			.400	-.817	.891	.400	-.766	.894			
			.450	-.726	.897	.450	-.724	.897			
			.500	-.744	.896	.500	-.707	.898			
			.550	-.708	.898	.550	-.657	.901			
			.600	-.628	.902	.600	-.614	.903			
			.650	-.609	.904	.700	-.449	.913			
			.700	-.548	.907	.800	-.265	.924			
			.800	-.336	.920	.900	-.117	.933			
			.900	-.079	.935	.950	-.111	.933			
			.550	-.018	.938	.990	-.130	.932			
			.950	.000	.940						
					LOWER SURFACE						
.100	.270	.955	.025	.765	.985	.025	.824	.988	.100	.138	.948
.300	-.115	.933	.050	.518	.970	.050	.452	.966	.300	-.169	.930
.600	-.145	.931	.100	.256	.955	.100	.220	.953	.600	-.171	.929
.800	.289	.957	.200	.052	.943	.200	.006	.940	.800	.232	.953
			.300	-.050	.937	.300	-.108	.933			
			.400	-.151	.931	.400	-.156	.930			
			.500	-.226	.926	.500	-.193	.928			
			.600	-.071	.935	.600	-.115	.933			
			.700	.148	.948	.700	.090	.945			
			.800	.328	.959	.800	.305	.958			
			.900	.379	.962	.900	.315	.959			
			.550	.337	.959	.950	.339	.960			
			1.000	.006	.940						
CN=				.9553			.9081				
CM=				-.0828			-.0670				

(a) M = 0.30. Continued.

$\alpha = 8.85^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.754	.777	0.000	-.343	.919	0.000	.095	.945	.050	-3.024	.761
.150	-1.469	.853	.012	-3.877	.711	.012	-3.814	.714	.150	-1.281	.864
.300	-.569	.882	.025	-3.891	.710	.025	-3.241	.748	.300	-.872	.888
.450	-.703	.898	.050	-3.068	.758	.050	-2.896	.769	.450	-.627	.903
.600	-.589	.905	.100	-1.982	.823	.100	-1.806	.833	.600	-.545	.907
.800	-.326	.920	.150	-1.584	.846	.150	-1.440	.855	.800	-.352	.919
.990	-.026	.938	.200	-1.369	.859	.200	-1.287	.864			
			.300	-1.065	.877	.300	-1.020	.879			
			.350	-.959	.883	.350	-.903	.886			
			.400	-.879	.888	.400	-.830	.891			
			.450	-.780	.894	.450	-.782	.893			
			.500	-.784	.893	.500	-.741	.896			
			.550	-.725	.897	.550	-.672	.900			
			.600	-.660	.901	.600	-.624	.903			
			.650	-.606	.904	.700	-.428	.914			
			.700	-.530	.908	.800	-.260	.924			
			.800	-.296	.922	.900	-.136	.932			
			.900	-.099	.934	.950	-.140	.931			
			.550	-.059	.936	.990	-.139	.931			
			.950	-.048	.937						
					LOWER SURFACE						
.100	.422	.965	.025	.864	.991	.025	.957	.996	.100	.297	.957
.300	-.025	.938	.050	.666	.979	.050	.622	.976	.300	-.094	.935
.600	-.115	.933	.100	.416	.964	.100	.385	.962	.600	-.153	.931
.800	.290	.957	.200	.156	.949	.200	.135	.948	.800	.251	.954
			.300	.024	.941	.300	-.014	.939			
			.400	-.079	.935	.400	-.090	.934			
			.500	-.175	.929	.500	-.132	.932			
			.600	-.030	.938	.600	-.077	.935			
			.700	.154	.949	.700	.120	.947			
			.800	.325	.959	.800	.310	.958			
			.900	.384	.962	.900	.319	.958			
			.550	.323	.959	.950	.334	.959			
			1.000	-.032	.938						
CN=				1.1279			1.0713				
CM=				-.0690			-.0577				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.30. Concluded.

$\alpha = 10.98^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.130	.753	0.000	-.781	.894	0.000	.087	.945	.050	-3.789	.717
.150	-1.618	.845	.012	-4.763	.660	.012	-4.786	.658	.150	-1.471	.853
.300	-1.040	.879	.025	-4.690	.664	.025	-4.175	.694	.300	-.915	.886
.450	-.722	.897	.050	-3.407	.739	.050	-3.329	.744	.450	-.667	.901
.600	-.573	.906	.100	-2.247	.808	.100	-2.091	.817	.600	-.572	.906
.800	-.247	.925	.150	-1.784	.835	.150	-1.621	.845	.800	-.397	.917
.990	-.049	.937	.200	-1.497	.852	.200	-1.339	.858			
			.300	-1.142	.873	.300	-1.104	.875			
			.350	-1.012	.880	.350	-.969	.883			
			.400	-.923	.886	.400	-.879	.888			
			.450	-.820	.892	.450	-.816	.892			
			.500	-.796	.893	.500	-.764	.895			
			.550	-.739	.896	.550	-.694	.899			
			.600	-.651	.902	.600	-.623	.903			
			.650	-.589	.905	.700	-.422	.915			
			.700	-.501	.910	.800	-.231	.926			
			.800	-.259	.925	.900	-.165	.930			
			.900	-.107	.934	.950	-.162	.930			
			.950	-.100	.934	.990	-.169	.930			
			.990	-.068	.936						
					LOWER SURFACE						
.100	.532	.971	.025	.935	.995	.025	1.006	.999	.100	.434	.965
.300	.067	.944	.050	.818	.988	.050	.770	.985	.300	-.004	.940
.600	-.035	.935	.100	.526	.971	.100	.522	.971	.600	-.121	.933
.800	.305	.958	.200	.268	.956	.200	.244	.954	.800	.266	.955
			.300	.114	.947	.300	.090	.945			
			.400	-.016	.939	.400	-.022	.939			
			.500	-.121	.933	.500	-.082	.935			
			.600	.003	.940	.600	-.047	.937			
			.700	.171	.950	.700	.138	.948			
			.800	.346	.960	.800	.313	.958			
			.900	.391	.963	.900	.318	.959			
			.950	.325	.959	.950	.326	.959			
			1.000	-.073	.936						
CN=				1.2707			1.2286				
CM=				-.0591			-.0463				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50

$\alpha = -4.27^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.404	.782	C.000	1.020	.993	0.000	.067	.852	.050	-.310	.796
.150	-.466	.773	.012	.336	.892	.012	.316	.885	.150	-.374	.787
.300	-.460	.774	.025	-.050	.835	.025	-.012	.841	.300	-.429	.779
.450	-.397	.783	.050	-.328	.794	.050	-.289	.800	.450	-.421	.780
.600	-.464	.774	.100	-.394	.784	.100	-.334	.793	.600	-.454	.775
.800	-.407	.782	.150	-.438	.777	.150	-.350	.790	.900	-.332	.793
.990	.059	.851	.200	-.458	.775	.200	-.425	.779			
			.300	-.467	.773	.300	-.441	.777			
			.350	-.451	.776	.350	-.437	.778			
			.400	-.448	.776	.400	-.422	.780			
			.450	-.443	.777	.450	-.466	.773			
			.500	-.511	.767	.500	-.493	.769			
			.550	-.514	.766	.550	-.499	.768			
			.600	-.480	.771	.600	-.507	.767			
			.650	-.526	.764	.700	-.431	.778			
			.700	-.511	.767	.800	-.335	.793			
			.800	-.372	.787	.900	-.066	.832			
			.900	-.099	.828	.950	.016	.845			
			.950	.026	.846	.990	.065	.852			
			.990	.099	.857						
					LOWER SURFACE						
.100	-.876	.713	.025	-.828	.720	.025	-.815	.722	.100	-1.084	.682
.300	-.670	.743	.050	-1.103	.679	.050	-1.206	.664	.300	-.619	.751
.600	-.332	.793	.100	-.911	.707	.100	-.954	.701	.600	-.307	.797
.800	.133	.862	.200	-.765	.729	.200	-.750	.731	.800	.155	.865
			.300	-.715	.736	.300	-.689	.740			
			.400	-.634	.748	.400	-.636	.748			
			.500	-.585	.756	.500	-.517	.766			
			.600	-.289	.799	.600	-.302	.798			
			.700	.038	.848	.700	-.007	.841			
			.800	.185	.870	.800	.215	.874			
			.900	.272	.883	.900	.266	.882			
			.950	.296	.886	.950	.297	.886			
			1.000	.129	.861						
CN=				-.0017			-.0372				
CM=				-.1046			-.1044				

(b) M = 0.50. Continued.

$\alpha = -3.04^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.623	.752	C.000	1.050	.998	0.000	.076	.855	.050	-.529	.766
.150	-.548	.763	.012	.102	.858	.012	.111	.860	.150	-.499	.770
.300	-.527	.766	.025	-.312	.798	.025	-.209	.813	.300	-.470	.774
.450	-.435	.779	.050	-.570	.760	.050	-.512	.768	.450	-.449	.777
.600	-.485	.772	.100	-.527	.766	.100	-.482	.772	.600	-.475	.774
.800	-.413	.783	.150	-.546	.763	.150	-.470	.774	.800	-.349	.792
.990	.057	.852	.200	-.565	.760	.200	-.533	.765			
			.300	-.519	.767	.300	-.517	.767			
			.350	-.515	.768	.350	-.495	.770			
			.400	-.510	.768	.400	-.488	.772			
			.450	-.487	.772	.450	-.504	.769			
			.500	-.543	.763	.500	-.533	.765			
			.550	-.548	.763	.550	-.529	.765			
			.600	-.510	.768	.600	-.535	.765			
			.650	-.548	.763	.700	-.454	.777			
			.700	-.533	.765	.800	-.339	.794			
			.800	-.383	.787	.900	-.074	.833			
			.900	-.111	.827	.950	.011	.845			
			.950	.018	.846	.990	.052	.851			
			.990	.099	.858						
					LOWER SURFACE						
.100	-.727	.736	.025	-.555	.762	.025	-.541	.764	.100	-.903	.710
.300	-.602	.755	.050	-.808	.724	.050	-.919	.708	.300	-.581	.758
.600	-.322	.796	.100	-.789	.727	.100	-.787	.728	.600	-.303	.799
.800	.189	.871	.200	-.670	.745	.200	-.681	.743	.800	.198	.872
			.300	-.636	.750	.300	-.631	.751			
			.400	-.587	.757	.400	-.592	.756			
			.500	-.553	.762	.500	-.489	.771			
			.600	-.262	.805	.600	-.286	.801			
			.700	.053	.851	.700	.008	.844			
			.800	.237	.878	.800	.257	.881			
			.900	.321	.891	.900	.299	.887			
			.950	.313	.890	.950	.325	.891			
			1.000	.120	.861						
CN=				.1174			.0889				
CM=				-.1107			-.1055				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\alpha = -2.40^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.734	.735	0.000	1.045	.997	0.000	.071	.854	.050	-.610	.754
.150	-.629	.751	.012	-.003	.843	.012	-.062	.834	.150	-.524	.766
.300	-.566	.760	.025	-.436	.779	.025	-.350	.792	.300	-.502	.770
.450	-.465	.775	.050	-.669	.745	.050	-.604	.754	.450	-.474	.774
.600	-.503	.769	.100	-.636	.750	.100	-.560	.761	.600	-.482	.772
.800	-.425	.781	.150	-.601	.755	.150	-.510	.768	.800	-.362	.790
.990	.055	.851	.200	-.629	.751	.200	-.537	.764			
			.300	-.560	.761	.300	-.549	.763			
			.350	-.549	.763	.350	-.525	.766			
			.400	-.538	.764	.400	-.514	.768			
			.450	-.518	.767	.450	-.531	.765			
			.500	-.576	.759	.500	-.549	.763			
			.550	-.574	.759	.550	-.551	.762			
			.600	-.529	.766	.600	-.548	.763			
			.650	-.566	.760	.700	-.460	.776			
			.700	-.542	.764	.800	-.344	.793			
			.800	-.393	.786	.900	-.074	.832			
			.900	-.115	.827	.950	-.006	.847			
			.950	.016	.846	.990	.039	.849			
			.990	.093	.857						
					LOWER SURFACE						
.100	-.645	.748	.025	-.438	.779	.025	-.423	.781	.100	-.790	.727
.300	-.566	.760	.050	-.751	.733	.050	-.782	.728	.300	-.548	.763
.600	-.309	.798	.100	-.687	.742	.100	-.713	.738	.600	-.303	.799
.800	.197	.872	.200	-.623	.752	.200	-.629	.751	.800	.216	.875
			.300	-.609	.754	.300	-.583	.758			
			.400	-.567	.760	.400	-.567	.760			
			.500	-.534	.765	.500	-.461	.776			
			.600	-.255	.806	.600	-.281	.802			
			.700	.041	.849	.700	.021	.846			
			.800	.250	.880	.800	.262	.882			
			.900	.333	.892	.900	.311	.889			
			.950	.321	.891	.950	.330	.892			
			1.000	.108	.859						
CN=				.1821			.1494				
CM=				-.1109			-.1054				

(b) M = 0.50. Continued.

$\alpha = -1.82^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.841	.720	0.000	1.058	.999	0.000	.064	.853	.050	-.735	.735
.150	-.666	.745	.012	-.110	.827	.012	-.150	.821	.150	-.580	.758
.300	-.587	.757	.025	-.558	.761	.025	-.497	.770	.300	-.533	.765
.450	-.478	.773	.050	-.800	.726	.050	-.702	.740	.450	-.488	.772
.600	-.511	.768	.100	-.704	.740	.100	-.677	.744	.600	-.492	.771
.800	-.424	.781	.150	-.665	.746	.150	-.576	.759	.800	-.356	.791
.990	.045	.850	.200	-.649	.748	.200	-.616	.753			
			.300	-.606	.754	.300	-.586	.757			
			.350	-.576	.759	.350	-.559	.761			
			.400	-.570	.760	.400	-.533	.765			
			.450	-.530	.765	.450	-.550	.763			
			.500	-.596	.756	.500	-.569	.760			
			.550	-.589	.757	.550	-.560	.761			
			.600	-.546	.763	.600	-.557	.761			
			.650	-.574	.759	.700	-.461	.776			
			.700	-.546	.763	.800	-.356	.791			
			.800	-.388	.786	.900	-.078	.832			
			.900	-.116	.826	.950	-.003	.843			
			.950	.019	.846	.990	.026	.847			
			.990	.091	.857						
					LOWER SURFACE						
.100	-.582	.758	.025	-.341	.793	.025	-.267	.804	.100	-.732	.736
.300	-.542	.764	.050	-.634	.750	.050	-.698	.741	.300	-.528	.766
.600	-.307	.798	.100	-.605	.754	.100	-.625	.751	.600	-.299	.799
.800	.221	.876	.200	-.572	.759	.200	-.566	.760	.800	.231	.877
			.300	-.575	.759	.300	-.570	.760			
			.400	-.544	.763	.400	-.541	.764			
			.500	-.520	.767	.500	-.451	.777			
			.600	-.245	.807	.600	-.271	.804			
			.700	.064	.853	.700	.020	.846			
			.800	.266	.883	.800	.275	.884			
			.900	.346	.894	.900	.313	.889			
			.950	.326	.891	.950	.338	.893			
			1.000	.102	.859						
CN=				.2405			.2132				
CM=				-.1115			-.1039				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\alpha = -1.19^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.963	.702	0.000	1.052	.998	0.000	.084	.856	.050	-.899	.711
.150	-.713	.739	.012	-.315	.757	.012	-.271	.804	.150	-.632	.759
.300	-.604	.755	.025	-.708	.739	.025	-.532	.765	.300	-.534	.761
.450	-.497	.770	.050	-.908	.710	.050	-.819	.723	.450	-.501	.770
.600	-.522	.767	.100	-.782	.728	.100	-.708	.739	.600	-.499	.770
.800	-.421	.782	.150	-.736	.735	.150	-.640	.749	.800	-.363	.790
.990	.045	.850	.200	-.713	.739	.200	-.660	.746			
			.300	-.637	.750	.300	-.620	.752			
			.350	-.612	.754	.350	-.593	.756			
			.400	-.598	.756	.400	-.555	.762			
			.450	-.551	.762	.450	-.582	.758			
			.500	-.616	.753	.500	-.594	.756			
			.550	-.606	.754	.550	-.587	.757			
			.600	-.556	.762	.600	-.576	.759			
			.650	-.582	.758	.700	-.471	.774			
			.700	-.552	.762	.800	-.339	.794			
			.800	-.390	.786	.900	-.087	.831			
			.900	-.112	.827	.950	-.014	.841			
			.950	.013	.845	.990	.016	.846			
			.990	.086	.856						
					LOWER SURFACE						
.100	-.493	.771	.025	-.192	.815	.025	-.093	.830	.100	-.637	.750
.300	-.515	.768	.050	-.511	.768	.050	-.585	.757	.300	-.520	.767
.600	-.304	.799	.100	-.545	.763	.100	-.545	.763	.600	-.301	.799
.800	.224	.876	.200	-.529	.766	.200	-.527	.766	.800	.230	.877
			.300	-.543	.764	.300	-.535	.765			
			.400	-.513	.768	.400	-.532	.765			
			.500	-.511	.768	.500	-.433	.780			
			.600	-.238	.809	.600	-.264	.805			
			.700	.064	.853	.700	.016	.846			
			.800	.259	.882	.800	.271	.883			
			.900	.354	.896	.900	.307	.888			
			.950	.330	.892	.950	.334	.893			
			1.000	.099	.858						
CN=				.2955			.2665				
CM=				-.1098			-.1009				

(b) M = 0.50. Continued.

$\alpha = -0.62^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.043	.690	0.000	1.043	.997	0.000	.082	.856	.050	-.934	.697
.150	-.768	.731	.012	-.429	.780	.012	-.456	.777	.150	-.672	.745
.300	-.639	.750	.025	-.805	.725	.025	-.708	.739	.300	-.590	.757
.450	-.528	.766	.050	-1.025	.693	.050	-.970	.701	.450	-.508	.769
.600	-.532	.765	.100	-.908	.710	.100	-.795	.727	.600	-.501	.770
.800	-.420	.782	.150	-.779	.729	.150	-.677	.744	.800	-.358	.790
.990	.343	.850	.200	-.752	.733	.200	-.708	.739			
			.300	-.666	.746	.300	-.643	.749			
			.350	-.637	.750	.350	-.610	.754			
			.400	-.610	.754	.400	-.578	.758			
			.450	-.574	.759	.450	-.592	.757			
			.500	-.628	.751	.500	-.605	.755			
			.550	-.621	.752	.550	-.589	.757			
			.600	-.570	.760	.600	-.578	.758			
			.650	-.595	.756	.700	-.469	.774			
			.700	-.555	.762	.800	-.350	.792			
			.800	-.397	.785	.900	-.044	.831			
			.900	-.108	.828	.950	-.019	.841			
			.950	.011	.845	.990	.013	.845			
			.990	.070	.854						
					LOWER SURFACE						
.100	-.495	.779	.025	-.123	.825	.025	.004	.844	.100	-.601	.755
.300	-.485	.772	.050	-.464	.775	.050	-.532	.765	.300	-.494	.771
.600	-.298	.800	.100	-.483	.772	.100	-.492	.771	.600	-.293	.800
.800	.231	.877	.200	-.478	.773	.200	-.482	.773	.800	.243	.879
			.300	-.505	.769	.300	-.499	.770			
			.400	-.489	.772	.400	-.498	.770			
			.500	-.489	.772	.500	-.424	.781			
			.600	-.229	.810	.600	-.259	.805			
			.700	.070	.854	.700	.026	.847			
			.800	.265	.882	.800	.275	.884			
			.900	.355	.896	.900	.313	.890			
			.950	.324	.891	.950	.334	.893			
			1.000	.091	.857						
CN=				.3481			.3138				
CM=				-.1088			-.0992				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\alpha = 0.01^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.186	.669	0.000	1.020	.994	0.000	.069	.854	.050	-1.114	.679
.150	-.808	.725	.012	-.567	.760	.012	-.592	.756	.150	-.737	.735
.300	-.673	.744	.025	-1.032	.691	.025	-.397	.711	.300	-.623	.752
.450	-.542	.764	.050	-1.142	.675	.050	-1.086	.684	.450	-.534	.765
.600	-.541	.764	.100	-.546	.704	.100	-.889	.713	.600	-.522	.767
.800	-.417	.782	.150	-.836	.720	.150	-.752	.733	.800	-.363	.790
.990	.040	.845	.200	-.793	.727	.200	-.742	.734			
			.300	-.709	.739	.300	-.684	.743			
			.350	-.671	.745	.350	-.635	.750			
			.400	-.633	.750	.400	-.607	.754			
			.450	-.595	.756	.450	-.618	.752			
			.500	-.638	.749	.500	-.626	.751			
			.550	-.632	.750	.550	-.604	.755			
			.600	-.588	.757	.600	-.599	.757			
			.650	-.597	.756	.700	-.472	.774			
			.700	-.563	.761	.800	-.326	.795			
			.800	-.391	.786	.900	-.048	.830			
			.900	-.102	.828	.950	-.036	.838			
			.950	.013	.845	.990	-.023	.840			
			.990	.070	.854						
					LOWER SURFACE						
.100	-.373	.785	.025	-.032	.839	.025	.062	.853	.100	-.555	.762
.300	-.458	.776	.050	-.318	.797	.050	-.389	.785	.300	-.479	.773
.600	-.281	.802	.100	-.385	.787	.100	-.439	.780	.600	-.291	.801
.800	.236	.878	.200	-.428	.780	.200	-.437	.779	.800	.232	.878
			.300	-.456	.775	.300	-.477	.773			
			.400	-.459	.776	.400	-.493	.772			
			.500	-.473	.774	.500	-.408	.783			
			.600	-.226	.810	.600	-.254	.806			
			.700	.067	.853	.700	.023	.847			
			.800	.273	.884	.800	.274	.884			
			.900	.356	.896	.900	.312	.888			
			.950	.332	.892	.950	.334	.893			
			1.000	.075	.854						
CN=				.4043			.3715				
CM=				-.1057			-.0950				

(b) M = 0.50. Continued.

$\alpha = 0.59^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.294	.653	0.000	1.013	.992	0.000	.060	.853	.050	-1.261	.658
.150	-.879	.714	.012	-.749	.733	.012	-.767	.732	.150	-.750	.733
.300	-.709	.739	.025	-1.212	.665	.025	-.588	.694	.300	-.649	.748
.450	-.560	.761	.050	-1.298	.654	.050	-1.231	.662	.450	-.542	.764
.600	-.550	.762	.100	-1.020	.693	.100	-.947	.704	.600	-.514	.768
.800	-.418	.782	.150	-.986	.713	.150	-.802	.725	.800	-.349	.792
.990	.040	.845	.200	-.842	.719	.200	-.743	.728			
			.300	-.739	.735	.300	-.715	.738			
			.350	-.699	.740	.350	-.666	.745			
			.400	-.662	.746	.400	-.616	.753			
			.450	-.616	.753	.450	-.626	.751			
			.500	-.654	.747	.500	-.631	.750			
			.550	-.642	.749	.550	-.619	.752			
			.600	-.596	.756	.600	-.586	.757			
			.650	-.610	.754	.700	-.474	.774			
			.700	-.562	.761	.800	-.322	.796			
			.800	-.386	.787	.900	-.077	.832			
			.900	-.096	.829	.950	-.049	.838			
			.950	.004	.844	.990	-.028	.839			
			.990	.058	.852						
					LOWER SURFACE						
.100	-.267	.801	.025	.041	.855	.025	.154	.866	.100	-.433	.772
.300	-.432	.780	.050	-.215	.812	.050	-.303	.794	.300	-.452	.777
.600	-.284	.802	.100	-.337	.794	.100	-.377	.788	.600	-.285	.801
.800	.242	.879	.200	-.398	.785	.200	-.417	.782	.900	.237	.878
			.300	-.444	.778	.300	-.448	.777			
			.400	-.434	.780	.400	-.463	.775			
			.500	-.465	.775	.500	-.391	.786			
			.600	-.213	.812	.600	-.244	.807			
			.700	.075	.854	.700	.034	.848			
			.800	.232	.885	.800	.261	.885			
			.900	.357	.896	.900	.313	.885			
			.950	.336	.893	.950	.333	.892			
			1.000	.067	.853						
CN=				.4545			.4176				
CM=				-.1046			-.0920				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\alpha = 1.80^{o}$

STATION .1592 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.572	.612	0.000	.945	.982	0.000	.077	.855	.050	-1.523	.620
.150	-.966	.701	.012	-1.075	.685	.012	-1.103	.681	.150	-.837	.720
.300	-.758	.732	.025	-1.574	.612	.025	-1.317	.650	.300	-.695	.741
.450	-.596	.756	.050	-1.606	.607	.050	-1.459	.629	.450	-.567	.760
.600	-.568	.760	.100	-1.213	.665	.100	-1.096	.682	.600	-.528	.766
.800	-.407	.784	.150	-1.017	.694	.150	-.891	.712	.800	-.348	.792
.990	.034	.848	.200	-.926	.707	.200	-.883	.714			
			.300	-.799	.726	.300	-.786	.728			
			.350	-.745	.734	.350	-.724	.737			
			.400	-.703	.740	.400	-.663	.746			
			.450	-.662	.746	.450	-.666	.746			
			.500	-.693	.742	.500	-.659	.747			
			.550	-.670	.745	.550	-.637	.750			
			.600	-.627	.751	.600	-.606	.754			
			.650	-.614	.753	.700	-.471	.774			
			.700	-.564	.761	.800	-.307	.798			
			.800	-.372	.789	.900	-.097	.829			
			.900	-.097	.829	.950	-.051	.836			
			.950	-.003	.843	.990	-.053	.836			
			.990	.045	.850						
					LOWER SURFACE						
.100	-.208	.813	.025	.220	.876	.025	.333	.892	.100	-.363	.790
.300	-.374	.789	.050	-.081	.832	.050	-.128	.825	.300	-.398	.785
.600	-.266	.804	.100	-.196	.815	.100	-.224	.811	.600	-.275	.803
.800	.247	.880	.200	-.307	.798	.200	-.321	.796	.800	.244	.879
			.300	-.381	.787	.300	-.383	.787			
			.400	-.397	.785	.400	-.427	.781			
			.500	-.433	.780	.500	-.370	.785			
			.600	-.200	.814	.600	-.221	.811			
			.700	.086	.856	.700	.042	.850			
			.800	.285	.885	.800	.282	.885			
			.900	.369	.898	.900	.316	.890			
			.950	.332	.892	.950	.340	.894			
			1.000	.041	.850						
CN=				.5630			.5263				
CM=				-.0986			-.0870				

(b) M = 0.50. Continued.

$\alpha = 3.00^{o}$

STATION .1592 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.841	.573	0.000	.854	.969	0.000	.077	.855	.050	-1.828	.576
.150	-1.055	.688	.012	-1.448	.630	.012	-1.453	.630	.150	-.957	.703
.300	-.801	.726	.025	-1.927	.560	.025	-1.621	.605	.300	-.737	.735
.450	-.623	.752	.050	-1.951	.556	.050	-1.770	.583	.450	-.586	.757
.600	-.573	.759	.100	-1.328	.648	.100	-1.270	.657	.600	-.530	.765
.800	-.396	.785	.150	-1.140	.676	.150	-1.018	.694	.800	-.326	.796
.990	.021	.847	.200	-1.047	.689	.200	-.975	.700			
			.300	-.863	.716	.300	-.839	.720			
			.350	-.801	.726	.350	-.766	.731			
			.400	-.739	.735	.400	-.715	.738			
			.450	-.699	.741	.450	-.696	.741			
			.500	-.717	.738	.500	-.679	.744			
			.550	-.688	.742	.550	-.649	.748			
			.600	-.628	.751	.600	-.612	.753			
			.650	-.624	.752	.700	-.464	.775			
			.700	-.562	.761	.800	-.304	.799			
			.800	-.357	.791	.900	-.102	.828			
			.900	-.084	.831	.950	-.085	.831			
			.950	-.012	.842	.990	-.081	.832			
			.990	.020	.846						
					LOWER SURFACE						
.100	-.083	.831	.025	.386	.900	.025	.530	.921	.100	-.230	.810
.300	-.322	.796	.050	.086	.856	.050	.028	.848	.300	-.365	.790
.600	-.244	.808	.100	-.095	.830	.100	-.122	.826	.600	-.271	.804
.800	.262	.882	.200	-.232	.809	.200	-.235	.809	.800	.244	.879
			.300	-.311	.798	.300	-.333	.795			
			.400	-.349	.792	.400	-.374	.788			
			.500	-.389	.786	.500	-.341	.793			
			.600	-.175	.818	.600	-.208	.813			
			.700	.093	.857	.700	.047	.850			
			.800	.294	.887	.800	.288	.886			
			.900	.377	.899	.900	.315	.890			
			.950	.330	.892	.950	.329	.892			
			1.000	.022	.847						
CN=				.6667			.6303				
CM=				-.0937			-.0804				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.50. Continued.

$\alpha = 4.26^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.212	.518	0.000	.743	.953	0.000	.074	.855	.050	-2.163	.526
.150	-1.192	.668	.012	-1.827	.575	.012	-1.939	.559	.150	-1.051	.689
.300	-.854	.718	.025	-2.462	.482	.025	-2.082	.537	.300	-.777	.729
.450	-.649	.746	.050	-2.285	.508	.050	-2.113	.533	.450	-.601	.755
.600	-.584	.758	.100	-1.487	.625	.100	-1.379	.641	.600	-.529	.766
.800	-.376	.788	.150	-1.238	.662	.150	-1.143	.676	.800	-.325	.796
.990	.012	.845	.200	-1.131	.677	.200	-1.061	.688			
			.300	-.924	.708	.300	-.883	.714			
			.350	-.846	.719	.350	-.804	.725			
			.400	-.779	.729	.400	-.745	.734			
			.450	-.732	.736	.450	-.721	.738			
			.500	-.746	.734	.500	-.708	.740			
			.550	-.703	.740	.550	-.660	.747			
			.600	-.642	.749	.600	-.620	.752			
			.650	-.631	.751	.700	-.456	.776			
			.700	-.562	.761	.800	-.279	.803			
			.800	-.338	.794	.900	-.115	.827			
			.900	-.083	.831	.950	-.103	.828			
			.950	-.022	.840	.990	-.115	.827			
			.990	.003	.844						
					LOWER SURFACE						
.100	.046	.850	.025	.524	.921	.025	.617	.934	.100	-.119	.826
.300	-.264	.805	.050	.220	.876	.050	.176	.869	.300	-.315	.797
.600	-.229	.810	.100	.032	.848	.100	-.006	.843	.600	-.257	.806
.800	.274	.884	.200	-.152	.821	.200	-.159	.820	.800	.244	.879
			.300	-.238	.809	.300	-.271	.804			
			.400	-.306	.799	.400	-.333	.795			
			.500	-.358	.791	.500	-.322	.796			
			.600	-.149	.822	.600	-.188	.816			
			.700	.103	.859	.700	.052	.851			
			.800	.304	.888	.800	.292	.887			
			.900	.385	.900	.900	.319	.890			
			.950	.339	.893	.950	.332	.892			
			1.000	.007	.845						
CN=				.7755			.7300				
CM=				-.0891			-.0731				

(b) M = 0.50. Concluded

$\alpha = 5.39^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.811	.430	0.000	.616	.934	0.000	.086	.956	.050	-2.588	.463
.150	-1.286	.654	.012	-2.182	.523	.012	-2.290	.507	.150	-1.133	.677
.300	-.902	.711	.025	-2.812	.430	.025	-2.500	.476	.300	-.802	.726
.450	-.676	.744	.050	-2.859	.423	.050	-2.522	.473	.450	-.608	.754
.600	-.585	.758	.100	-1.613	.606	.100	-1.520	.620	.600	-.515	.768
.800	-.336	.794	.150	-1.351	.645	.150	-1.225	.663	.800	-.331	.795
.990	-.011	.842	.200	-1.202	.667	.200	-1.138	.676			
			.300	-.975	.700	.300	-.929	.707			
			.350	-.891	.712	.350	-.833	.721			
			.400	-.823	.722	.400	-.778	.729			
			.450	-.766	.731	.450	-.743	.734			
			.500	-.759	.732	.500	-.718	.738			
			.550	-.709	.739	.550	-.671	.745			
			.600	-.647	.748	.600	-.618	.753			
			.650	-.614	.753	.700	-.429	.780			
			.700	-.538	.764	.800	-.254	.806			
			.800	-.313	.798	.900	-.118	.826			
			.900	-.085	.831	.950	-.114	.827			
			.950	-.043	.837	.990	-.126	.825			
			.990	-.024	.840						
					LOWER SURFACE						
.100	.126	.862	.025	.615	.934	.025	.745	.953	.100	-.037	.843
.300	-.211	.813	.050	.357	.896	.050	.289	.886	.300	-.258	.806
.600	-.214	.812	.100	.127	.862	.100	.087	.856	.600	-.238	.808
.800	.279	.885	.200	-.078	.832	.200	-.109	.828	.800	.243	.879
			.300	-.188	.816	.300	-.210	.813			
			.400	-.270	.804	.400	-.291	.801			
			.500	-.331	.795	.500	-.270	.804			
			.600	-.138	.823	.600	-.178	.817			
			.700	.112	.860	.700	.069	.854			
			.800	.307	.889	.800	.294	.887			
			.900	.377	.899	.900	.331	.892			
			.950	.333	.892	.950	.331	.892			
			1.000	-.023	.840						
CN=				.8689			.8203				
CM=				-.0781			-.0643				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60

$\alpha = -4.49^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.413	.702	C.000	1.039	.989	0.000	.076	.799	.050	-.306	.723
.150	-.461	.693	.012	.425	.868	.012	.401	.863	.150	-.408	.703
.300	-.468	.691	.025	.006	.785	.025	.066	.797	.300	-.441	.697
.450	-.395	.706	.050	-.284	.728	.050	-.297	.725	.450	-.441	.697
.600	-.482	.688	.100	-.367	.711	.100	-.344	.716	.600	-.462	.693
.800	-.406	.704	.150	-.419	.701	.150	-.351	.715	.800	-.332	.718
.990	.076	.799	.200	-.470	.691	.200	-.438	.697			
			.300	-.478	.689	.300	-.479	.689			
			.350	-.469	.691	.350	-.457	.693			
			.400	-.478	.689	.400	-.454	.694			
			.450	-.455	.694	.450	-.496	.686			
			.500	-.534	.678	.500	-.521	.681			
			.550	-.542	.677	.550	-.517	.682			
			.600	-.488	.687	.600	-.529	.679			
			.650	-.553	.675	.700	-.438	.697			
			.700	-.524	.680	.800	-.314	.722			
			.800	-.376	.709	.900	-.039	.776			
			.900	-.075	.769	.950	.021	.788			
			.950	.042	.792	.990	.056	.795			
			.990	.127	.809						
					LOWER SURFACE						
.100	-.985	.589	.025	-.847	.616	.025	-.883	.609	.100	-1.304	.526
.300	-.736	.638	.050	-1.285	.530	.050	-1.396	.508	.300	-.691	.647
.600	-.319	.721	.100	-1.095	.567	.100	-1.181	.550	.600	-.318	.721
.800	.104	.804	.200	-.856	.615	.200	-.864	.613	.800	.106	.805
			.300	-.804	.625	.300	-.798	.626			
			.400	-.702	.645	.400	-.714	.643			
			.500	-.636	.658	.500	-.576	.670			
			.600	-.293	.726	.600	-.311	.722			
			.700	.037	.791	.700	-.018	.780			
			.800	.155	.815	.800	.195	.822			
			.900	.249	.833	.900	.241	.832			
			.950	.287	.841	.950	.284	.840			
			1.000	.133	.810						
CN=				-.0627			-.1001				
CM=				-.1050			-.1033				

(c) M = 0.60. Continued.

$\alpha = -3.10^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.621	.661	C.000	1.068	.995	0.000	.074	.798	.050	-.531	.679
.150	-.600	.665	.012	.190	.821	.012	.151	.814	.150	-.525	.680
.300	-.550	.675	.025	-.203	.744	.025	-.103	.764	.300	-.520	.681
.450	-.455	.694	.050	-.532	.679	.050	-.488	.687	.450	-.470	.691
.600	-.517	.682	.100	-.575	.670	.100	-.505	.684	.600	-.497	.686
.800	-.424	.700	.150	-.577	.670	.150	-.489	.687	.800	-.357	.713
.990	.067	.797	.200	-.594	.666	.200	-.547	.676			
			.300	-.556	.674	.300	-.556	.674			
			.350	-.561	.673	.350	-.531	.679			
			.400	-.526	.680	.400	-.517	.682			
			.450	-.518	.681	.450	-.553	.674			
			.500	-.595	.666	.500	-.572	.671			
			.550	-.601	.665	.550	-.569	.671			
			.600	-.555	.674	.600	-.564	.672			
			.650	-.591	.667	.700	-.461	.693			
			.700	-.560	.673	.800	-.334	.718			
			.800	-.391	.707	.900	-.068	.770			
			.900	-.094	.765	.950	-.005	.783			
			.950	.032	.790	.990	.026	.785			
			.990	.099	.803						
					LOWER SURFACE						
.100	-.803	.625	.025	-.567	.672	.025	-.494	.686	.100	-1.014	.583
.300	-.674	.651	.050	-.935	.599	.050	-1.087	.565	.300	-.640	.657
.600	-.330	.719	.100	-.903	.605	.100	-.910	.604	.600	-.327	.719
.800	.145	.813	.200	-.788	.628	.200	-.768	.632	.800	.176	.819
			.300	-.728	.640	.300	-.715	.642			
			.400	-.655	.654	.400	-.666	.652			
			.500	-.614	.663	.500	-.556	.674			
			.600	-.274	.730	.600	-.321	.720			
			.700	.043	.792	.700	-.008	.782			
			.800	.222	.828	.800	.246	.832			
			.900	.309	.845	.900	.300	.843			
			.950	.317	.846	.950	.316	.846			
			1.000	.115	.806						
CN=				.0815			.0517				
CM=				-.1133			-.1057				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\alpha = -2.35^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.649	.646	0.000	1.078	.997	0.000	.076	.799	.050	-.648	.656
.150	-.649	.656	.012	.649	.793	.012	.033	.790	.150	-.588	.667
.300	-.591	.667	.025	-.433	.698	.025	-.314	.722	.300	-.546	.676
.450	-.479	.689	.050	-.679	.650	.050	-.622	.661	.450	-.496	.686
.600	-.532	.679	.100	-.665	.652	.100	-.658	.654	.600	-.516	.682
.800	-.434	.698	.150	-.658	.654	.150	-.560	.673	.800	-.362	.712
.990	.069	.797	.200	-.660	.653	.200	-.620	.661			
			.300	-.618	.662	.300	-.596	.666			
			.350	-.592	.667	.350	-.581	.669			
			.400	-.580	.669	.400	-.556	.674			
			.450	-.551	.675	.450	-.587	.668			
			.500	-.607	.664	.500	-.602	.665			
			.550	-.623	.661	.550	-.587	.668			
			.600	-.573	.671	.600	-.585	.668			
			.650	-.606	.664	.700	-.468	.691			
			.700	-.572	.671	.800	-.333	.718			
			.800	-.394	.706	.900	-.069	.770			
			.900	-.095	.765	.950	-.016	.781			
			.950	.029	.789	.990	.010	.786			
			.990	.098	.803						
					LOWER SURFACE						
.100	-.696	.646	.025	-.426	.700	.025	-.347	.715	.100	-.937	.599
.300	-.620	.661	.050	-.780	.630	.050	-.928	.600	.300	-.615	.662
.600	-.320	.721	.100	-.786	.628	.100	-.798	.626	.600	-.336	.717
.800	.185	.820	.200	-.711	.643	.200	-.715	.642	.800	.194	.822
			.300	-.672	.651	.300	-.678	.650			
			.400	-.623	.661	.400	-.629	.655			
			.500	-.593	.667	.500	-.533	.678			
			.600	-.272	.730	.600	-.307	.723			
			.700	.055	.795	.700	-.002	.783			
			.800	.239	.831	.800	.265	.836			
			.900	.345	.852	.900	.315	.846			
			.950	.332	.850	.950	.333	.850			
			1.000	.104	.804						
CN=				.1661			.1356				
CM=				-.1145			-.1057				

(c) M = 0.60. Continued.

$\alpha = -1.66^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.958	.594	0.000	1.075	.996	0.000	.084	.800	.050	-.813	.623
.150	-.733	.638	.012	-.090	.766	.012	-.146	.754	.150	-.641	.657
.300	-.633	.658	.025	-.575	.670	.025	-.390	.706	.300	-.587	.667
.450	-.521	.680	.050	-.798	.625	.050	-.786	.628	.450	-.520	.681
.600	-.547	.675	.100	-.734	.638	.100	-.713	.642	.600	-.523	.680
.800	-.423	.700	.150	-.726	.640	.150	-.649	.655	.800	-.353	.714
.990	.062	.796	.200	-.699	.645	.200	-.669	.651			
			.300	-.652	.654	.300	-.638	.657			
			.350	-.628	.659	.350	-.602	.664			
			.400	-.618	.661	.400	-.587	.667			
			.450	-.582	.668	.450	-.609	.663			
			.500	-.647	.655	.500	-.627	.659			
			.550	-.641	.656	.550	-.603	.664			
			.600	-.602	.664	.600	-.598	.665			
			.650	-.618	.661	.700	-.468	.691			
			.700	-.586	.667	.800	-.329	.718			
			.800	-.401	.704	.900	-.066	.770			
			.900	-.084	.767	.950	-.012	.781			
			.950	.028	.789	.990	.005	.785			
			.990	.095	.802						
					LOWER SURFACE						
.100	-.636	.658	.025	-.310	.722	.025	-.235	.737	.100	-.839	.617
.300	-.599	.665	.050	-.655	.654	.050	-.719	.641	.300	-.583	.668
.600	-.317	.721	.100	-.655	.654	.100	-.716	.642	.600	-.328	.719
.800	.202	.824	.200	-.651	.654	.200	-.642	.656	.800	.217	.826
			.300	-.642	.656	.300	-.649	.655			
			.400	-.591	.666	.400	-.610	.663			
			.500	-.578	.669	.500	-.507	.683			
			.600	-.275	.729	.600	-.301	.724			
			.700	.060	.795	.700	.006	.785			
			.800	.257	.834	.800	.284	.840			
			.900	.360	.855	.900	.326	.848			
			.950	.345	.852	.950	.348	.852			
			1.000	.100	.803						
CN=				.2363			.2054				
CM=				-.1143			-.1040				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\alpha = -0.99^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.976	.591	0.000	1.078	.957	0.000	.075	.795	.050	-.973	.591
.150	-.798	.626	.012	-.197	.745	.012	-.277	.729	.150	-.749	.638
.300	-.665	.652	.025	-.714	.643	.025	-.568	.672	.300	-.636	.658
.450	-.538	.678	.050	-.960	.594	.050	-.896	.607	.450	-.544	.676
.600	-.553	.675	.100	-.859	.614	.100	-.794	.627	.600	-.535	.678
.800	-.426	.700	.150	-.799	.626	.150	-.700	.646	.800	-.371	.711
.990	.044	.793	.200	-.770	.632	.200	-.722	.641			
			.300	-.703	.645	.300	-.676	.650			
			.350	-.666	.652	.350	-.637	.658			
			.400	-.647	.656	.400	-.610	.663			
			.450	-.604	.664	.450	-.624	.660			
			.500	-.665	.652	.500	-.635	.658			
			.550	-.655	.654	.550	-.615	.662			
			.600	-.612	.663	.600	-.601	.665			
			.650	-.625	.660	.700	-.471	.691			
			.700	-.587	.668	.800	-.322	.720			
			.800	-.401	.705	.900	-.076	.769			
			.900	-.086	.767	.950	-.022	.780			
			.950	.020	.788	.990	-.019	.780			
			.990	.076	.799						
					LOWER SURFACE						
.100	-.525	.680	.025	-.178	.749	.025	-.118	.761	.100	-.712	.643
.300	-.566	.672	.050	-.541	.677	.050	-.596	.666	.300	-.562	.673
.600	-.316	.721	.100	-.574	.670	.100	-.608	.664	.600	-.331	.718
.800	.218	.827	.200	-.584	.668	.200	-.595	.666	.800	.228	.829
			.300	-.603	.665	.300	-.599	.665			
			.400	-.570	.671	.400	-.579	.669			
			.500	-.568	.672	.500	-.492	.687			
			.600	-.254	.734	.600	-.299	.725			
			.700	.070	.798	.700	.010	.786			
			.800	.268	.837	.800	.286	.840			
			.900	.369	.857	.900	.323	.848			
			.950	.337	.850	.950	.340	.851			
			1.000	.089	.801						
CN=				.3040			.2664				
CM=				-.1132			-.1003				

(c) M = 0.60. Continued.

$\alpha = -0.31^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.202	.546	0.000	1.069	.995	0.000	.089	.801	.050	-1.107	.565
.150	-.852	.615	.012	-.355	.714	.012	-.442	.696	.150	-.778	.630
.300	-.706	.644	.025	-.918	.602	.025	-.732	.639	.300	-.638	.658
.450	-.548	.675	.050	-1.133	.560	.050	-1.089	.568	.450	-.555	.674
.600	-.564	.672	.100	-.975	.591	.100	-.911	.604	.600	-.532	.679
.800	-.412	.702	.150	-.875	.611	.150	-.792	.627	.800	-.354	.714
.990	.043	.792	.200	-.819	.622	.200	-.784	.629			
			.300	-.734	.639	.300	-.733	.639			
			.350	-.699	.646	.350	-.671	.651			
			.400	-.672	.651	.400	-.636	.658			
			.450	-.631	.659	.450	-.647	.656			
			.500	-.676	.650	.500	-.661	.653			
			.550	-.667	.652	.550	-.636	.658			
			.600	-.620	.661	.600	-.613	.663			
			.650	-.631	.659	.700	-.469	.691			
			.700	-.577	.670	.800	-.315	.721			
			.800	-.380	.709	.900	-.081	.768			
			.900	-.082	.768	.950	-.037	.776			
			.950	.021	.788	.990	-.023	.779			
			.990	.064	.796						
					LOWER SURFACE						
.100	-.438	.697	.025	-.057	.772	.025	.032	.790	.100	-.651	.655
.300	-.531	.679	.050	-.438	.697	.050	-.511	.683	.300	-.536	.678
.600	-.297	.725	.100	-.505	.684	.100	-.501	.685	.600	-.332	.718
.800	.225	.828	.200	-.529	.679	.200	-.536	.678	.800	.242	.832
			.300	-.562	.673	.300	-.594	.674			
			.400	-.535	.678	.400	-.560	.673			
			.500	-.540	.677	.500	-.482	.685			
			.600	-.245	.735	.600	-.281	.728			
			.700	.070	.798	.700	.019	.788			
			.800	.272	.838	.800	.287	.840			
			.900	.359	.855	.900	.334	.850			
			.950	.340	.851	.950	.340	.851			
			1.000	.071	.798						
CN=				.3633			.3400				
CM=				-.1087			-.0965				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\alpha = 0.35^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.385	.510	0.000	1.065	.994	0.000	.081	.800	.050	-1.257	.535
.150	-.905	.605	.012	-.524	.680	.012	-.556	.674	.150	-.793	.627
.300	-.735	.638	.025	-.989	.588	.025	-.881	.609	.300	-.693	.647
.450	-.576	.670	.050	-1.323	.522	.050	-1.251	.536	.450	-.570	.671
.600	-.570	.671	.100	-1.092	.568	.100	-1.056	.575	.600	-.541	.677
.800	-.407	.703	.150	-.925	.601	.150	-.826	.620	.800	-.347	.715
.990	.045	.793	.200	-.887	.608	.200	-.837	.618			
			.300	-.773	.631	.300	-.755	.634			
			.350	-.735	.638	.350	-.705	.644			
			.400	-.698	.646	.400	-.661	.653			
			.450	-.660	.653	.450	-.683	.649			
			.500	-.697	.646	.500	-.673	.651			
			.550	-.678	.649	.550	-.646	.656			
			.600	-.629	.659	.600	-.614	.662			
			.650	-.639	.657	.700	-.461	.693			
			.700	-.584	.668	.800	-.300	.724			
			.800	-.375	.709	.900	-.090	.766			
			.900	-.074	.769	.950	-.060	.772			
			.950	.012	.786	.990	-.044	.775			
			.990	.050	.794						
					LOWER SURFACE						
.100	-.377	.709	.025	.017	.787	.025	.121	.808	.100	-.596	.666
.300	-.484	.688	.050	-.306	.723	.050	-.392	.706	.300	-.516	.682
.600	-.301	.724	.100	-.420	.701	.100	-.458	.693	.600	-.326	.719
.800	.238	.831	.200	-.485	.688	.200	-.480	.689	.800	.238	.831
			.300	-.519	.681	.300	-.524	.680			
			.400	-.508	.683	.400	-.531	.679			
			.500	-.527	.679	.500	-.474	.690			
			.600	-.249	.734	.600	-.284	.728			
			.700	.074	.798	.700	.018	.787			
			.800	.277	.839	.800	.292	.841			
			.900	.371	.857	.900	.329	.849			
			.950	.337	.850	.950	.343	.852			
			1.000	.067	.797						
CN=				.4248			.3952				
CM=				-.1060			-.0930				

(c) M = 0.60. Continued.

$\alpha = 1.03^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.538	.486	0.000	1.042	.990	0.000	.086	.801	.050	-1.452	.497
.150	-.973	.591	.012	-.685	.648	.012	-.789	.628	.150	-.855	.615
.300	-.783	.629	.025	-1.181	.550	.025	-1.068	.572	.300	-.709	.644
.450	-.599	.665	.050	-1.581	.471	.050	-1.445	.498	.450	-.577	.670
.600	-.577	.670	.100	-1.215	.543	.100	-1.139	.555	.600	-.546	.676
.800	-.403	.704	.150	-.982	.590	.150	-.886	.609	.800	-.338	.717
.950	.037	.791	.200	-.951	.596	.200	-.884	.609			
			.300	-.817	.622	.300	-.794	.627			
			.350	-.759	.634	.350	-.726	.640			
			.400	-.720	.641	.400	-.691	.647			
			.450	-.683	.649	.450	-.694	.647			
			.500	-.713	.643	.500	-.687	.648			
			.550	-.693	.647	.550	-.656	.654			
			.600	-.645	.656	.600	-.623	.661			
			.650	-.642	.657	.700	-.465	.692			
			.700	-.574	.670	.800	-.294	.726			
			.800	-.369	.711	.900	-.093	.765			
			.900	-.078	.768	.950	-.065	.771			
			.950	.006	.785	.990	-.063	.771			
			.990	.039	.791						
					LOWER SURFACE						
.100	-.276	.729	.025	.120	.807	.025	.229	.829	.100	-.474	.690
.300	-.466	.692	.050	-.190	.746	.050	-.276	.729	.300	-.474	.690
.600	-.299	.725	.100	-.327	.719	.100	-.343	.716	.600	-.315	.721
.800	.242	.832	.200	-.443	.696	.200	-.427	.699	.800	.243	.832
			.300	-.485	.688	.300	-.486	.688			
			.400	-.476	.690	.400	-.506	.684			
			.500	-.505	.684	.500	-.445	.696			
			.600	-.238	.737	.600	-.263	.732			
			.700	.079	.799	.700	.020	.788			
			.800	.282	.840	.800	.291	.841			
			.900	.365	.856	.900	.336	.850			
			.950	.340	.851	.950	.344	.852			
			1.000	.051	.794						
CN=				.4918			.4637				
CM=				-.1019			-.0892				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60. Continued.

$\alpha = 1.72^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.685	.450	0.000	1.014	.984	0.000	.085	.801	.050	-1.752	.437
.150	-1.039	.578	.012	-.824	.621	.012	-.899	.606	.150	-.920	.602
.300	-.803	.625	.025	-1.394	.508	.025	-1.233	.540	.300	-.725	.640
.450	-.624	.660	.050	-1.776	.432	.050	-1.725	.442	.450	-.596	.666
.600	-.585	.668	.100	-1.364	.514	.100	-1.249	.537	.600	-.544	.676
.800	-.394	.706	.150	-1.056	.575	.150	-.974	.591	.800	-.350	.714
.990	.024	.738	.200	-1.007	.585	.200	-.948	.596			
			.300	-.868	.612	.300	-.837	.618			
			.350	-.792	.627	.350	-.756	.634			
			.400	-.748	.636	.400	-.712	.643			
			.450	-.712	.643	.450	-.705	.644			
			.500	-.735	.638	.500	-.698	.646			
			.550	-.707	.644	.550	-.661	.653			
			.600	-.654	.654	.600	-.617	.662			
			.650	-.641	.657	.700	-.455	.694			
			.700	-.578	.669	.800	-.284	.728			
			.800	-.340	.716	.900	-.095	.765			
			.900	-.090	.768	.950	-.080	.768			
			.950	-.009	.782	.990	-.086	.767			
			.990	.023	.788						
					LOWER SURFACE						
.100	-.241	.736	.025	.219	.827	.025	.307	.844	.100	-.436	.697
.300	-.437	.697	.050	-.118	.760	.050	-.145	.755	.300	-.456	.694
.600	-.284	.727	.100	-.251	.734	.100	-.297	.725	.600	-.312	.722
.800	.248	.833	.200	-.369	.711	.200	-.392	.706	.800	.247	.833
			.300	-.434	.698	.300	-.447	.695			
			.400	-.458	.693	.400	-.496	.686			
			.500	-.493	.686	.500	-.430	.699			
			.600	-.228	.739	.600	-.265	.731			
			.700	.079	.799	.700	.038	.791			
			.800	.287	.840	.800	.289	.841			
			.900	.371	.857	.900	.334	.850			
			.950	.340	.851	.950	.341	.851			
			1.000	.027	.789						
CN=				.5599			.5222				
CM=				-.0977			-.0838				

(c) M = 0.60. Continued.

$\alpha = 2.42^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.427	.403	0.000	.990	.980	0.000	.085	.801	.050	-1.954	.398
.150	-1.008	.573	.012	-.948	.596	.012	-1.066	.573	.150	-.956	.595
.300	-.820	.622	.025	-1.540	.479	.025	-1.280	.531	.300	-.750	.636
.450	-.632	.659	.050	-1.974	.394	.050	-1.909	.406	.450	-.600	.665
.600	-.582	.669	.100	-1.805	.427	.100	-1.455	.496	.600	-.544	.676
.800	-.385	.708	.150	-1.084	.569	.150	-.991	.588	.800	-.333	.718
.990	.025	.789	.200	-1.046	.577	.200	-.983	.590			
			.300	-.878	.610	.300	-.856	.615			
			.350	-.813	.623	.350	-.796	.626			
			.400	-.760	.634	.400	-.729	.640			
			.450	-.726	.640	.450	-.728	.640			
			.500	-.731	.639	.500	-.710	.644			
			.550	-.701	.645	.550	-.665	.652			
			.600	-.651	.655	.600	-.629	.659			
			.650	-.625	.660	.700	-.444	.696			
			.700	-.553	.674	.800	-.265	.732			
			.800	-.322	.720	.900	-.105	.763			
			.900	-.060	.772	.950	-.096	.765			
			.950	-.008	.782	.990	-.087	.767			
			.990	.007	.785						
					LOWER SURFACE						
.100	-.162	.752	.025	.295	.842	.025	.429	.869	.100	-.366	.712
.300	-.342	.706	.050	-.034	.777	.050	-.073	.769	.300	-.422	.700
.600	-.278	.729	.100	-.185	.747	.100	-.213	.742	.600	-.310	.723
.800	.253	.834	.200	-.314	.722	.200	-.324	.720	.800	.258	.835
			.300	-.387	.707	.300	-.417	.701			
			.400	-.430	.699	.400	-.454	.694			
			.500	-.469	.691	.500	-.420	.701			
			.600	-.216	.741	.600	-.254	.734			
			.700	.085	.801	.700	.029	.790			
			.800	.289	.841	.800	.302	.844			
			.900	.386	.860	.900	.335	.850			
			.950	.335	.850	.950	.346	.852			
			1.000	.011	.786						
CN=				.6219			.5836				
CM=				-.0894			-.0799				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(c) M = 0.60. Concluded.

$\alpha = 3.79^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.302	.329	0.000	.897	.961	0.000	.088	.801	.050	-2.238	.341
.150	-1.029	.580	.012	-1.227	.541	.012	-1.339	.519	.150	-.985	.589
.300	-.849	.616	.025	-1.814	.425	.025	-1.564	.475	.300	-.788	.628
.450	-.649	.656	.050	-2.187	.351	.050	-2.102	.368	.450	-.617	.662
.600	-.592	.667	.100	-2.280	.333	.100	-2.093	.370	.600	-.536	.678
.800	-.368	.711	.150	-1.350	.517	.150	-1.194	.548	.800	-.342	.716
.990	.023	.738	.200	-1.021	.582	.200	-1.010	.584			
			.300	-.920	.602	.300	-.906	.605			
			.350	-.850	.616	.350	-.827	.620			
			.400	-.783	.629	.400	-.769	.632			
			.450	-.760	.633	.450	-.746	.636			
			.500	-.764	.633	.500	-.735	.639			
			.550	-.717	.642	.550	-.686	.648			
			.600	-.657	.654	.600	-.636	.658			
			.650	-.630	.659	.700	-.442	.697			
			.700	-.557	.674	.800	-.279	.729			
			.800	-.327	.719	.900	-.107	.763			
			.900	-.078	.768	.950	-.083	.767			
			.950	-.008	.782	.990	-.067	.770			
			.990	.023	.788						
					LOWER SURFACE						
.100	-.022	.779	.025	.432	.369	.025	.551	.893	.100	-.196	.747
.300	-.319	.721	.050	.160	.815	.050	.080	.800	.300	-.366	.711
.600	-.231	.734	.100	-.062	.771	.100	-.077	.769	.600	-.291	.726
.800	.267	.837	.200	-.227	.739	.200	-.249	.735	.800	.248	.833
			.300	-.321	.720	.300	-.337	.717			
			.400	-.366	.712	.400	-.404	.704			
			.500	-.422	.700	.500	-.365	.712			
			.600	-.184	.747	.600	-.229	.735			
			.700	.099	.803	.700	.044	.793			
			.800	.310	.845	.800	.309	.845			
			.900	.385	.860	.900	.353	.854			
			.950	.350	.853	.950	.355	.854			
			1.000	.032	.790						
CN=				.7402			.7092				
CM=				-.0861			-.0730				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(d) M = 0.65

$\alpha = -4.63^{\circ}$

TEST 543 RUN 54 POINT 59 CONFIG MACH= .650 ALPHA= DATE 09/15/70

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.330	.675	C.CCC	1.060	.989	C.000	.073	.769	.050	-.218	.734
.150	-.456	.651	.012	.481	.803	.012	.390	.840	.150	-.426	.654
.300	-.473	.647	.025	.068	.764	.025	.122	.785	.300	-.466	.647
.450	-.405	.663	.050	-.287	.683	.050	-.263	.694	.450	-.463	.650
.600	-.487	.644	.100	-.332	.668	.100	-.346	.676	.600	-.497	.642
.800	-.404	.663	.150	-.421	.659	.150	-.365	.671	.800	-.327	.680
.990	.090	.773	.200	-.469	.648	.200	-.454	.652			
			.300	-.483	.646	.300	-.483	.645			
			.350	-.498	.642	.350	-.485	.645			
			.400	-.497	.642	.400	-.466	.649			
			.450	-.485	.645	.450	-.510	.639			
			.500	-.502	.627	.500	-.951	.630			
			.550	-.564	.627	.550	-.540	.633			
			.600	-.511	.633	.600	-.556	.629			
			.650	-.556	.629	.700	-.440	.655			
			.700	-.536	.633	.800	-.285	.685			
			.800	-.361	.672	.900	-.026	.747			
			.900	-.045	.743	.950	.024	.758			
			.950	.073	.769	.990	.041	.762			
			.990	.132	.782						
					LOWER SURFACE						
.100	-1.115	.604	.025	-.845	.506	.025	-.734	.589	.100	-1.632	.589
.300	-.783	.578	.050	-1.480	.423	.050	-1.390	.443	.300	-.714	.594
.600	-.303	.685	.100	-1.391	.492	.100	-1.472	.425	.600	-.311	.643
.800	.064	.767	.200	-.563	.513	.200	-.488	.555	.800	.072	.769
			.300	-.874	.558	.300	-.855	.562			
			.400	-.757	.584	.400	-.758	.584			
			.500	-.658	.606	.500	-.599	.615			
			.600	-.269	.693	.600	-.306	.685			
			.700	.021	.757	.700	-.030	.746			
			.800	.120	.789	.800	.157	.788			
			.900	.207	.799	.900	.209	.795			
			.950	.251	.809	.950	.262	.811			
			1.000	.140	.784						
CN=				-.1334			-.1352				
CM=				-.1026			-.0950				

(d) M = 0.65. Continued.

$\alpha = -3.11^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.621	.614	C.CCC	1.089	.995	C.000	.079	.770	.050	-.519	.687
.150	-.616	.615	.012	.203	.754	.012	.213	.800	.150	-.534	.683
.300	-.567	.626	.025	-.151	.710	.025	-.146	.720	.300	-.532	.684
.450	-.464	.649	.050	-.532	.634	.050	-.504	.640	.450	-.500	.641
.600	-.530	.635	.100	-.577	.624	.100	-.546	.631	.600	-.519	.637
.800	-.415	.660	.150	-.566	.626	.150	-.500	.641	.800	-.343	.676
.990	.070	.768	.200	-.643	.609	.200	-.579	.624			
			.300	-.602	.617	.300	-.580	.623			
			.350	-.570	.626	.350	-.574	.625			
			.400	-.580	.623	.400	-.535	.634			
			.450	-.533	.633	.450	-.576	.624			
			.500	-.630	.612	.500	-.599	.619			
			.550	-.614	.615	.550	-.600	.619			
			.600	-.565	.627	.600	-.563	.623			
			.650	-.606	.618	.700	-.454	.651			
			.700	-.572	.625	.800	-.307	.684			
			.800	-.381	.668	.900	-.051	.741			
			.900	-.067	.733	.950	-.018	.749			
			.950	.046	.763	.990	.002	.755			
			.990	.102	.775						
					LOWER SURFACE						
.100	-.891	.554	.025	-.574	.625	.025	-.490	.644	.100	-1.244	.475
.300	-.698	.597	.050	-.365	.684	.050	-1.073	.514	.300	-.676	.602
.600	-.301	.686	.100	-.957	.540	.100	-1.026	.524	.600	-.344	.676
.800	.141	.784	.200	-.831	.567	.200	-.820	.570	.800	.133	.732
			.300	-.771	.581	.300	-.777	.580			
			.400	-.711	.594	.400	-.718	.593			
			.500	-.649	.603	.500	-.584	.623			
			.600	-.288	.687	.600	-.324	.680			
			.700	.054	.765	.700	-.004	.752			
			.800	.198	.797	.800	.228	.803			
			.900	.310	.822	.900	.285	.816			
			.950	.328	.826	.950	.302	.820			
			1.000	.116	.779						
CN=				.0668			.0325				
CM=				-.1124			-.1028				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

α = -2.39°

TEST 543 RUN 54 POINT 61 CONFIG MACH= .650 ALPHA= DATE 09/10/70

STATION .1552 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.723	.552	0.000	1.093	.556	0.000	.093	.773	.050	-.662	.605
.150	-.684	.600	.012	.110	.777	.012	.033	.760	.150	-.593	.619
.300	-.612	.616	.025	-.365	.671	.025	-.273	.692	.300	-.578	.624
.450	-.495	.642	.050	-.555	.553	.050	-.039	.618	.450	-.522	.636
.600	-.543	.632	.100	-.673	.603	.100	-.618	.615	.600	-.527	.635
.800	-.414	.661	.150	-.673	.605	.150	-.590	.621	.800	-.556	.673
.990	.068	.766	.200	-.685	.600	.200	-.634	.612			
			.300	-.626	.613	.300	-.619	.615			
			.350	-.617	.615	.350	-.597	.620			
			.400	-.604	.613	.400	-.570	.626			
			.450	-.587	.626	.450	-.610	.617			
			.500	-.638	.611	.500	-.636	.611			
			.550	-.649	.603	.550	-.615	.616			
			.600	-.603	.613	.600	-.611	.617			
			.650	-.632	.612	.700	-.471	.646			
			.700	-.582	.623	.800	-.315	.683			
			.800	-.375	.664	.900	-.065	.736			
			.900	-.072	.737	.950	-.025	.747			
			.950	.039	.761	.990	.004	.754			
			.990	.099	.775						
					LOWER SURFACE						
.100	-.782	.578	.025	-.440	.655	.025	-.337	.676	.100	-1.071	.514
.300	-.663	.605	.050	-.865	.569	.050	-.964	.539	.300	-.641	.610
.600	-.305	.665	.100	-.826	.569	.100	-.582	.656	.600	-.542	.676
.800	.170	.751	.200	-.789	.577	.200	-.784	.578	.800	.151	.733
			.300	-.745	.587	.300	-.736	.585			
			.400	-.669	.604	.400	-.681	.601			
			.500	-.623	.613	.500	-.577	.624			
			.600	-.281	.653	.600	-.319	.662			
			.700	.070	.764	.700	.009	.755			
			.800	.226	.803	.800	.264	.811			
			.900	.340	.830	.900	.314	.823			
			.950	.333	.827	.950	.344	.829			
			1.000	.102	.775						
CN=				.1440			.1157				
CM=				-.1142			-.1074				

(d) M = 0.65. Continued.

α = -1.68°

STATION .1552 X/C	CP	P/PTINF	STATION .4245 X/C	CP	P/PTINF	STATION .7325 X/C	CP	P/PTINF	STATION .9025 X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.617	.570	0.000	1.056	.997	0.000	.095	.774	.050	-.483	.556
.150	-.781	.585	.012	.010	.755	.012	-.089	.733	.150	-.677	.602
.300	-.654	.607	.025	-.554	.629	.025	-.389	.666	.300	-.627	.613
.450	-.533	.634	.050	-.796	.575	.050	-.636	.586	.450	-.540	.632
.600	-.554	.629	.100	-.773	.580	.100	-.732	.583	.600	-.539	.633
.800	-.421	.656	.150	-.754	.582	.150	-.650	.605	.800	-.547	.675
.990	.057	.765	.200	-.745	.587	.200	-.703	.596			
			.300	-.672	.603	.300	-.669	.604			
			.350	-.655	.607	.350	-.644	.609			
			.400	-.644	.609	.400	-.599	.615			
			.450	-.609	.617	.450	-.641	.610			
			.500	-.662	.605	.500	-.658	.606			
			.550	-.668	.604	.550	-.644	.609			
			.600	-.613	.616	.600	-.628	.613			
			.650	-.632	.612	.700	-.475	.647			
			.700	-.587	.622	.800	-.312	.683			
			.800	-.380	.664	.900	-.070	.737			
			.900	-.077	.735	.950	-.021	.748			
			.950	.038	.761	.990	-.010	.750			
			.990	.090	.775						
					LOWER SURFACE						
.100	-.669	.603	.025	-.280	.695	.025	-.209	.706	.100	-.916	.549
.300	-.632	.612	.050	-.864	.569	.050	-.753	.585	.300	-.618	.615
.600	-.305	.664	.100	-.712	.594	.100	-.780	.578	.600	-.545	.676
.800	.183	.753	.200	-.710	.594	.200	-.713	.594	.800	.202	.738
			.300	-.687	.600	.300	-.697	.597			
			.400	-.643	.609	.400	-.656	.605			
			.500	-.611	.616	.500	-.549	.630			
			.600	-.271	.652	.600	-.310	.683			
			.700	.072	.769	.700	.012	.755			
			.800	.234	.809	.800	.269	.818			
			.900	.344	.829	.900	.325	.825			
			.950	.338	.823	.950	.346	.830			
			1.000	.096	.774						
CN=				.2188			.1932				
CM=				-.1135			-.1041				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\alpha = -0.93^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.557	.531	C.000	1.051	.556	C.000	.091	.773	.050	-.792	.532
.150	-.830	.568	.012	-.133	.723	.012	-.223	.705	.150	-.773	.581
.300	-.665	.600	.025	-.649	.604	.025	-.481	.646	.300	-.552	.608
.450	-.565	.627	.050	-1.026	.524	.050	-.994	.531	.450	-.570	.626
.600	-.513	.625	.100	-.858	.553	.100	-.868	.560	.600	-.554	.629
.800	-.402	.663	.150	-.855	.562	.150	-.739	.588	.800	-.348	.675
.990	.050	.764	.200	-.837	.565	.200	-.773	.581			
			.300	-.737	.589	.300	-.721	.592			
			.350	-.696	.593	.350	-.664	.605			
			.400	-.678	.602	.400	-.640	.610			
			.450	-.636	.611	.450	-.661	.605			
			.500	-.707	.595	.500	-.675	.602			
			.550	-.683	.601	.550	-.651	.608			
			.600	-.645	.609	.600	-.526	.613			
			.650	-.644	.609	.700	-.470	.646			
			.700	-.586	.622	.800	-.299	.686			
			.800	-.383	.667	.900	-.079	.735			
			.900	-.069	.737	.950	-.035	.745			
			.950	.033	.760	.990	-.021	.748			
			.990	.071	.769						
					LOWER SURFACE						
.100	-.565	.627	.025	-.175	.714	.025	-.062	.723	.100	-.936	.567
.300	-.603	.619	.050	-.517	.634	.050	-.613	.616	.300	-.576	.624
.600	-.316	.682	.100	-.642	.613	.100	-.690	.599	.600	-.340	.677
.800	.200	.757	.200	-.618	.619	.200	-.646	.605	.800	.225	.803
			.300	-.653	.607	.300	-.653	.607			
			.400	-.610	.617	.400	-.623	.614			
			.500	-.598	.620	.500	-.530	.635			
			.600	-.266	.694	.600	-.302	.686			
			.700	.075	.769	.700	.013	.756			
			.800	.263	.811	.800	.283	.816			
			.900	.363	.834	.900	.337	.828			
			.950	.342	.829	.950	.349	.831			
			1.000	.086	.772						
CN=				.2970			.2662				
CM=				-.1127			-.1007				

(d) M = 0.65. Continued.

$\alpha = -0.27^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.200	.486	C.000	1.056	.557	C.000	.066	.772	.050	-1.193	.486
.150	-.900	.552	.012	-.287	.687	.012	-.367	.671	.150	-.854	.553
.300	-.715	.593	.025	-.810	.573	.025	-.625	.614	.300	-.691	.599
.450	-.567	.627	.050	-1.212	.483	.050	-1.097	.508	.450	-.582	.623
.600	-.577	.624	.100	-1.060	.517	.100	-.942	.543	.600	-.552	.630
.800	-.403	.663	.150	-.924	.547	.150	-.801	.574	.800	-.342	.677
.990	.041	.762	.200	-.878	.557	.200	-.826	.569			
			.300	-.785	.578	.300	-.765	.582			
			.350	-.739	.588	.350	-.715	.594			
			.400	-.704	.596	.400	-.677	.602			
			.450	-.667	.604	.450	-.679	.602			
			.500	-.711	.594	.500	-.690	.598			
			.550	-.691	.599	.550	-.662	.605			
			.600	-.648	.608	.600	-.534	.632			
			.650	-.650	.608	.700	-.459	.651			
			.700	-.651	.621	.800	-.281	.690			
			.800	-.471	.673	.900	-.086	.734			
			.900	-.061	.737	.950	-.055	.741			
			.950	.016	.755	.990	-.059	.740			
			.990	.040	.762						
					LOWER SURFACE						
.100	-.485	.645	.025	-.066	.733	.025	.047	.763	.100	-.705	.596
.300	-.565	.627	.050	-.421	.659	.050	-.553	.630	.300	-.558	.628
.600	-.311	.684	.100	-.533	.634	.100	-.562	.626	.600	-.344	.676
.800	.224	.803	.200	-.580	.624	.200	-.570	.626	.800	.233	.805
			.300	-.602	.619	.300	-.618	.615			
			.400	-.589	.622	.400	-.601	.619			
			.500	-.583	.623	.500	-.517	.633			
			.600	-.270	.693	.600	-.302	.685			
			.700	.068	.764	.700	.014	.756			
			.800	.269	.813	.800	.292	.818			
			.900	.361	.833	.900	.329	.826			
			.950	.344	.829	.950	.339	.828			
			1.000	.058	.766						
CN=				.3617			.3273				
CM=				-.1077			-.0965				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\alpha = 0.44^{\circ}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.349	.452	0.000	1.061	.993	0.000	.088	.772	.050	-1.360	.450
.150	-.523	.547	.012	-.408	.662	.012	-.514	.638	.150	-.815	.571
.300	-.783	.583	.025	-.535	.545	.025	-.607	.579	.300	-.717	.573
.450	-.601	.615	.050	-1.323	.453	.050	-1.339	.454	.450	-.990	.621
.600	-.576	.625	.100	-1.242	.475	.100	-1.096	.509	.600	-.559	.628
.800	-.392	.665	.150	-.334	.545	.150	-.857	.562	.800	-.340	.677
.990	.030	.761	.200	-.541	.543	.200	-.884	.556			
			.300	-.814	.571	.300	-.811	.572			
			.350	-.760	.584	.350	-.752	.585			
			.400	-.725	.591	.400	-.691	.595			
			.450	-.693	.598	.450	-.656	.597			
			.500	-.723	.592	.500	-.702	.596			
			.550	-.695	.598	.550	-.670	.603			
			.600	-.648	.609	.600	-.637	.611			
			.650	-.638	.611	.700	-.455	.652			
			.700	-.574	.625	.800	-.274	.692			
			.800	-.352	.674	.900	-.092	.732			
			.900	-.063	.733	.950	-.070	.737			
			.950	.002	.753	.990	-.066	.738			
			.990	.042	.762						
					LOWER SURFACE						
.100	-.417	.660	.025	.032	.760	.025	.129	.781	.100	-.620	.615
.300	-.531	.635	.050	-.329	.630	.050	-.398	.664	.300	-.546	.631
.600	-.308	.684	.100	-.457	.651	.100	-.471	.648	.600	-.349	.675
.800	.221	.804	.200	-.521	.637	.200	-.550	.635	.800	.235	.805
			.300	-.566	.627	.300	-.579	.624			
			.400	-.546	.631	.400	-.583	.623			
			.500	-.559	.628	.500	-.509	.639			
			.600	-.260	.695	.600	-.299	.686			
			.700	.080	.771	.700	.009	.755			
			.800	.271	.813	.800	.283	.810			
			.900	.365	.834	.900	.322	.824			
			.950	.339	.828	.950	.340	.830			
			1.000	.039	.761						
CN=				.4176			.3914				
CM=				-.1040			-.0908				

(d) M = 0.65. Continued.

$\alpha = 1.11^{\circ}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.523	.413	0.000	1.066	.990	0.000	.089	.772	.050	-1.452	.429
.150	-.620	.543	.012	-.515	.633	.012	-.626	.613	.150	-.761	.583
.300	-.792	.576	.025	-1.062	.516	.025	-.546	.542	.300	-.738	.568
.450	-.617	.615	.050	-1.502	.413	.050	-1.474	.424	.450	-.604	.616
.600	-.578	.624	.100	-1.390	.438	.100	-1.526	.413	.600	-.560	.628
.800	-.378	.668	.150	-1.082	.511	.150	-.881	.556	.800	-.342	.676
.990	.033	.760	.200	-.550	.541	.200	-.920	.548			
			.300	-.843	.585	.300	-.855	.562			
			.350	-.793	.575	.350	-.769	.581			
			.400	-.749	.586	.400	-.723	.591			
			.450	-.711	.594	.450	-.716	.593			
			.500	-.736	.589	.500	-.714	.594			
			.550	-.705	.595	.550	-.675	.602			
			.600	-.658	.605	.600	-.635	.611			
			.650	-.630	.612	.700	-.438	.655			
			.700	-.567	.626	.800	-.267	.693			
			.800	-.327	.680	.900	-.107	.729			
			.900	-.092	.741	.950	-.080	.735			
			.950	-.067	.751	.990	-.077	.736			
			.990	.027	.759						
					LOWER SURFACE						
.100	-.273	.652	.025	.124	.780	.025	.279	.815	.100	-.545	.631
.300	-.488	.644	.050	-.197	.707	.050	-.298	.680	.300	-.526	.635
.600	-.300	.686	.100	-.343	.675	.100	-.400	.664	.600	-.338	.677
.800	.232	.804	.200	-.442	.654	.200	-.471	.648	.900	.239	.806
			.300	-.567	.640	.300	-.537	.633			
			.400	-.523	.635	.400	-.557	.625			
			.500	-.544	.631	.500	-.490	.643			
			.600	-.246	.697	.600	-.294	.687			
			.700	.083	.771	.700	.018	.757			
			.800	.285	.816	.800	.284	.817			
			.900	.368	.835	.900	.327	.825			
			.950	.345	.827	.950	.345	.830			
			1.000	.028	.759						
CN=				.4962			.4651				
CM=				-.0972			-.0851				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(d) M = 0.65. Continued.

$\alpha = 2.70^{\circ}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.783	.356	0.000	1.000	.575	0.000	.000	.772	.050	-1.916	.348
.150	-1.754	.353	.012	-.775	.560	.012	-.900	.552	.150	-1.516	.415
.300	-.802	.574	.025	-1.342	.494	.025	-1.162	.494	.300	-.758	.584
.450	-.645	.609	.050	-1.740	.385	.050	-1.705	.423	.450	-.613	.616
.600	-.556	.620	.100	-1.931	.323	.100	-1.487	.383	.600	-.545	.631
.800	-.385	.667	.150	-1.835	.344	.150	-1.749	.383	.900	-.342	.677
.990	.033	.760	.200	-1.450	.433	.200	-.961	.539			
			.300	-.756	.585	.300	-.834	.587			
			.350	-.783	.573	.350	-.776	.580			
			.400	-.766	.582	.400	-.743	.587			
			.450	-.748	.586	.450	-.736	.589			
			.500	-.755	.584	.500	-.742	.588			
			.550	-.728	.591	.550	-.691	.599			
			.600	-.686	.603	.600	-.655	.607			
			.650	-.648	.609	.700	-.455	.651			
			.700	-.581	.623	.800	-.281	.690			
			.800	-.351	.675	.900	-.084	.734			
			.900	-.078	.736	.950	-.001	.735			
			.950	.016	.756	.990	-.039	.744			
			.990	.060	.766						
					LOWER SURFACE						
.100	-.130	.724	.025	.320	.824	.025	.430	.840	.100	-.344	.676
.300	-.392	.666	.050	.012	.756	.050	-.084	.734	.300	-.448	.653
.600	-.279	.691	.100	-.150	.719	.100	-.228	.702	.600	-.300	.686
.800	.266	.812	.200	-.314	.684	.200	-.313	.688	.900	.252	.809
			.300	-.401	.664	.300	-.429	.657			
			.400	-.444	.654	.400	-.473	.647			
			.500	-.478	.646	.500	-.433	.656			
			.600	-.208	.706	.600	-.255	.696			
			.700	.105	.773	.700	.045	.763			
			.800	.320	.824	.800	.315	.823			
			.900	.351	.840	.900	.357	.832			
			.950	.366	.834	.950	.371	.835			
			1.000	.063	.767						
CN=				.6837			.6214				
CM=				-.0927			-.0766				

(d) M = 0.65. Continued.

$\alpha = 4.20^{\circ}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.073	.291	0.000	.930	.960	0.000	.094	.774	.050	-2.909	.305
.150	-2.117	.281	.012	-.384	.534	.012	-1.217	.482	.150	-2.026	.302
.300	-.731	.590	.025	-1.557	.403	.025	-1.440	.432	.300	-.818	.571
.450	-.634	.612	.050	-1.347	.319	.050	-1.890	.332	.450	-.604	.617
.600	-.590	.621	.100	-2.138	.277	.100	-2.075	.291	.600	-.526	.636
.800	-.379	.668	.150	-2.055	.295	.150	-2.021	.303	.900	-.373	.670
.990	.045	.763	.200	-2.020	.303	.200	-1.902	.329			
			.300	-1.164	.494	.300	-.938	.544			
			.350	-.752	.585	.350	-.686	.600			
			.400	-.659	.605	.400	-.670	.602			
			.450	-.677	.602	.450	-.698	.597			
			.500	-.701	.597	.500	-.716	.593			
			.550	-.692	.599	.550	-.690	.595			
			.600	-.651	.609	.600	-.644	.609			
			.650	-.632	.612	.700	-.484	.645			
			.700	-.571	.626	.800	-.325	.680			
			.800	-.356	.674	.900	-.087	.733			
			.900	-.083	.734	.950	-.029	.746			
			.950	.011	.755	.990	.002	.753			
			.990	.071	.769						
					LOWER SURFACE						
.100	.026	.759	.025	.465	.855	.025	.597	.836	.100	-.184	.712
.300	-.322	.681	.050	.184	.794	.050	.120	.780	.300	-.374	.670
.600	-.237	.700	.100	-.062	.752	.100	-.041	.744	.600	-.303	.686
.800	.285	.816	.200	-.201	.703	.200	-.228	.702	.900	.264	.812
			.300	-.306	.683	.300	-.336	.678			
			.400	-.366	.671	.400	-.404	.663			
			.500	-.423	.659	.500	-.370	.670			
			.600	-.177	.713	.600	-.225	.703			
			.700	.122	.780	.700	.061	.766			
			.800	.333	.827	.800	.335	.827			
			.900	.416	.849	.900	.380	.837			
			.950	.387	.839	.950	.388	.839			
			1.000	.083	.771						
CN=				.8482			.8124				
CM=				-.0805			-.0710				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(d) M = 0.65. Concluded.

$\alpha = 5.54^{\circ}$

STATION .1592			STATION .4249			STATION .7325			STATION .9025		
x/c	CP	P/PTINF	x/c	CP	P/PTINF	x/c	CP	P/PTINF	x/c	CP	P/PTINF
					UPPER SURFACE						
.050	-2.238	.255	0.000	.871	.947	0.000	.086	.773	.050	-2.156	.274
.150	-2.244	.254	.012	-1.157	.495	.012	-1.349	.453	.150	-2.138	.278
.300	-.567	.538	.025	-1.720	.371	.025	-1.690	.377	.300	-1.074	.514
.450	-.614	.617	.050	-2.089	.289	.050	-2.085	.290	.450	-.606	.618
.600	-.556	.630	.100	-2.250	.244	.100	-2.212	.261	.600	-.546	.632
.800	-.325	.681	.150	-2.215	.261	.150	-2.108	.271	.800	-.365	.672
.950	.038	.762	.200	-2.173	.273	.200	-2.130	.279			
			.300	-1.341	.444	.300	-1.293	.466			
			.350	-1.077	.514	.350	-.987	.551			
			.400	-.783	.573	.400	-.892	.559			
			.450	-.677	.603	.450	-.864	.605			
			.500	-.654	.603	.500	-.808	.605			
			.550	-.622	.615	.550	-.824	.614			
			.600	-.585	.623	.600	-.809	.618			
			.650	-.535	.634	.700	-.453	.652			
			.700	-.490	.644	.800	-.312	.684			
			.800	-.310	.684	.900	-.079	.731			
			.900	-.096	.732	.950	-.043	.744			
			.950	-.000	.753	.990	-.018	.749			
			.990	.040	.762						
					LOWER SURFACE						
.100	.100	.775	.025	.572	.830	.025	.676	.803	.100	-.095	.733
.300	-.254	.697	.050	.302	.823	.050	.246	.808	.300	-.328	.680
.600	-.231	.702	.100	.096	.774	.100	.042	.762	.600	-.297	.687
.800	.250	.818	.200	-.117	.727	.200	-.152	.719	.800	.260	.811
			.300	-.232	.702	.300	-.278	.692			
			.400	-.317	.683	.400	-.371	.671			
			.500	-.365	.668	.500	-.347	.676			
			.600	-.153	.719	.600	-.205	.706			
			.700	.122	.765	.700	.061	.767			
			.800	.332	.827	.800	.330	.827			
			.900	.417	.845	.900	.370	.835			
			.950	.389	.843	.950	.389	.840			
			1.000	.054	.765						
CA=				.5478			.9191				
CM=				-.0771			-.0629				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(e) M = 0.70

α = -4.98°

STATION .1532			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.281	.657	0.000	1.065	.384	0.000	.086	.742	.050	-.242	.661
.150	-.456	.608	.012	.479	.839	.012	.455	.833	.150	-.436	.613
.300	-.494	.599	.025	.126	.752	.025	.177	.765	.300	-.503	.597
.450	-.391	.624	.050	-.240	.662	.050	-.200	.672	.450	-.496	.594
.600	-.516	.594	.100	-.350	.634	.100	-.339	.637	.600	-.519	.593
.800	-.405	.621	.150	-.416	.618	.150	-.396	.623	.800	-.339	.637
.990	.086	.742	.200	-.471	.605	.200	-.430	.615			
			.300	-.506	.595	.300	-.530	.590			
			.350	-.509	.595	.350	-.508	.595			
			.400	-.531	.590	.400	-.505	.596			
			.450	-.516	.595	.450	-.553	.584			
			.500	-.603	.572	.500	-.588	.576			
			.550	-.606	.571	.550	-.592	.575			
			.600	-.547	.585	.600	-.589	.575			
			.650	-.605	.572	.700	-.449	.610			
			.700	-.588	.576	.800	-.281	.652			
			.800	-.374	.629	.900	-.032	.713			
			.900	-.056	.707	.950	.006	.723			
			.950	.055	.735	.990	.011	.724			
			.990	.112	.749						
					LOWER SURFACE						
.100	-1.256	.411	.025	-.670	.556	.025	-.632	.565	.100	-1.647	.314
.300	-.749	.536	.050	-1.255	.400	.050	-1.205	.422	.300	-.786	.527
.600	-.278	.652	.100	-1.436	.363	.100	-1.481	.355	.600	-.424	.641
.800	.090	.743	.200	-1.477	.355	.200	-1.503	.350	.800	.106	.747
			.300	-1.148	.437	.300	-1.472	.357			
			.400	-.679	.553	.400	-.612	.570			
			.500	-.672	.555	.500	-.563	.582			
			.600	-.298	.650	.600	-.324	.641			
			.700	.052	.734	.700	.007	.723			
			.800	.229	.779	.800	.214	.774			
			.900	.321	.803	.900	.257	.785			
			.950	.329	.802	.950	.273	.789			
			1.000	.128	.753						
CA=				-.1746			-.2077				
CM=				-.1315			-.1123				

(e) M = 0.70. Continued.

α = -3.35°

STATION .1532			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.555	.584	0.000	1.102	.554	0.000	.092	.744	.050	-.404	.621
.150	-.637	.564	.012	.308	.797	.012	.226	.777	.150	-.583	.577
.300	-.577	.578	.025	-.140	.686	.025	-.019	.716	.300	-.584	.576
.450	-.454	.609	.050	-.480	.602	.050	-.420	.617	.450	-.531	.590
.600	-.540	.588	.100	-.554	.574	.100	-.516	.593	.600	-.549	.586
.800	-.406	.621	.150	-.584	.567	.150	-.484	.602	.800	-.322	.642
.990	.084	.742	.200	-.628	.565	.200	-.589	.576			
			.300	-.625	.567	.300	-.630	.565			
			.350	-.607	.571	.350	-.582	.577			
			.400	-.611	.570	.400	-.562	.582			
			.450	-.562	.582	.450	-.611	.570			
			.500	-.652	.560	.500	-.646	.562			
			.550	-.647	.561	.550	-.622	.567			
			.600	-.578	.578	.600	-.610	.570			
			.650	-.625	.567	.700	-.445	.611			
			.700	-.579	.578	.800	-.271	.654			
			.800	-.358	.633	.900	-.046	.709			
			.900	-.037	.712	.950	-.026	.715			
			.950	.056	.735	.990	-.013	.718			
			.990	.100	.745						
					LOWER SURFACE						
.100	-.570	.481	.025	-.543	.587	.025	-.391	.625	.100	-1.474	.357
.300	-.786	.527	.050	-1.050	.462	.050	-.994	.475	.300	-.634	.564
.600	-.267	.655	.100	-1.182	.429	.100	-1.318	.399	.600	-.340	.637
.800	.092	.744	.200	-.966	.482	.200	-1.169	.432	.800	.123	.752
			.300	-.866	.507	.300	-.839	.514			
			.400	-.773	.530	.400	-.771	.531			
			.500	-.685	.551	.500	-.628	.566			
			.600	-.277	.653	.600	-.327	.640			
			.700	.045	.733	.700	-.004	.720			
			.800	.169	.763	.800	.219	.775			
			.900	.272	.788	.900	.268	.787			
			.950	.310	.798	.950	.304	.796			
			1.000	.121	.751						
CA=				-.0042			-.0334				
CM=				-.1120			-.1054				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(e) M = 0.70. Continued

$\alpha = -2.50^{\circ}$

STATION .1562			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.556	.574	0.000	1.112	.938	0.000	.089	.743	.050	-.640	.583
.150	-.694	.590	.012	.166	.762	.012	.150	.758	.150	-.663	.557
.300	-.667	.556	.025	-.242	.661	.025	-.247	.660	.300	-.614	.569
.450	-.524	.552	.050	-.055	.554	.050	-.399	.573	.450	-.555	.564
.600	-.566	.561	.100	-.738	.539	.100	-.669	.556	.600	-.559	.533
.800	-.406	.621	.150	-.583	.552	.150	-.608	.571	.900	-.422	.642
.990	.072	.739	.200	-.734	.540	.200	-.663	.557			
			.300	-.676	.554	.300	-.696	.552			
			.250	-.646	.562	.350	-.643	.562			
			.400	-.629	.566	.400	-.611	.570			
			.450	-.618	.559	.450	-.655	.555			
			.500	-.701	.543	.500	-.675	.554			
			.550	-.682	.553	.550	-.656	.559			
			.600	-.623	.567	.600	-.628	.566			
			.650	-.647	.561	.700	-.449	.610			
			.700	-.595	.574	.800	-.271	.654			
			.800	-.363	.631	.900	-.059	.706			
			.900	-.049	.709	.950	-.033	.713			
			.950	.045	.732	.990	-.019	.716			
			.990	.093	.744						
					LOWER SURFACE						
.100	-.754	.525	.025	-.392	.624	.025	-.299	.647	.100	-1.367	.393
.300	-.734	.540	.050	-.840	.514	.050	-.928	.492	.300	-.691	.550
.600	-.279	.652	.100	-1.042	.484	.100	-1.023	.488	.600	-.351	.634
.800	.151	.759	.200	-.533	.491	.200	-.690	.501	.800	.133	.754
			.300	-.645	.512	.300	-.851	.511			
			.400	-.750	.535	.400	-.751	.535			
			.500	-.668	.551	.500	-.627	.566			
			.600	-.277	.653	.600	-.341	.637			
			.700	.057	.735	.700	-.009	.715			
			.800	.204	.772	.800	.227	.777			
			.900	.320	.800	.900	.281	.791			
			.950	.330	.803	.950	.310	.798			
			1.000	.102	.746						
CA=				.0835			.0733				
CM=				-.1154			-.0592				

(e) M = 0.70. Continued.

$\alpha = -1.53^{\circ}$

STATION .1562			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.518	.464	0.000	1.121	.953	0.000	.096	.745	.050	-.452	.511
.150	-.647	.512	.012	.026	.727	.012	-.019	.716	.150	-.763	.532
.300	-.717	.544	.025	-.431	.615	.025	-.341	.637	.300	-.681	.553
.450	-.566	.581	.050	-.863	.503	.050	-.789	.520	.450	-.592	.575
.600	-.564	.577	.100	-.910	.495	.100	-.810	.521	.600	-.502	.582
.800	-.402	.622	.150	-.922	.513	.150	-.714	.545	.800	-.319	.642
.990	.062	.736	.200	-.898	.497	.200	-.781	.528			
			.300	-.770	.531	.300	-.739	.539			
			.350	-.711	.549	.350	-.692	.550			
			.400	-.663	.562	.400	-.660	.558			
			.450	-.664	.557	.450	-.693	.550			
			.500	-.729	.541	.500	-.724	.542			
			.550	-.716	.544	.550	-.689	.551			
			.600	-.653	.560	.600	-.643	.562			
			.650	-.668	.556	.700	-.456	.608			
			.700	-.606	.571	.800	-.271	.654			
			.800	-.362	.632	.900	-.077	.702			
			.900	-.048	.707	.950	-.048	.709			
			.950	.038	.731	.990	-.039	.711			
			.990	.071	.739						
					LOWER SURFACE						
.100	-.667	.551	.025	-.262	.655	.025	-.166	.680	.100	-1.061	.459
.300	-.698	.549	.050	-.648	.561	.050	-.762	.533	.300	-.674	.555
.600	-.280	.652	.100	-.784	.527	.100	-.807	.522	.600	-.357	.633
.800	.162	.761	.200	-.788	.526	.200	-.802	.523	.800	.159	.760
			.300	-.773	.530	.300	-.792	.525			
			.400	-.703	.547	.400	-.720	.543			
			.500	-.665	.557	.500	-.617	.569			
			.600	-.270	.655	.600	-.338	.638			
			.700	.065	.733	.700	.005	.722			
			.800	.220	.776	.800	.276	.769			
			.900	.332	.803	.900	.341	.805			
			.950	.325	.801	.950	.344	.806			
			1.000	.082	.741						
CA=				.2132			.1645				
CM=				-.1110			-.1024				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\alpha = -0.71^{O}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.988	.477	0.000	1.110	.995	0.000	.092	.744	.050	-1.303	.473
.150	-1.002	.474	.012	-.110	.994	.012	-.167	.680	.150	-.965	.483
.300	-.740	.538	.025	-.533	.979	.025	-.446	.611	.300	-.724	.542
.450	-.575	.579	.050	-.365	.478	.050	-.347	.487	.450	-.611	.570
.600	-.567	.576	.100	-1.220	.420	.100	-.961	.484	.600	-.573	.579
.800	-.401	.622	.150	-.516	.495	.150	-.810	.521	.800	-.476	.641
.990	.032	.729	.200	-.543	.493	.200	-.857	.505			
			.300	-.622	.513	.300	-.821	.516			
			.350	-.743	.533	.350	-.737	.535			
			.400	-.735	.540	.400	-.684	.552			
			.450	-.654	.550	.450	-.709	.546			
			.500	-.761	.534	.500	-.730	.541			
			.550	-.730	.541	.550	-.692	.550			
			.600	-.665	.557	.600	-.652	.560			
			.650	-.663	.557	.700	-.453	.605			
			.700	-.573	.580	.800	-.256	.658			
			.800	-.333	.637	.900	-.088	.699			
			.900	-.053	.704	.950	-.006	.706			
			.950	.019	.726	.990	-.049	.705			
			.990	.049	.733						
					LOWER SURFACE						
.100	-.574	.579	.025	-.142	.695	.025	-.040	.711	.100	-.904	.498
.300	-.652	.560	.050	-.490	.593	.050	-.603	.574	.300	-.633	.564
.600	-.309	.645	.100	-.630	.564	.100	-.658	.559	.600	-.506	.611
.800	.187	.767	.200	-.676	.554	.200	-.693	.550	.800	.191	.768
			.300	-.710	.545	.300	-.737	.539			
			.400	-.676	.554	.400	-.691	.550			
			.500	-.652	.560	.500	-.679	.555			
			.600	-.269	.635	.600	-.520	.642			
			.700	.082	.741	.700	.014	.725			
			.800	.232	.773	.800	.280	.790			
			.900	.342	.805	.900	.336	.804			
			.950	.337	.804	.950	.344	.807			
			1.000	.072	.737						
CN=				.3336			.2712				
CM=				-.1056			-.0575				

(e) M = 0.70. Continued

$\alpha = 0.12^{O}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.176	.430	0.000	1.107	.995	0.000	.091	.744	.050	-1.176	.431
.150	-1.255	.401	.012	-.180	.677	.012	-.297	.648	.150	-1.209	.422
.300	-.778	.529	.025	-.716	.344	.025	-.536	.564	.300	-.737	.539
.450	-.623	.567	.050	-1.196	.435	.050	-1.103	.447	.450	-.611	.570
.600	-.554	.575	.100	-1.355	.387	.100	-1.227	.418	.600	-.563	.577
.800	-.377	.628	.150	-1.304	.399	.150	-1.195	.426	.800	-.338	.638
.990	.046	.733	.200	-1.254	.411	.200	-.879	.504			
			.300	-.800	.524	.300	-.868	.507			
			.350	-.756	.535	.350	-.760	.533			
			.400	-.745	.537	.400	-.712	.545			
			.450	-.725	.542	.450	-.724	.542			
			.500	-.702	.548	.500	-.753	.535			
			.550	-.737	.539	.550	-.699	.545			
			.600	-.649	.561	.600	-.561	.565			
			.650	-.671	.555	.700	-.451	.610			
			.700	-.605	.572	.800	-.262	.657			
			.800	-.342	.637	.900	-.089	.699			
			.900	-.049	.709	.950	-.004	.706			
			.950	.029	.728	.990	-.067	.705			
			.990	.062	.737						
					LOWER SURFACE						
.100	-.472	.605	.025	-.010	.717	.025	.120	.751	.100	-.737	.539
.300	-.580	.578	.050	-.355	.633	.050	-.488	.601	.300	-.620	.559
.600	-.253	.649	.100	-.535	.589	.100	-.560	.585	.600	-.367	.631
.800	.189	.768	.200	-.621	.568	.200	-.587	.576	.800	.234	.779
			.300	-.663	.557	.300	-.663	.557			
			.400	-.625	.567	.400	-.641	.563			
			.500	-.630	.566	.500	-.566	.581			
			.600	-.263	.655	.600	-.329	.641			
			.700	.082	.741	.700	.013	.724			
			.800	.253	.784	.800	.275	.794			
			.900	.356	.807	.900	.345	.806			
			.950	.342	.805	.950	.363	.811			
			1.000	.071	.737						
CN=				.4039			.3744				
CM=				-.1019			-.0536				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(e) M = 0.70. Continued.

$\alpha = 1.11^{\circ}$

STATION .1562			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.382	.340	0.000	1.084	.987	0.000	.103	.747	.050	-1.275	.406
.150	-1.482	.355	.012	-.352	.634	.012	-.460	.607	.150	-1.502	.350
.300	-.719	.543	.025	-.864	.508	.025	-.742	.533	.300	-.693	.450
.450	-.636	.564	.050	-1.302	.457	.050	-1.256	.411	.450	-.615	.569
.600	-.603	.572	.100	-1.537	.441	.100	-1.422	.378	.600	-.581	.578
.800	-.369	.622	.150	-1.421	.463	.150	-1.424	.389	.800	-.341	.637
.990	.055	.735	.200	-1.451	.382	.200	-1.382	.388			
			.300	-1.245	.413	.300	-.817	.515			
			.350	-.685	.552	.350	-.685	.552			
			.400	-.651	.503	.400	-.658	.555			
			.450	-.678	.554	.450	-.701	.548			
			.500	-.734	.543	.500	-.749	.536			
			.550	-.726	.542	.550	-.705	.545			
			.600	-.683	.552	.600	-.665	.557			
			.650	-.672	.553	.700	-.674	.604			
			.700	-.665	.572	.850	-.510	.644			
			.800	-.550	.634	.900	-.073	.703			
			.900	-.043	.713	.950	-.034	.713			
			.950	.035	.733	.990	-.022	.716			
			.990	.075	.743						
					LOWER SURFACE						
.100	-.330	.640	.025	.110	.743	.025	.203	.771	.100	-.579	.580
.300	-.531	.550	.050	-.229	.604	.050	-.302	.646	.300	-.576	.579
.600	-.274	.633	.100	-.366	.631	.100	-.426	.616	.600	-.366	.631
.800	.239	.748	.200	-.506	.593	.200	-.491	.606	.800	.248	.762
			.300	-.554	.584	.300	-.593	.575			
			.400	-.575	.574	.400	-.592	.575			
			.500	-.580	.574	.500	-.584	.589			
			.600	-.234	.661	.600	-.307	.645			
			.700	.055	.746	.700	.051	.729			
			.800	.271	.768	.800	.309	.757			
			.900	.376	.814	.900	.350	.808			
			.950	.358	.810	.950	.379	.815			
			1.000	.082	.741						
CN=				.5373			.4889				
CM=				-.0937			-.0883				

(e) M = 0.70. Continued.

$\alpha = 2.02^{\circ}$

STATION .1562			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.453	.367	0.000	1.065	.984	0.000	.091	.744	.050	-1.434	.367
.150	-1.583	.330	.012	-.451	.610	.012	-.549	.586	.150	-1.703	.301
.300	-1.381	.360	.025	-1.037	.468	.025	-.835	.514	.300	-.677	.554
.450	-.611	.570	.050	-1.409	.378	.050	-1.323	.394	.450	-.597	.574
.600	-.590	.575	.100	-1.617	.322	.100	-1.526	.344	.600	-.575	.579
.800	-.393	.624	.150	-1.535	.341	.150	-1.569	.334	.800	-.353	.634
.990	.058	.736	.200	-1.576	.332	.200	-1.506	.349			
			.300	-1.554	.337	.300	-1.542	.340			
			.350	-1.487	.354	.350	-1.105	.448			
			.400	-.662	.553	.400	-.650	.556			
			.450	-.606	.571	.450	-.622	.568			
			.500	-.601	.573	.500	-.672	.555			
			.550	-.656	.557	.550	-.673	.555			
			.600	-.653	.560	.600	-.644	.562			
			.650	-.652	.560	.700	-.674	.604			
			.700	-.581	.573	.800	-.320	.642			
			.800	-.366	.631	.900	-.069	.704			
			.900	-.091	.707	.950	-.026	.714			
			.950	.048	.733	.990	.003	.722			
			.990	.102	.743						
					LOWER SURFACE						
.100	-.191	.674	.025	.200	.773	.025	.342	.806	.100	-.444	.611
.300	-.475	.604	.050	-.084	.701	.050	-.201	.672	.300	-.512	.595
.600	-.269	.655	.100	-.271	.654	.100	-.306	.646	.600	-.354	.634
.800	.233	.779	.200	-.416	.617	.200	-.418	.618	.900	.250	.783
			.300	-.504	.597	.300	-.531	.590			
			.400	-.516	.594	.400	-.561	.583			
			.500	-.543	.587	.500	-.561	.598			
			.600	-.220	.667	.600	-.271	.654			
			.700	.114	.750	.700	.037	.730			
			.800	.263	.783	.800	.329	.802			
			.900	.390	.814	.900	.374	.814			
			.950	.356	.813	.950	.391	.814			
			1.000	.122	.751						
CN=				.6591			.6268				
CM=				-.1091			-.0886				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(e) M = 0.70. Concluded.

$\alpha = 3.83^{\circ}$

STATION .1552			STATION .4265			STATION .7365			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.709	.300	0.000	1.002	.769	0.000	.095	.748	.050	-1.650	.314
.150	-1.790	.280	.012	-.577	.554	.012	-.457	.515	.150	-1.567	.291
.300	-1.636	.317	.025	-1.150	.423	.025	-1.031	.407	.300	-1.966	.339
.450	-.706	.547	.050	-1.988	.333	.050	-1.571	.334	.450	-.615	.570
.600	-.521	.553	.100	-1.806	.279	.100	-1.737	.293	.600	-.540	.588
.800	-.383	.632	.150	-1.771	.285	.150	-1.745	.291	.800	-.369	.641
.990	.067	.738	.200	-1.771	.289	.200	-1.714	.294			
			.300	-1.766	.286	.300	-1.710	.296			
			.350	-1.741	.292	.350	-1.730	.295			
			.400	-1.189	.423	.400	-1.523	.349			
			.450	-1.052	.452	.450	-.989	.477			
			.500	-.549	.544	.500	-.794	.529			
			.550	-.702	.548	.550	-.592	.578			
			.600	-.492	.603	.600	-.544	.587			
			.650	-.457	.604	.700	-.420	.618			
			.700	-.455	.604	.800	-.332	.640			
			.800	-.302	.647	.900	-.083	.701			
			.900	-.073	.704	.950	.001	.722			
			.950	.022	.727	.990	.063	.737			
			.990	.090	.744						
					LOWER SURFACE						
.100	-.055	.708	.025	.406	.422	.025	.524	.681	.100	-.272	.604
.300	-.356	.634	.050	.068	.743	.050	.059	.736	.300	-.436	.614
.600	-.242	.662	.100	-.075	.709	.100	-.130	.650	.600	-.327	.641
.800	.269	.768	.200	-.270	.655	.200	-.270	.655	.800	.206	.768
			.300	-.358	.633	.300	-.401	.623			
			.400	-.421	.614	.400	-.480	.603			
			.500	-.472	.605	.500	-.497	.614			
			.600	-.150	.675	.600	-.245	.661			
			.700	.131	.754	.700	.060	.736			
			.800	.335	.804	.900	.340	.805			
			.900	.424	.820	.980	.332	.818			
			.950	.406	.822	.990	.406	.822			
			1.000	.108	.741						

CN=	.5053	.8542
CM=	-.1026	-.1904

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(f) M = 0.73

α = -5.13°

STATION .1552			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.272	.630	0.000	1.025	.560	0.000	.095	.726	.050	-.255	.634
.150	-.445	.585	.012	.319	.693	.012	-.459	.621	.150	-.425	.570
.300	-.502	.570	.025	.127	.739	.025	.289	.750	.300	-.532	.567
.450	-.404	.595	.050	-.207	.647	.050	-.192	.651	.450	-.525	.594
.600	-.532	.567	.100	-.387	.603	.100	-.314	.619	.600	-.547	.559
.800	-.410	.594	.150	-.439	.587	.150	-.345	.611	.900	-.320	.617
.950	.071	.720	.200	-.465	.576	.200	-.454	.582			
			.300	-.522	.564	.300	-.548	.568			
			.350	-.542	.559	.350	-.541	.559			
			.400	-.545	.558	.400	-.521	.565			
			.450	-.524	.564	.450	-.485	.576			
			.500	-.497	.571	.500	-.439	.585			
			.550	-.439	.584	.550	-.426	.587			
			.600	-.392	.595	.600	-.414	.582			
			.650	-.443	.583	.700	-.436	.588			
			.700	-.369	.599	.800	-.232	.648			
			.800	-.167	.650	.900	-.026	.694			
			.900	-.024	.697	.950	-.007	.699			
			.950	.069	.718	.990	.012	.704			
			.990	.118	.732						
					LOWER SURFACE						
.100	-1.181	.352	.025	-.365	.644	.025	-.526	.583	.100	-1.330	.300
.300	-1.336	.351	.050	-1.179	.592	.050	-1.110	.405	.300	-1.263	.373
.600	-.254	.635	.100	-1.334	.552	.100	-1.358	.345	.600	-.332	.614
.800	.090	.729	.200	-1.383	.539	.200	-1.390	.337	.800	.103	.726
			.300	-1.471	.515	.300	-1.496	.307			
			.400	-1.056	.624	.400	-1.036	.438			
			.500	-.619	.539	.500	-.579	.545			
			.600	-.204	.643	.600	-.247	.636			
			.700	.071	.720	.700	-.035	.692			
			.800	.231	.762	.800	.143	.739			
			.900	.313	.783	.900	.181	.746			
			.950	.309	.782	.950	.219	.759			
			1.000	.116	.732						
CN=				-.1931			-.2246				
CM=				-.1280			-.0929				

(f) M = 0.73. Continued.

α = -3.40°

STATION .1552			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.528	.560	0.000	1.119	.554	0.000	.074	.726	.050	-.460	.581
.150	-.640	.534	.012	.330	.704	.012	.279	.774	.150	-.510	.562
.300	-.624	.534	.025	-.126	.661	.025	-.024	.659	.300	-.616	.540
.450	-.490	.573	.050	-.463	.587	.050	-.300	.570	.450	-.557	.555
.600	-.565	.554	.100	-.571	.552	.100	-.561	.554	.600	-.557	.555
.800	-.401	.596	.150	-.616	.540	.150	-.585	.547	.800	-.306	.621
.950	.076	.721	.200	-.672	.529	.200	-.616	.540			
			.300	-.686	.527	.300	-.663	.527			
			.350	-.643	.535	.350	-.627	.537			
			.400	-.621	.539	.400	-.597	.545			
			.450	-.583	.547	.450	-.555	.550			
			.500	-.728	.511	.500	-.709	.515			
			.550	-.707	.515	.550	-.678	.524			
			.600	-.671	.523	.600	-.642	.533			
			.650	-.669	.525	.700	-.440	.590			
			.700	-.557	.549	.800	-.235	.640			
			.800	-.347	.610	.900	-.053	.687			
			.900	-.035	.672	.950	-.042	.650			
			.950	.053	.715	.990	-.025	.695			
			.990	.093	.726						
					LOWER SURFACE						
.100	-.895	.467	.025	-.442	.589	.025	-.334	.614	.100	-1.055	.440
.300	-.956	.449	.050	-.552	.441	.050	-.315	.462	.300	-.873	.473
.600	-.265	.632	.100	-1.144	.401	.100	-1.236	.377	.600	-.443	.610
.800	.059	.727	.200	-1.195	.388	.200	-1.244	.375	.800	.167	.745
			.300	-1.235	.379	.300	-1.302	.360			
			.400	-.666	.529	.400	-.836	.462			
			.500	-.643	.534	.500	-.509	.555			
			.600	-.277	.627	.600	-.299	.623			
			.700	.060	.717	.700	.021	.707			
			.800	.236	.761	.800	.249	.746			
			.900	.335	.790	.900	.309	.762			
			.950	.339	.793	.950	.326	.767			
			1.000	.095	.726						
CN=				-.0057			-.0356				
CM=				-.1270			-.1110				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

α = -2.44°

STATION .1532			STATION .4245			STATION .7325			STATION .9325		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.675	.524	0.000	1.161	.731	0.000	.106	.763	.050	-.057	.594
.150	-.754	.504	.012	.228	.701	.012	.120	.727	.150	-.177	.581
.300	-.667	.526	.025	-.234	.640	.025	-.148	.652	.300	-.271	.575
.450	-.522	.562	.050	-.626	.547	.050	-.393	.566	.450	-.304	.563
.600	-.378	.550	.100	-.683	.522	.100	-.457	.547	.600	-.376	.550
.800	-.371	.604	.150	-.704	.517	.150	-.442	.553	.750	-.332	.622
.990	.059	.717	.200	-.724	.505	.200	-.411	.545			
			.300	-.770	.493	.300	-.755	.503			
			.350	-.691	.523	.350	-.675	.524			
			.400	-.678	.523	.400	-.637	.534			
			.450	-.640	.534	.450	-.607	.515			
			.500	-.761	.502	.500	-.744	.509			
			.550	-.741	.507	.550	-.707	.515			
			.600	-.640	.533	.600	-.651	.550			
			.650	-.556	.551	.700	-.542	.585			
			.700	-.592	.545	.800	-.244	.637			
			.800	-.348	.612	.900	-.096	.686			
			.900	-.041	.693	.950	-.044	.650			
			.950	.049	.716	.990	-.043	.655			
			.975	.073	.720						
					LOWER SURFACE						
.100	-.822	.486	.025	-.527	.615	.025	-.243	.635	.100	-1.216	.353
.300	-.517	.461	.050	-.825	.464	.050	-.406	.496	.300	-.913	.543
.600	-.268	.631	.100	-1.003	.433	.100	-1.079	.416	.600	-.364	.605
.800	.105	.729	.200	-.979	.443	.200	-1.081	.415	.900	.140	.744
			.300	-1.003	.438	.300	-1.115	.407			
			.400	-.784	.501	.400	-.965	.527			
			.500	-.694	.519	.500	-.930	.535			
			.600	-.257	.634	.600	-.314	.615			
			.700	.063	.713	.700	.016	.709			
			.800	.151	.751	.800	.260	.765			
			.900	.309	.782	.900	.317	.754			
			.950	.335	.787	.950	.334	.756			
			1.000	.062	.723						
CN=				.6900			.6402				
CM=				-.1187			-.1063				

(f) M = 0.73. Continued.

α = -1.62°

STATION .1532			STATION .4245			STATION .7325			STATION .9325		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.823	.466	0.000	1.106	.692	0.000	.097	.727	.050	-.003	.671
.150	-.562	.449	.012	.112	.733	.012	.032	.710	.150	-.244	.575
.300	-.760	.502	.025	-.346	.611	.025	-.274	.625	.300	-.775	.434
.450	-.603	.543	.050	-.741	.507	.050	-.496	.494	.450	-.585	.543
.600	-.552	.546	.100	-.550	.492	.100	-.414	.488	.600	-.478	.550
.800	-.363	.606	.150	-.751	.506	.150	-.740	.506	.900	-.223	.625
.990	.048	.714	.200	-.802	.495	.200	-.797	.493			
			.300	-.801	.491	.300	-.805	.470			
			.350	-.733	.507	.350	-.744	.506			
			.400	-.694	.519	.400	-.664	.527			
			.450	-.666	.525	.450	-.719	.515			
			.500	-.758	.492	.500	-.775	.498			
			.550	-.778	.497	.550	-.740	.508			
			.600	-.650	.531	.600	-.657	.529			
			.650	-.661	.523	.700	-.543	.585			
			.700	-.586	.543	.800	-.245	.637			
			.800	-.320	.617	.900	-.067	.684			
			.900	-.045	.689	.950	-.041	.650			
			.950	.032	.710	.990	-.043	.650			
			.990	.067	.719						
					LOWER SURFACE						
.100	-.668	.526	.025	-.420	.644	.025	-.149	.662	.100	-1.134	.404
.300	-.761	.502	.050	-.553	.511	.050	-.719	.513	.300	-.931	.520
.600	-.280	.628	.100	-.906	.493	.100	-1.009	.437	.600	-.455	.607
.800	.078	.722	.200	-.864	.479	.200	-.897	.466	.800	.141	.735
			.300	-.863	.473	.300	-1.011	.436			
			.400	-.784	.495	.400	-.882	.523			
			.500	-.689	.521	.500	-.849	.531			
			.600	-.256	.634	.600	-.323	.617			
			.700	.069	.713	.700	.008	.702			
			.800	.154	.752	.800	.258	.765			
			.900	.316	.784	.900	.320	.785			
			.950	.327	.787	.950	.337	.785			
			1.000	.066	.724						
CN=				.1855			.1559				
CM=				-.1096			-.1029				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(f) M = 0.73. Continued.

α = -0.61°

STATION .1552			STATION .4242			STATION .7323			STATION .9525		
X/C	CP	P/PITOT	X/C	CP	P/PITOT	X/C	CP	P/PITOT	X/C	CP	P/PITOT
					UPPER SURFACE						
.050	-.581	.451	0.000	1.122	.959	0.000	-.952	.729	.050	-.734	.697
.150	-1.163	.411	.012	-.314	.807	.012	-.104	.687	.150	-1.152	.496
.300	-.624	.468	.025	-.031	.832	.025	-.454	.586	.300	-.743	.636
.450	-.623	.530	.050	-.040	.899	.050	-.714	.662	.450	-.635	.914
.600	-.595	.599	.100	-1.162	.857	.100	-1.074	.620	.600	-.605	.942
.800	-.377	.603	.150	-1.119	.913	.150	-1.040	.629	.800	-.277	.923
.950	.055	.719	.200	-1.107	.911	.200	-1.035	.638			
			.300	-1.032	.931	.300	-.980	.656			
			.400	-.744	.907	.350	-.756	.695			
			.450	-.631	.933	.400	-.681	.924			
			.497	-.599	.911	.450	-.730	.916			
			.500	-.620	.907	.500	-.770	.936			
			.550	-.773	.941	.550	-.747	.909			
			.600	-.693	.924	.600	-.708	.927			
			.650	-.689	.926	.700	-.698	.885			
			.700	-.595	.940	.800	-.264	.856			
			.800	-.526	.918	.900	-.062	.884			
			.900	-.048	.878	.950	-.052	.888			
			.950	.029	.711	.990	-.055	.887			
			.990	.057	.713						
					LOWER SURFACE						
.100	-.581	.549	.029	-.351	.877	.029	-.326	.705	.100	-.702	.643
.300	-.675	.535	.050	-.000	.871	.050	-.296	.696	.300	-.958	.922
.600	-.274	.630	.100	-.034	.933	.100	-.007	.727	.600	-.382	.936
.800	.150	.741	.200	-.756	.933	.200	-.769	.901	.900	.191	.794
			.300	-.781	.947	.300	-.975	.972			
			.400	-.767	.915	.400	-.714	.914			
			.500	-.688	.922	.500	-.643	.938			
			.600	-.764	.932	.600	-.369	.918			
			.700	.073	.762	.700	.011	.704			
			.800	.224	.784	.800	.276	.774			
			.900	.342	.771	.900	.391	.751			
			.950	.333	.756	.950	.446	.752			
			1.000	.081	.722						
CN=				.3147			.2552				
CM=				-.1034			-.0541				

(f) M = 0.73. Continued.

α = 0.35°

STATION .1552			STATION .4242			STATION .7323			STATION .9525		
X/C	CP	P/PITOT	X/C	CP	P/PITOT	X/C	CP	P/PITOT	X/C	CP	P/PITOT
					UPPER SURFACE						
.050	-1.082	.415	0.000	1.111	.992	0.000	-.954	.720	.050	-1.030	.417
.150	-1.279	.387	.012	-.159	.867	.012	-.265	.672	.150	-1.133	.447
.300	-.116	.409	.025	-.032	.891	.025	-.514	.667	.300	-.998	.545
.450	-.590	.547	.050	-1.084	.925	.050	-1.054	.725	.450	-.621	.833
.600	-.593	.596	.100	-1.263	.897	.100	-1.223	.677	.600	-.900	.944
.800	-.374	.602	.150	-1.264	.879	.150	-1.210	.634	.800	-.309	.921
.990	.058	.716	.200	-1.265	.870	.200	-1.160	.652			
			.300	-1.253	.873	.300	-1.215	.664			
			.350	-1.267	.870	.350	-1.247	.675			
			.400	-1.262	.871	.400	-1.157	.687			
			.450	-.665	.927	.450	-.869	.729			
			.500	-.630	.939	.500	-.695	.819			
			.550	-.614	.941	.550	-.557	.822			
			.600	-.693	.929	.600	-.530	.934			
			.650	-.695	.917	.700	-.442	.820			
			.700	-.584	.943	.800	-.275	.824			
			.800	-.526	.913	.900	-.069	.884			
			.900	-.034	.872	.950	-.055	.882			
			.950	.048	.713	.990	-.110	.918			
			.990	.068	.722						
					LOWER SURFACE						
.100	-.428	.589	.029	.039	.741	.029	-.133	.722	.100	-.600	.692
.300	-.660	.544	.050	-.388	.893	.050	-.436	.695	.300	-.647	.832
.600	-.262	.624	.100	-.537	.881	.100	-.344	.697	.600	-.364	.896
.800	.191	.751	.200	-.627	.835	.200	-.630	.696	.900	.229	.761
			.300	-.675	.824	.300	-.716	.813			
			.400	-.650	.841	.400	-.680	.823			
			.500	-.644	.838	.500	-.613	.841			
			.600	-.246	.833	.600	-.313	.811			
			.700	.031	.763	.700	.027	.704			
			.800	.267	.771	.800	.299	.730			
			.900	.353	.774	.900	.366	.756			
			.950	.360	.760	.950	.370	.753			
			1.000	.054	.725						
CN=				.4937			.4434				
CM=				-.1054			-.0544				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(f) $M_\infty = 0.73$. Concluded.

$\alpha = 1.42^\circ$

STATION .1952			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.241	.376	0.000	1.105	.991	0.000	.079	.727	.050	-1.209	.345
.150	-1.407	.333	.012	-.245	.625	.012	-.376	.603	.150	-1.529	.301
.300	-1.300	.361	.025	-.753	.504	.025	-.623	.529	.300	-1.346	.349
.450	-.662	.528	.050	-1.170	.365	.050	-1.143	.402	.450	-.806	.542
.600	-.535	.560	.100	-1.407	.332	.100	-1.320	.355	.600	-.571	.551
.800	-.373	.603	.150	-1.386	.333	.150	-1.353	.347	.800	-.294	.624
.990	.083	.723	.200	-1.409	.332	.200	-1.322	.355			
			.300	-1.385	.339	.300	-1.358	.345			
			.350	-1.393	.336	.350	-1.362	.344			
			.400	-1.386	.338	.400	-1.339	.350			
			.450	-1.347	.349	.450	-1.382	.339			
			.500	-.930	.464	.500	-.737	.504			
			.550	-.658	.529	.550	-.623	.534			
			.600	-.540	.559	.600	-.563	.554			
			.650	-.538	.559	.700	-.420	.591			
			.700	-.508	.588	.800	-.290	.625			
			.800	-.322	.617	.900	-.054	.687			
			.900	-.042	.697	.950	.007	.703			
			.950	.058	.716	.990	.021	.707			
			.990	.115	.731						
					LOWER SURFACE						
.100	-.297	.623	.025	.125	.734	.025	.265	.771	.100	-.572	.591
.300	-.535	.561	.050	-.155	.659	.050	-.288	.625	.300	-.597	.545
.600	-.254	.635	.100	-.362	.606	.100	-.419	.551	.600	-.362	.596
.800	.211	.756	.200	-.508	.548	.200	-.533	.501	.800	.242	.735
			.300	-.587	.547	.300	-.635	.535			
			.400	-.589	.547	.400	-.632	.536			
			.500	-.604	.543	.500	-.548	.557			
			.600	-.221	.643	.600	-.289	.625			
			.700	.117	.732	.700	.045	.713			
			.800	.252	.773	.800	.325	.780			
			.900	.386	.802	.900	.475	.795			
			.950	.373	.793	.950	.396	.800			
			1.000	.126	.734						
CN=				.5581			.5623				
CM=				-.1066			-.1000				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(g) M = 0.75

α = -5.06°

STATION .1562			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.276	.613	0.000	1.113	.953	0.000	.096	.712	.050	-.225	.627
.150	-.464	.597	.012	.634	.848	.012	.450	.811	.150	-.484	.596
.300	-.634	.568	.025	.097	.719	.025	.105	.733	.300	-.657	.547
.450	-.622	.574	.050	-.237	.624	.050	-.216	.630	.450	-.692	.539
.600	-.554	.586	.100	-.572	.567	.100	-.523	.601	.600	-.589	.529
.800	-.252	.652	.150	-.459	.564	.150	-.347	.954	.800	-.320	.601
.950	.072	.703	.200	-.535	.548	.200	-.469	.550			
			.300	-.550	.533	.300	-.569	.529			
			.350	-.555	.537	.350	-.550	.539			
			.400	-.572	.534	.400	-.541	.542			
			.450	-.533	.544	.450	-.521	.520			
			.500	-.712	.495	.500	-.649	.502			
			.550	-.704	.498	.550	-.714	.495			
			.600	-.575	.532	.600	-.645	.512			
			.650	-.701	.494	.700	-.446	.587			
			.700	-.581	.551	.800	-.200	.634			
			.800	-.265	.603	.900	-.053	.674			
			.900	-.034	.677	.950	-.014	.689			
			.950	.061	.709	.990	.007	.695			
			.990	.102	.716						
					LOWER SURFACE						
.100	-.557	.616	.025	-.554	.593	.025	-.436	.670	.100	-1.414	.305
.300	-1.339	.525	.050	-1.078	.336	.050	-1.007	.415	.300	-1.362	.314
.600	-.276	.614	.100	-1.227	.355	.100	-1.235	.337	.600	-.360	.565
.800	.033	.657	.200	-1.321	.333	.200	-1.343	.324	.900	.056	.703
			.300	-1.139	.377	.300	-1.431	.300			
			.400	-.737	.481	.400	-1.223	.357			
			.500	-.664	.503	.500	-.547	.535			
			.600	-.451	.569	.600	-.306	.605			
			.700	-.249	.622	.700	-.193	.636			
			.800	.017	.693	.800	-.096	.662			
			.900	.166	.733	.900	.058	.704			
			.950	.142	.727	.950	.104	.716			
			1.000	.107	.717						
CA=				-.1923			-.2035				
CM=				-.0810			-.0819				

(g) M = 0.75. Continued.

α = -3.51°

STATION .1562			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.454	.565	0.000	1.126	.952	0.000	.095	.714	.050	-.453	.567
.150	-.660	.526	.012	.617	.774	.012	.234	.708	.150	-.599	.526
.300	-.632	.517	.025	-.096	.652	.025	-.003	.666	.300	-.654	.511
.450	-.490	.594	.050	-.415	.578	.050	-.332	.952	.450	-.983	.931
.600	-.564	.534	.100	-.547	.543	.100	-.533	.544	.600	-.592	.526
.800	-.268	.595	.150	-.581	.531	.150	-.522	.547	.800	-.290	.608
.950	.060	.703	.200	-.711	.493	.200	-.629	.916			
			.300	-.709	.495	.300	-.676	.605			
			.350	-.626	.519	.350	-.646	.613			
			.400	-.642	.514	.400	-.607	.624			
			.450	-.609	.523	.450	-.670	.907			
			.500	-.769	.481	.500	-.727	.491			
			.550	-.760	.482	.550	-.811	.468			
			.600	-.614	.522	.600	-.654	.511			
			.650	-.644	.511	.700	-.423	.574			
			.700	-.570	.534	.800	-.229	.622			
			.800	-.313	.604	.900	-.052	.674			
			.900	-.020	.648	.950	-.030	.690			
			.950	.055	.705	.990	-.023	.692			
			.990	.095	.712						
					LOWER SURFACE						
.100	-.887	.455	.025	-.468	.573	.025	-.305	.680	.100	-1.274	.341
.300	-1.141	.379	.050	-.696	.429	.050	-.868	.455	.300	-1.334	.326
.600	-.232	.626	.100	-1.116	.365	.100	-1.146	.378	.600	-.353	.591
.800	.059	.707	.200	-1.175	.373	.200	-1.213	.359	.900	.173	.737
			.300	-1.253	.349	.300	-1.263	.340			
			.400	-1.322	.333	.400	-1.388	.312			
			.500	-.551	.519	.500	-.693	.511			
			.600	-.219	.629	.600	-.247	.622			
			.700	.054	.703	.700	.013	.692			
			.800	.220	.750	.800	.210	.745			
			.900	.329	.777	.900	.261	.755			
			.950	.321	.775	.950	.321	.776			
			1.000	.109	.713						
CA=				-.0502			-.0625				
CM=				-.1103			-.0580				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(g) M = 0.75. Continued.

α = -2.60°

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.608	.523	0.000	1.125	.334	0.000	.101	.716	.050	-.630	.517
.150	-.797	.472	.012	.255	.759	.012	.152	.730	.150	-.728	.491
.300	-.696	.501	.025	-.200	.634	.025	-.109	.659	.300	-.543	.466
.450	-.540	.542	.050	-.559	.537	.050	-.585	.536	.450	-.606	.524
.600	-.582	.531	.100	-.806	.470	.100	-.632	.517	.600	-.559	.525
.800	-.346	.594	.150	-.659	.510	.150	-.617	.521	.800	-.254	.608
.990	.056	.704	.200	-.806	.473	.200	-.713	.495			
			.300	-.792	.474	.300	-.822	.485			
			.350	-.773	.473	.350	-.829	.483			
			.400	-.661	.503	.400	-.814	.522			
			.450	-.615	.523	.450	-.682	.502			
			.500	-.781	.476	.500	-.749	.485			
			.550	-.628	.504	.550	-.825	.485			
			.600	-.647	.513	.600	-.719	.493			
			.650	-.639	.515	.700	-.419	.575			
			.700	-.557	.537	.800	-.224	.622			
			.800	-.310	.604	.900	-.066	.670			
			.900	-.019	.683	.950	-.037	.676			
			.950	.041	.699	.990	-.026	.681			
			.990	.075	.709						
					LOWER SURFACE						
.100	-.732	.490	.025	-.407	.605	.025	-.190	.637	.100	-1.220	.357
.300	-1.033	.408	.050	-.786	.475	.050	-.766	.475	.300	-1.263	.346
.600	-.223	.628	.100	-.948	.431	.100	-1.062	.395	.600	-.361	.591
.800	.059	.715	.200	-1.066	.399	.200	-1.069	.398	.900	.181	.737
			.300	-1.059	.399	.300	-1.162	.373			
			.400	-1.153	.375	.400	-1.269	.344			
			.500	-.549	.540	.500	-.465	.557			
			.600	-.224	.623	.600	-.251	.620			
			.700	.054	.703	.700	.021	.674			
			.800	.213	.745	.800	.264	.760			
			.900	.316	.774	.900	.315	.775			
			.950	.329	.778	.950	.332	.778			
			1.000	.080	.710						
CN=				.0635			.0436				
CM=				-.1134			-.1071				

(g) M = 0.75. Continued.

α = -1.63°

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.773	.475	0.000	1.132	.335	0.000	.090	.713	.050	-.722	.493
.150	-.561	.428	.012	.138	.723	.012	.074	.708	.150	-.783	.472
.300	-.689	.501	.025	-.266	.611	.025	-.260	.615	.300	-.634	.461
.450	-.574	.533	.050	-.755	.486	.050	-.707	.497	.450	-.632	.517
.600	-.585	.530	.100	-.556	.429	.100	-.632	.463	.600	-.604	.525
.800	-.364	.590	.150	-.656	.495	.150	-.799	.472	.800	-.281	.612
.990	.059	.705	.200	-.665	.494	.200	-.761	.482			
			.300	-.539	.494	.300	-.930	.436			
			.350	-.851	.497	.350	-.868	.448			
			.400	-.756	.483	.400	-.870	.453			
			.450	-.658	.513	.450	-.758	.483			
			.500	-.771	.477	.500	-.710	.496			
			.550	-.795	.473	.550	-.776	.478			
			.600	-.679	.504	.600	-.681	.504			
			.650	-.637	.516	.700	-.415	.576			
			.700	-.551	.539	.800	-.232	.626			
			.800	-.281	.612	.900	-.067	.676			
			.900	-.028	.681	.950	-.047	.676			
			.950	.051	.702	.990	-.051	.675			
			.990	.059	.704						
					LOWER SURFACE						
.100	-.571	.533	.025	-.212	.631	.025	-.112	.658	.100	-1.102	.380
.300	-.563	.427	.050	-.636	.515	.050	-.647	.513	.300	-.706	.497
.600	-.237	.624	.100	-.821	.466	.100	-.911	.441	.600	-.349	.594
.800	.058	.704	.200	-.921	.439	.200	-.902	.444	.800	.157	.731
			.300	-.966	.426	.300	-1.053	.403			
			.400	-1.042	.405	.400	-1.165	.373			
			.500	-.622	.520	.500	-.546	.540			
			.600	-.233	.625	.600	-.298	.607			
			.700	.077	.709	.700	.027	.696			
			.800	.210	.745	.800	.272	.762			
			.900	.314	.774	.900	.330	.778			
			.950	.335	.779	.950	.336	.779			
			1.000	.080	.710						
CN=				.1693			.1476				
CM=				-.1067			-.1005				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(g) M = 0.75. Continued.

$\alpha = -0.55^{\circ}$

STATION .1952			STATION .4249			STATION .7329			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.548	.481	0.000	1.126	.934	0.000	.106	.717	.050	-.873	.452
.150	-1.096	.351	.012	.031	.697	.012	-.081	.667	.150	-1.214	.358
.300	-1.001	.417	.025	-.460	.564	.025	-.355	.592	.300	-.711	.496
.450	-.672	.506	.050	-.866	.494	.050	-.658	.496	.450	-.643	.514
.600	-.578	.532	.100	-1.115	.383	.100	-1.010	.415	.600	-.604	.524
.800	-.355	.532	.150	-1.066	.337	.150	-1.024	.411	.800	-.298	.610
.990	.066	.700	.200	-1.066	.334	.200	-1.001	.417			
			.300	-1.114	.386	.300	-1.035	.405			
			.350	-1.064	.399	.350	-1.098	.351			
			.400	-1.091	.393	.400	-1.086	.394			
			.450	-1.021	.412	.450	-1.023	.411			
			.500	-.756	.483	.500	-.744	.487			
			.550	-.611	.523	.550	-.682	.504			
			.600	-.586	.533	.600	-.614	.522			
			.650	-.641	.515	.700	-.412	.577			
			.700	-.536	.543	.800	-.230	.626			
			.800	-.310	.609	.900	-.055	.674			
			.900	-.035	.677	.950	-.051	.675			
			.950	.059	.708	.990	-.029	.681			
			.990	.066	.707						
					LOWER SURFACE						
.100	-.460	.564	.025	-.064	.905	.025	.052	.703	.100	-.771	.425
.300	-.725	.492	.050	-.915	.947	.050	-.950	.540	.300	-.988	.503
.600	-.248	.621	.100	-.857	.913	.100	-.676	.505	.600	-.342	.596
.800	.059	.715	.200	-.785	.879	.200	-.640	.481	.800	.177	.737
			.300	-.815	.868	.300	-.936	.435			
			.400	-.805	.877	.400	-.761	.482			
			.500	-.711	.873	.500	-.623	.520			
			.600	-.243	.824	.600	-.294	.609			
			.700	.087	.772	.700	.026	.696			
			.800	.241	.756	.800	.282	.765			
			.900	.335	.773	.900	.344	.782			
			.950	.346	.782	.950	.359	.786			
			1.000	.108	.718						
CA=				.3201			.3108				
CM=				-.1045			-.0991				

(g) M = 0.75. Continued.

$\alpha = 0.52^{\circ}$

STATION .1952			STATION .4249			STATION .7329			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.043	.406	0.000	1.125	.954	0.000	.106	.717	.050	-1.007	.416
.150	-1.267	.349	.012	-.095	.662	.012	-.212	.631	.150	-1.330	.328
.300	-1.176	.370	.025	-.604	.524	.025	-.481	.559	.300	-1.229	.355
.450	-1.056	.391	.050	-.355	.419	.050	-.389	.420	.450	-.671	.507
.600	-.522	.547	.100	-1.240	.451	.100	-1.153	.376	.600	-.590	.524
.800	-.255	.552	.150	-1.215	.359	.150	-1.162	.375	.800	-.206	.611
.990	.066	.710	.200	-1.248	.353	.200	-1.132	.382			
			.300	-1.222	.397	.300	-1.195	.365			
			.350	-1.220	.384	.350	-1.242	.352			
			.400	-1.244	.391	.400	-1.202	.363			
			.450	-1.203	.362	.450	-1.290	.329			
			.500	-1.262	.346	.500	-1.272	.344			
			.550	-.753	.484	.550	-.760	.482			
			.600	-.586	.533	.600	-.587	.529			
			.650	-.510	.551	.700	-.396	.581			
			.700	-.457	.563	.800	-.262	.617			
			.800	-.292	.603	.900	-.057	.673			
			.900	-.044	.675	.950	-.006	.686			
			.950	.050	.702	.990	-.010	.686			
			.990	.106	.714						
					LOWER SURFACE						
.100	-.282	.612	.025	.017	.967	.025	.107	.718	.100	-.704	.498
.300	-.603	.525	.050	-.836	.967	.050	-.595	.551	.300	-.712	.495
.600	-.252	.620	.100	-.915	.949	.100	-.592	.533	.600	-.556	.592
.800	.198	.739	.200	-.647	.913	.200	-.653	.511	.800	.228	.750
			.300	-.722	.891	.300	-.845	.459			
			.400	-.717	.894	.400	-.688	.504			
			.500	-.676	.905	.500	-.638	.515			
			.600	-.233	.862	.600	-.293	.627			
			.700	.101	.715	.700	.034	.688			
			.800	.254	.734	.800	.295	.762			
			.900	.365	.767	.900	.352	.764			
			.950	.364	.767	.950	.384	.793			
			1.000	.103	.717						
CA=				.4772			.4666				
CM=				-.1165			-.1064				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(g) M = 0.75. Concluded.

$\alpha = 1.31^{\circ}$

STATION .1592			STATION .4245			STATION .7369			STATION .9025		
x/c	CP	P/PTINF	x/c	CP	P/PTINF	x/c	CP	P/PTINF	x/c	CP	P/PTINF
					UPPER SURFACE						
.050	-1.135	.382	0.000	1.115	.451	0.000	.103	.719	.050	-1.110	.389
.150	-1.258	.333	.012	-.131	.637	.012	-.291	.610	.150	-1.497	.311
.300	-1.270	.346	.025	-.552	.502	.025	-.549	.541	.300	-1.412	.337
.450	-1.132	.383	.050	-1.064	.401	.050	-1.074	.399	.450	-.691	.502
.600	-.901	.454	.100	-1.304	.338	.100	-1.232	.356	.600	-.579	.532
.800	-.357	.592	.150	-1.278	.343	.150	-1.252	.350	.800	-.262	.613
.990	.088	.713	.200	-1.305	.335	.200	-1.251	.351			
			.300	-1.309	.335	.300	-1.295	.339			
			.250	-1.333	.328	.350	-1.296	.339			
			.400	-1.313	.334	.400	-1.274	.344			
			.450	-1.271	.345	.450	-1.355	.322			
			.500	-1.265	.347	.500	-1.365	.320			
			.550	-.788	.476	.550	-.810	.470			
			.600	-.676	.506	.600	-.646	.514			
			.650	-.526	.547	.700	-.406	.575			
			.700	-.453	.567	.800	-.295	.612			
			.800	-.237	.625	.900	-.071	.670			
			.900	-.060	.673	.950	-.006	.688			
			.950	.021	.695	.990	.014	.693			
			.990	.021	.695						
					LOWER SURFACE						
.100	-.233	.626	.025	.134	.725	.025	.252	.759	.100	-.627	.520
.300	-.578	.533	.050	-.230	.627	.050	-.295	.606	.300	-.437	.517
.600	-.278	.614	.100	-.401	.581	.100	-.476	.560	.600	-.365	.570
.800	.152	.730	.200	-.566	.535	.200	-.586	.531	.800	.237	.753
			.300	-.652	.513	.300	-.777	.478			
			.400	-.661	.510	.400	-.685	.504			
			.500	-.640	.515	.500	-.626	.516			
			.600	-.228	.623	.600	-.302	.607			
			.700	.113	.723	.700	.033	.652			
			.800	.266	.761	.800	.311	.733			
			.900	.374	.790	.900	.461	.787			
			.950	.345	.781	.950	.392	.755			
			1.000	.078	.710						
CA=				.5577			.5536				
CM=				-.1117			-.1055				

[redacted]

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(h) M = 0.76

$\alpha = -4.39^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.342	.587	0.000	1.129	.993	0.000	.109	.712	.050	-.353	.584
.150	-.560	.527	.012	.457	.804	.012	.405	.753	.150	-.534	.533
.300	-.606	.514	.025	.043	.653	.025	.086	.705	.300	-.641	.504
.450	-.483	.548	.050	-.215	.555	.050	-.342	.587	.450	-.569	.524
.600	-.569	.525	.100	-.448	.553	.100	-.416	.567	.600	-.636	.506
.800	-.361	.582	.150	-.525	.537	.150	-.426	.563	.800	-.310	.576
.990	.062	.639	.200	-.597	.517	.200	-.540	.532			
			.300	-.630	.504	.300	-.636	.506			
			.350	-.604	.513	.350	-.612	.512			
			.400	-.556	.517	.400	-.597	.517			
			.450	-.568	.525	.450	-.641	.505			
			.500	-.757	.473	.500	-.717	.464			
			.550	-.735	.482	.550	-.796	.461			
			.600	-.616	.511	.600	-.762	.471			
			.650	-.694	.501	.700	-.421	.565			
			.700	-.575	.523	.800	-.180	.632			
			.800	-.291	.601	.900	-.019	.676			
			.900	-.016	.677	.950	-.017	.677			
			.950	.049	.653	.990	-.005	.660			
			.990	.090	.706						
					LOWER SURFACE						
.100	-.901	.433	.025	-.429	.568	.025	-.351	.585	.100	-1.318	.319
.300	-1.243	.338	.050	-.579	.411	.050	-.934	.424	.300	-1.385	.299
.600	-.272	.607	.100	-1.127	.373	.100	-1.187	.354	.600	-.362	.541
.800	.022	.664	.200	-1.211	.347	.200	-1.252	.336	.800	.122	.715
			.300	-1.245	.334	.300	-1.341	.311			
			.400	-.649	.502	.400	-.707	.458			
			.500	-.578	.522	.500	-.645	.503			
			.600	-.406	.569	.600	-.336	.599			
			.700	-.330	.590	.700	-.341	.587			
			.800	-.125	.647	.800	-.092	.656			
			.900	.107	.711	.900	-.051	.667			
			.950	.132	.718	.950	.156	.725			
			1.000	.117	.714						
CN=				-.1535			-.1725				
CM=				-.0653			-.0544				

(h) M = 0.76. Continued.

$\alpha = -3.54^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.416	.566	0.000	1.127	.993	0.000	.104	.710	.050	-.407	.552
.150	-.606	.497	.012	.350	.778	.012	.285	.760	.150	-.631	.507
.300	-.675	.495	.025	-.053	.667	.025	-.012	.678	.300	-.760	.471
.450	-.504	.542	.050	-.435	.581	.050	-.424	.563	.450	-.576	.522
.600	-.571	.524	.100	-.571	.524	.100	-.539	.532	.600	-.621	.510
.800	-.348	.585	.150	-.568	.524	.150	-.519	.539	.800	-.300	.578
.990	.068	.700	.200	-.735	.479	.200	-.623	.509			
			.300	-.757	.472	.300	-.760	.471			
			.350	-.678	.494	.350	-.720	.482			
			.400	-.620	.510	.400	-.550	.518			
			.450	-.564	.520	.450	-.663	.496			
			.500	-.763	.471	.500	-.730	.480			
			.550	-.826	.453	.550	-.847	.447			
			.600	-.645	.503	.600	-.767	.469			
			.650	-.692	.501	.700	-.402	.570			
			.700	-.552	.529	.800	-.167	.635			
			.800	-.276	.605	.900	-.037	.671			
			.900	-.002	.681	.950	-.021	.675			
			.950	.062	.699	.990	-.011	.678			
			.990	.088	.705						
					LOWER SURFACE						
.100	-.820	.455	.025	-.347	.586	.025	-.269	.607	.100	-1.265	.332
.300	-1.150	.384	.050	-.688	.496	.050	-.820	.455	.300	-1.344	.310
.600	-.288	.602	.100	-1.052	.391	.100	-1.118	.372	.600	-.352	.584
.800	.047	.653	.200	-1.144	.365	.200	-1.154	.363	.800	.165	.727
			.300	-1.228	.342	.300	-1.252	.335			
			.400	-.703	.487	.400	-.835	.451			
			.500	-.527	.533	.500	-.589	.519			
			.600	-.448	.558	.600	-.442	.555			
			.700	-.244	.614	.700	-.171	.634			
			.800	-.185	.630	.800	.049	.695			
			.900	.185	.732	.900	.115	.713			
			.950	.166	.727	.950	.136	.719			
			1.000	.108	.711						
CN=				-.0867			-.0834				
CM=				-.0640			-.0830				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\alpha = -2.65^{o}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.601	.516	0.000	1.135	.355	0.000	.103	.710	.050	-.923	.510
.150	-.604	.460	.012	.272	.757	.012	.211	.740	.150	-.779	.466
.300	-.725	.481	.025	-.172	.634	.025	-.096	.654	.300	-.824	.454
.450	-.517	.539	.050	-.531	.535	.050	-.546	.531	.450	-.901	.516
.600	-.579	.522	.100	-.710	.485	.100	-.663	.496	.600	-.613	.512
.800	-.339	.588	.150	-.658	.503	.150	-.610	.511	.800	-.284	.603
.990	.065	.700	.200	-.754	.462	.200	-.693	.490			
			.300	-.827	.451	.300	-.786	.465			
			.350	-.753	.462	.350	-.832	.452			
			.400	-.770	.469	.400	-.805	.459			
			.450	-.647	.503	.450	-.725	.481			
			.500	-.809	.453	.500	-.698	.489			
			.550	-.809	.453	.550	-.809	.458			
			.600	-.706	.485	.600	-.755	.473			
			.650	-.668	.497	.700	-.590	.572			
			.700	-.552	.529	.800	-.184	.631			
			.800	-.279	.604	.900	-.058	.666			
			.900	-.008	.679	.950	-.038	.671			
			.950	.038	.692	.990	-.031	.673			
			.990	.072	.701						
					LOWER SURFACE						
.100	-.762	.471	.025	-.270	.607	.025	-.161	.637	.100	-1.195	.351
.300	-1.071	.386	.050	-.751	.463	.050	-.741	.477	.300	-1.217	.345
.600	-.257	.611	.100	-.539	.422	.100	-1.057	.390	.600	-.347	.566
.800	.039	.692	.200	-1.040	.364	.200	-1.059	.389	.800	.177	.730
			.300	-1.149	.364	.300	-1.184	.355			
			.400	-1.136	.363	.400	-1.268	.328			
			.500	-.986	.520	.500	-.833	.507			
			.600	-.308	.596	.600	-.263	.605			
			.700	.028	.683	.700	.006	.683			
			.800	.198	.736	.800	.243	.749			
			.900	.258	.764	.900	.265	.755			
			.950	.277	.758	.950	.311	.767			
			1.000	.100	.707						
CN=				.0437			.0263				
CM=				-.1051			-.0564				

(h) M = 0.76. Continued.

$\alpha = -1.68^{o}$

STATION .1552			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.749	.475	0.000	1.145	.493	0.000	.101	.710	.050	-.721	.482
.150	-.801	.433	.012	.153	.724	.012	.090	.705	.150	-1.025	.399
.300	-.750	.475	.025	-.290	.602	.025	-.206	.625	.300	-.736	.478
.450	-.657	.489	.050	-.637	.506	.050	-.717	.484	.450	-.653	.500
.600	-.579	.522	.100	-.539	.423	.100	-.834	.451	.600	-.618	.511
.800	-.347	.586	.150	-.537	.453	.150	-.786	.465	.800	-.269	.607
.990	.056	.657	.200	-.665	.443	.200	-.837	.451			
			.300	-.926	.426	.300	-.904	.432			
			.350	-.914	.429	.350	-.941	.422			
			.400	-.853	.435	.400	-.884	.434			
			.450	-.774	.468	.450	-.909	.431			
			.500	-.688	.436	.500	-.874	.440			
			.550	-.759	.461	.550	-.778	.467			
			.600	-.595	.517	.600	-.647	.503			
			.650	-.636	.506	.700	-.401	.571			
			.700	-.532	.535	.800	-.210	.624			
			.800	-.253	.612	.900	-.062	.664			
			.900	-.020	.675	.950	-.044	.670			
			.950	.036	.692	.990	-.043	.670			
			.990	.069	.701						
					LOWER SURFACE						
.100	-.564	.520	.025	-.149	.627	.025	-.074	.661	.100	-1.105	.377
.300	-.537	.523	.050	-.670	.487	.050	-.654	.501	.300	-1.110	.375
.600	-.222	.620	.100	-.855	.440	.100	-.950	.419	.600	-.358	.583
.800	.032	.690	.200	-.911	.430	.200	-.882	.428	.800	.174	.730
			.300	-.938	.423	.300	-1.049	.392			
			.400	-1.080	.383	.400	-1.173	.358			
			.500	-.649	.502	.500	-.554	.523			
			.600	-.179	.632	.600	-.255	.611			
			.700	.051	.656	.700	.030	.690			
			.800	.206	.739	.800	.271	.756			
			.900	.318	.769	.900	.324	.771			
			.950	.335	.774	.950	.333	.774			
			1.000	.080	.704						
CN=				.1704			.1654				
CM=				-.1093			-.1023				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(h) M = 0.76. Continued.

$\alpha = -0.58^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.861	.444	0.000	1.127	.955	0.000	.110	.712	.050	-.437	.451
.150	-1.056	.340	.012	.029	.693	.012	-.035	.672	.150	-1.189	.354
.300	-1.022	.400	.025	-.411	.569	.025	-.325	.552	.300	-1.117	.374
.450	-.905	.432	.050	-.816	.455	.050	-.830	.453	.450	-.662	.499
.600	-.546	.521	.100	-1.045	.364	.100	-.491	.408	.600	-.610	.513
.800	-.340	.565	.150	-1.024	.339	.150	-1.012	.403	.800	-.242	.604
.990	.062	.699	.200	-1.059	.390	.200	-.770	.414			
			.300	-1.067	.368	.300	-1.044	.374			
			.250	-1.063	.359	.350	-1.062	.389			
			.400	-1.059	.370	.400	-1.042	.395			
			.450	-1.008	.404	.450	-1.073	.386			
			.500	-1.141	.367	.500	-.988	.409			
			.550	-1.052	.392	.550	-.760	.472			
			.600	-.987	.920	.600	-.597	.517			
			.650	-.544	.522	.700	-.381	.577			
			.700	-.403	.554	.800	-.210	.624			
			.800	-.278	.605	.900	-.061	.665			
			.900	-.013	.673	.950	-.038	.671			
			.950	.047	.655	.990	-.039	.671			
			.990	.066	.703						
					LOWER SURFACE						
.100	-.432	.564	.025	-.067	.603	.025	.021	.696	.100	-.334	.419
.300	-.861	.444	.050	-.492	.546	.050	-.557	.528	.300	-.463	.444
.600	-.246	.614	.100	-.838	.505	.100	-.680	.494	.600	-.351	.544
.800	.052	.707	.200	-.773	.483	.200	-.799	.462	.800	.175	.730
			.300	-.852	.447	.300	-.974	.413			
			.400	-.561	.417	.400	-1.070	.397			
			.500	-.643	.504	.500	-.941	.533			
			.600	-.226	.623	.600	-.277	.606			
			.700	.071	.701	.700	.022	.683			
			.800	.238	.743	.800	.278	.759			
			.900	.348	.773	.900	.332	.774			
			.950	.329	.775	.950	.349	.778			
			1.000	.086	.706						
CN=				.3392			.2693				
CM=				-.1132			-.0581				

(h) M = 0.76. Continued.

$\alpha = 0.38^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.002	.406	0.000	1.129	.953	0.000	.097	.709	.050	-.776	.413
.150	-1.169	.359	.012	-.057	.655	.012	-.142	.643	.150	-1.280	.329
.300	-1.144	.387	.025	-.533	.535	.025	-.415	.567	.300	-1.224	.343
.450	-1.038	.358	.050	-.527	.426	.050	-.929	.426	.450	-.698	.489
.600	-.504	.542	.100	-1.109	.359	.100	-1.113	.375	.600	-.604	.514
.800	-.331	.591	.150	-1.137	.367	.150	-1.097	.375	.900	-.290	.602
.990	.080	.704	.200	-1.171	.359	.200	-1.132	.370			
			.300	-1.180	.354	.300	-1.149	.365			
			.250	-1.210	.343	.350	-1.167	.360			
			.400	-1.209	.341	.400	-1.169	.359			
			.450	-1.153	.364	.450	-1.226	.344			
			.500	-1.256	.335	.500	-1.239	.340			
			.550	-1.015	.402	.550	-1.040	.395			
			.600	-.651	.502	.600	-.620	.511			
			.650	-.496	.543	.700	-.349	.574			
			.700	-.406	.573	.800	-.246	.614			
			.800	-.256	.617	.900	-.069	.663			
			.900	-.043	.670	.950	-.027	.674			
			.950	.006	.684	.990	.001	.682			
			.990	.050	.696						
					LOWER SURFACE						
.100	-.354	.584	.025	.023	.648	.025	.157	.725	.100	-.790	.464
.300	-.689	.492	.050	-.374	.579	.050	-.437	.561	.300	-.729	.481
.600	-.221	.621	.100	-.525	.537	.100	-.559	.528	.600	-.357	.593
.800	.109	.712	.200	-.635	.489	.200	-.689	.492	.100	.192	.735
			.300	-.743	.477	.300	-.806	.443			
			.400	-.807	.459	.400	-.715	.430			
			.500	-.731	.483	.500	-.623	.510			
			.600	-.227	.619	.600	-.281	.604			
			.700	.075	.703	.700	.029	.659			
			.800	.253	.752	.800	.251	.762			
			.900	.342	.776	.900	.352	.773			
			.950	.317	.769	.950	.373	.785			
			1.000	.086	.700						
CN=				.4352			.4306				
CM=				-.1044			-.1074				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(h) M = 0.76. Concluded.

$\alpha = 1.08^{o}$

STATION .1592			STATION .4249			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.094	.380	0.000	1.126	.933	0.000	.050	.707	.050	-1.018	.401
.150	-1.242	.340	.012	-.124	.643	.012	-.213	.623	.150	-1.336	.313
.300	-1.202	.350	.025	-.607	.514	.025	-.500	.544	.300	-1.357	.308
.450	-1.089	.382	.050	-.991	.403	.050	-.977	.413	.450	-.741	.473
.600	-.493	.546	.100	-1.226	.344	.100	-1.167	.360	.600	-.571	.524
.800	-.324	.592	.150	-1.196	.352	.150	-1.168	.360	.800	-.274	.606
.990	.069	.701	.200	-1.233	.342	.200	-1.174	.359			
			.300	-1.264	.333	.300	-1.224	.344			
			.350	-1.265	.333	.350	-1.231	.343			
			.400	-1.255	.336	.400	-1.217	.346			
			.450	-1.216	.347	.450	-1.277	.330			
			.500	-.844	.447	.500	-1.319	.318			
			.550	-.704	.483	.550	-.803	.460			
			.600	-.652	.502	.600	-.646	.504			
			.650	-.507	.542	.700	-.426	.564			
			.700	-.436	.562	.800	-.290	.602			
			.800	-.227	.619	.900	-.096	.655			
			.900	-.130	.646	.950	-.027	.675			
			.950	-.051	.663	.990	.012	.685			
			.990	-.027	.675						
					LOWER SURFACE						
.100	-.241	.615	.025	.093	.708	.025	.198	.737	.100	-.750	.491
.300	-.630	.508	.050	-.276	.606	.050	-.343	.567	.300	-.743	.477
.600	-.251	.613	.100	-.457	.556	.100	-.514	.540	.600	-.370	.560
.800	.083	.705	.200	-.623	.513	.200	-.612	.513	.900	.207	.739
			.300	-.686	.493	.300	-.623	.495			
			.400	-.760	.472	.400	-.752	.475			
			.500	-.765	.471	.500	-.710	.486			
			.600	-.231	.613	.600	-.303	.556			
			.700	.054	.704	.700	.027	.650			
			.800	.231	.746	.800	.298	.724			
			.900	.346	.777	.900	.354	.736			
			.950	.322	.771	.950	.377	.746			
			1.000	-.076	.661						
CN=				.4465			.4856				
CM=				-.0995			-.1088				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(i) M = 0.80

$\alpha = -4.15^{o}$

STATION .1562			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.251	.552	0.000	1.146	.955	0.000	.081	.676	.050	-.350	.552
.150	-.602	.476	.012	.438	.784	.012	.350	.760	.150	-.624	.472
.300	-.621	.473	.025	.042	.668	.025	.082	.690	.300	-.679	.456
.450	-.551	.496	.050	-.332	.554	.050	-.329	.559	.450	-.656	.468
.600	-.735	.439	.100	-.462	.523	.100	-.432	.524	.600	-.767	.423
.800	-.368	.547	.150	-.504	.507	.150	-.473	.516	.800	-.251	.582
.990	-.114	.622	.200	-.631	.479	.200	-.549	.494			
			.300	-.643	.466	.300	-.671	.459			
			.350	-.674	.457	.350	-.724	.442			
			.400	-.699	.451	.400	-.715	.445			
			.450	-.628	.471	.450	-.761	.432			
			.500	-.619	.474	.500	-.788	.424			
			.550	-.499	.513	.550	-.492	.553			
			.600	-.802	.417	.600	-.964	.372			
			.650	-.797	.421	.700	-.421	.591			
			.700	-.412	.534	.800	-.228	.588			
			.800	-.179	.603	.900	-.144	.613			
			.900	-.124	.619	.950	-.139	.615			
			.950	-.097	.627	.990	-.106	.624			
			.990	-.076	.633						
					LOWER SURFACE						
.100	-.756	.432	.025	-.803	.566	.025	-.209	.594	.100	-1.143	.319
.300	-1.147	.318	.050	-.814	.415	.050	-.758	.432	.300	-1.351	.256
.600	-.333	.558	.100	-.588	.365	.100	-1.025	.354	.600	-.471	.517
.800	-.277	.574	.200	-1.077	.333	.200	-1.101	.332	.800	-.089	.629
			.300	-1.172	.311	.300	-1.177	.309			
			.400	-.651	.464	.400	-.652	.464			
			.500	-.588	.483	.500	-.607	.477			
			.600	-.614	.475	.600	-.578	.485			
			.700	-.483	.513	.700	-.507	.506			
			.800	-.343	.559	.800	-.258	.580			
			.900	-.053	.640	.900	-.179	.603			
			.950	.004	.657	.950	-.074	.634			
			1.000	-.055	.638						
CN=				-.1562			-.1206				
CM=				-.0326			-.0295				

(i) M = 0.80. Continued.

$\alpha = -3.38^{o}$

STATION .1562			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.423	.532	0.000	1.144	.952	0.000	.090	.683	.050	-.454	.523
.150	-.693	.455	.012	.382	.769	.012	.332	.754	.150	-.790	.424
.300	-.631	.471	.025	-.027	.643	.025	.036	.667	.300	-.673	.457
.450	-.583	.485	.050	-.350	.542	.050	-.402	.536	.450	-.705	.447
.600	-.730	.442	.100	-.630	.471	.100	-.539	.478	.600	-.784	.426
.800	-.346	.555	.150	-.538	.494	.150	-.534	.500	.800	-.218	.592
.990	-.071	.636	.200	-.676	.458	.200	-.582	.485			
			.300	-.734	.441	.300	-.756	.474			
			.350	-.767	.431	.350	-.780	.427			
			.400	-.751	.436	.400	-.787	.425			
			.450	-.664	.461	.450	-.812	.419			
			.500	-.852	.405	.500	-.839	.410			
			.550	-.310	.589	.550	-.733	.382			
			.600	-.815	.417	.600	-.949	.363			
			.650	-.553	.482	.700	-.366	.549			
			.700	-.344	.555	.800	-.205	.596			
			.800	-.180	.604	.900	-.140	.615			
			.900	-.096	.624	.950	-.087	.631			
			.950	-.101	.627	.990	-.050	.642			
			.990	-.077	.634						
					LOWER SURFACE						
.100	-.655	.451	.025	-.269	.577	.025	-.109	.624	.100	-1.094	.334
.300	-1.077	.340	.050	-.754	.436	.050	-.679	.457	.300	-1.310	.272
.600	-.307	.566	.100	-.617	.387	.100	-.984	.387	.600	-.496	.511
.800	-.268	.578	.200	-1.017	.354	.200	-1.046	.349	.800	-.034	.646
			.300	-1.128	.329	.300	-1.163	.315			
			.400	-.651	.469	.400	-.721	.445			
			.500	-.940	.453	.500	-.557	.493			
			.600	-.524	.503	.600	-.542	.497			
			.700	-.455	.523	.700	-.436	.528			
			.800	-.294	.573	.800	-.285	.573			
			.900	-.075	.634	.900	-.150	.612			
			.950	-.024	.649	.950	-.065	.637			
			1.000	-.032	.647						
CN=				-.1045			-.0765				
CM=				-.0250			-.0262				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(i) M = 0.80. Continued.

$\alpha = -2.77^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.466	.511	0.000	1.147	.393	0.000	.108	.688	.050	-.507	.595
.150	-.723	.444	.012	.311	.748	.012	.279	.738	.150	-.843	.409
.300	-.732	.441	.025	-.094	.629	.025	-.032	.647	.300	-.618	.475
.450	-.617	.475	.050	-.452	.512	.050	-.468	.515	.450	-.728	.443
.600	-.710	.448	.100	-.745	.433	.100	-.630	.471	.600	-.795	.423
.800	-.331	.559	.150	-.556	.493	.150	-.599	.480	.800	-.244	.555
.990	-.028	.643	.200	-.716	.446	.200	-.602	.479			
			.300	-.819	.416	.300	-.785	.426			
			.350	-.827	.413	.350	-.842	.409			
			.400	-.834	.411	.400	-.834	.411			
			.450	-.725	.443	.450	-.834	.394			
			.500	-.870	.401	.500	-.900	.382			
			.550	-.941	.380	.550	-.960	.374			
			.600	-.737	.440	.600	-1.002	.362			
			.650	-.511	.505	.700	-.343	.556			
			.700	-.307	.566	.800	-.177	.605			
			.800	-.171	.606	.900	-.116	.622			
			.900	-.101	.627	.950	-.084	.632			
			.950	-.077	.634	.990	-.062	.638			
			.990	-.052	.641						
					LOWER SURFACE						
.100	-.661	.462	.025	-.223	.591	.025	-.085	.651	.100	-1.061	.345
.300	-1.015	.398	.050	-.718	.445	.050	-.631	.471	.300	-1.269	.284
.600	-.284	.573	.100	-.865	.402	.100	-.932	.383	.600	-.475	.517
.800	-.275	.576	.200	-.945	.379	.200	-.989	.366	.800	.004	.656
			.300	-1.069	.342	.300	-1.096	.335			
			.400	-.887	.396	.400	-.842	.409			
			.500	-.493	.511	.500	-.545	.496			
			.600	-.526	.502	.600	-.548	.495			
			.700	-.378	.545	.700	-.387	.543			
			.800	-.204	.597	.800	-.300	.566			
			.900	-.085	.631	.900	-.110	.624			
			.950	.009	.659	.950	-.074	.635			
			1.000	.004	.657						
CN=				-.0603			-.0456				
CM=				-.0268			-.0208				

(i) M = 0.80. Continued.

$\alpha = -2.04^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.546	.496	0.000	1.159	.387	0.000	.099	.696	.050	-.583	.485
.150	-.790	.424	.012	.270	.736	.012	.202	.716	.150	-.936	.381
.300	-.805	.420	.025	-.166	.608	.025	-.120	.621	.300	-.910	.389
.450	-.656	.464	.050	-.530	.501	.050	-.543	.497	.450	-.741	.449
.600	-.617	.475	.100	-.751	.424	.100	-.682	.456	.600	-.799	.422
.800	-.313	.565	.150	-.723	.444	.150	-.706	.449	.800	-.227	.590
.990	.019	.662	.200	-.760	.433	.200	-.726	.443			
			.300	-.843	.409	.300	-.818	.416			
			.350	-.862	.403	.350	-.876	.399			
			.400	-.862	.403	.400	-.862	.403			
			.450	-.752	.424	.450	-.942	.380			
			.500	-.946	.373	.500	-.968	.372			
			.550	-.968	.372	.550	-1.040	.351			
			.600	-.613	.476	.600	-.842	.409			
			.650	-.406	.537	.700	-.340	.556			
			.700	-.282	.574	.800	-.223	.591			
			.800	-.143	.614	.900	-.120	.621			
			.900	-.072	.633	.950	-.086	.631			
			.950	-.079	.633	.990	-.059	.639			
			.990	-.054	.641						
					LOWER SURFACE						
.100	-.564	.485	.025	-.178	.604	.025	-.025	.645	.100	-1.002	.362
.300	-.975	.370	.050	-.635	.470	.050	-.602	.480	.300	-1.219	.298
.600	-.329	.560	.100	-.816	.417	.100	-.873	.400	.600	-.467	.519
.800	-.227	.590	.200	-.910	.389	.200	-.922	.386	.800	.036	.667
			.300	-1.022	.356	.300	-1.041	.351			
			.400	-1.076	.340	.400	-1.005	.361			
			.500	-.470	.513	.500	-.531	.500			
			.600	-.453	.523	.600	-.512	.506			
			.700	-.334	.553	.700	-.398	.540			
			.800	-.184	.602	.800	-.251	.583			
			.900	-.070	.635	.900	-.110	.624			
			.950	-.020	.651	.950	-.018	.651			
			1.000	-.075	.634						
CN=				-.0328			.0061				
CM=				-.0220			-.0249				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(i) M = 0.80. Continued.

$\alpha = -1.36^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.668	.478	0.000	1.147	.353	0.000	.100	.686	.050	-.937	.469
.150	-.839	.410	.012	.205	.717	.012	.121	.692	.150	-1.000	.363
.300	-.887	.402	.025	-.217	.593	.025	-.168	.687	.300	-.979	.369
.450	-.725	.444	.050	-.598	.481	.050	-.611	.677	.450	-.734	.441
.600	-.506	.508	.100	-.852	.405	.100	-.779	.628	.600	-.784	.426
.800	-.297	.569	.150	-.927	.414	.150	-.799	.622	.800	-.242	.585
.990	.018	.662	.200	-.882	.397	.200	-.771	.630			
			.300	-.898	.355	.300	-.879	.598			
			.350	-.932	.383	.350	-.916	.387			
			.400	-.922	.386	.400	-.923	.395			
			.450	-.885	.403	.450	-.978	.369			
			.500	-1.025	.355	.500	-1.025	.356			
			.550	-.868	.401	.550	-1.106	.332			
			.600	-.469	.519	.600	-.965	.451			
			.650	-.346	.559	.700	-.354	.553			
			.700	-.253	.573	.800	-.229	.589			
			.800	-.165	.603	.900	-.171	.606			
			.900	-.100	.627	.950	-.111	.624			
			.950	-.104	.626	.990	-.079	.633			
			.990	-.061	.634						
					LOWER SURFACE						
.100	-.494	.512	.025	-.127	.619	.025	.036	.667	.100	-.983	.368
.300	-.514	.388	.050	-.547	.496	.050	-.561	.492	.300	-1.148	.319
.600	-.283	.573	.100	-.725	.443	.100	-.810	.413	.600	-.407	.537
.800	-.211	.594	.200	-.831	.413	.200	-.845	.408	.800	.112	.649
			.300	-.894	.378	.300	-.957	.384			
			.400	-1.058	.345	.400	-1.133	.324			
			.500	-.463	.529	.500	-.500	.510			
			.600	-.438	.523	.600	-.465	.520			
			.700	-.332	.553	.700	-.381	.545			
			.800	-.201	.597	.800	-.243	.585			
			.900	-.015	.652	.900	-.120	.621			
			.950	.011	.660	.950	-.056	.640			
			1.000	-.052	.641						
CN=				.0387			.0426				
CM=				-.0244			-.0155				

(i) M = 0.80. Continued.

$\alpha = -0.67^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.717	.446	0.000	1.134	.355	0.000	.100	.686	.050	-.711	.447
.150	-.925	.385	.012	.160	.703	.012	.059	.674	.150	-1.032	.353
.300	-.926	.384	.025	-.296	.571	.025	-.205	.596	.300	-1.037	.352
.450	-.758	.422	.050	-.651	.465	.050	-.659	.463	.450	-.806	.420
.600	-.431	.530	.100	-.820	.389	.100	-.847	.408	.600	-.662	.462
.800	-.269	.577	.150	-.896	.393	.150	-.876	.399	.800	-.248	.583
.990	-.001	.656	.200	-.956	.375	.200	-.848	.407			
			.300	-.982	.363	.300	-.954	.376			
			.350	-.986	.367	.350	-.955	.376			
			.400	-.994	.364	.400	-.974	.370			
			.450	-.901	.392	.450	-1.032	.353			
			.500	-1.012	.359	.500	-1.075	.341			
			.550	-.552	.494	.550	-.893	.394			
			.600	-.435	.523	.600	-.473	.517			
			.650	-.350	.554	.700	-.357	.552			
			.700	-.278	.575	.800	-.271	.577			
			.800	-.158	.593	.900	-.186	.602			
			.900	-.137	.615	.950	-.164	.608			
			.950	-.110	.624	.990	-.100	.627			
			.990	-.076	.633						
					LOWER SURFACE						
.100	-.448	.525	.025	-.056	.640	.025	.078	.679	.100	-.918	.387
.300	-.876	.395	.050	-.478	.516	.050	-.504	.506	.300	-1.096	.334
.600	-.347	.554	.100	-.665	.461	.100	-.766	.431	.600	-.404	.538
.800	-.204	.596	.200	-.750	.424	.200	-.767	.431	.800	.083	.661
			.300	-.861	.393	.300	-.941	.380			
			.400	-1.001	.362	.400	-1.083	.338			
			.500	-.530	.501	.500	-.479	.516			
			.600	-.422	.533	.600	-.449	.524			
			.700	-.345	.555	.700	-.372	.547			
			.800	-.264	.590	.800	-.274	.576			
			.900	-.061	.634	.900	-.135	.617			
			.950	.050	.671	.950	-.018	.651			
			1.000	-.073	.635						
CN=				.0086			.0554				
CM=				-.0167			-.0212				

TABLE V.- PRESSURE COEFFICIENTS FOR CONFIGURATION 1; HORIZONTAL TAIL OFF; WAKE RAKE ON;

AILERON UNSEALED - Concluded

(i) M = 0.80. Concluded.

$\alpha = 0.02^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.791	.424	0.000	1.148	.994	0.000	.083	.691	.050	-.768	.431
.150	-1.012	.359	.012	.113	.530	.012	.026	.664	.150	-1.075	.341
.300	-.584	.368	.025	-.338	.557	.025	-.261	.580	.300	-1.145	.320
.450	-.850	.407	.050	-.716	.446	.050	-.711	.448	.450	-.871	.401
.600	-.416	.534	.100	-.972	.371	.100	-.903	.391	.600	-.950	.445
.800	-.218	.592	.150	-.940	.380	.150	-.911	.395	.800	-.248	.544
.990	.004	.656	.200	-1.011	.360	.200	-.934	.382			
			.300	-1.032	.353	.300	-.992	.365			
			.350	-1.047	.349	.350	-1.013	.359			
			.400	-1.057	.345	.400	-1.030	.354			
			.450	-.964	.374	.450	-1.097	.334			
			.500	-.754	.435	.500	-1.050	.348			
			.550	-.503	.509	.550	-.562	.491			
			.600	-.419	.533	.600	-.476	.516			
			.650	-.377	.545	.700	-.378	.546			
			.700	-.321	.562	.800	-.294	.570			
			.800	-.225	.590	.900	-.245	.584			
			.900	-.187	.602	.950	-.183	.606			
			.950	-.135	.617	.990	-.126	.619			
			.990	-.095	.629						
					LOWER SURFACE						
.100	-.378	.545	.025	.006	.653	.025	.131	.655	.100	-.884	.403
.300	-.844	.405	.050	-.419	.533	.050	-.439	.527	.300	-1.018	.357
.600	-.375	.546	.100	-.575	.487	.100	-.680	.457	.600	-.403	.538
.800	-.189	.601	.200	-.703	.450	.200	-.729	.442	.800	.040	.668
			.300	-.835	.411	.300	-.704	.391			
			.400	-.673	.471	.400	-1.059	.345			
			.500	-.658	.465	.500	-.545	.496			
			.600	-.400	.539	.600	-.445	.526			
			.700	-.368	.543	.700	-.373	.547			
			.800	-.210	.595	.800	-.237	.587			
			.900	-.042	.647	.900	-.086	.631			
			.950	.035	.667	.950	.019	.662			
			1.000	-.049	.642						
CN=				.1023			.1356				
CM=				-.0138			-.0248				

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED

(a) M = 0.70

$\alpha = -4.97^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.323	.641	0.000	1.079	.988	0.000	.088	.742	.050	-.255	.657
.150	-.482	.601	.012	.491	.842	.012	.416	.823	.150	-.399	.622
.300	-.520	.592	.025	.081	.740	.025	.162	.761	.300	-.510	.594
.450	-.381	.626	.050	-.198	.671	.050	-.194	.672	.450	-.491	.599
.600	-.516	.593	.100	-.361	.631	.100	-.337	.637	.600	-.528	.590
.800	-.404	.620	.150	-.425	.615	.150	-.351	.634	.800	-.331	.639
.990	.082	.741	.200	-.463	.606	.200	-.455	.608			
			.300	-.502	.596	.300	-.508	.595			
			.350	-.512	.594	.350	-.512	.594			
			.400	-.522	.591	.400	-.502	.596			
			.450	-.499	.597	.450	-.559	.582			
			.500	-.598	.572	.500	-.596	.573			
			.550	-.614	.568	.550	-.585	.576			
			.600	-.544	.586	.600	-.588	.575			
			.650	-.613	.569	.700	-.444	.611			
			.700	-.575	.578	.800	-.281	.651			
			.800	-.379	.627	.900	-.041	.710			
			.900	-.048	.709	.950	-.001	.720			
			.950	.058	.735	.990	.009	.723			
			.990	.109	.747						
					LOWER SURFACE						
.100	-1.256	.409	.025	-.682	.552	.025	-.607	.570	.100	-1.630	.317
.300	-.747	.536	.050	-1.311	.396	.050	-1.211	.421	.300	-.827	.516
.600	-.266	.655	.100	-1.399	.374	.100	-1.507	.347	.600	-.334	.638
.800	.074	.739	.200	-1.479	.354	.200	-1.525	.343	.800	.106	.747
			.300	-1.329	.391	.300	-1.448	.362			
			.400	-.667	.555	.400	-.590	.574			
			.500	-.665	.556	.500	-.568	.580			
			.600	-.283	.650	.600	-.307	.644			
			.700	.056	.734	.700	-.005	.719			
			.800	.213	.773	.800	.234	.778			
			.900	.329	.802	.900	.271	.788			
			.950	.327	.802	.950	.275	.789			
			1.000	.127	.752						
CN=				-.1872			-.2023				
CM=				-.1297			-.1147				

(a) M = 0.70. Continued.

$\alpha = -3.32^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.540	.587	0.000	1.108	.995	0.000	.092	.743	.050	-.451	.609
.150	-.604	.571	.012	.249	.782	.012	.220	.775	.150	-.552	.584
.300	-.585	.576	.025	-.154	.682	.025	-.022	.715	.300	-.583	.576
.450	-.461	.606	.050	-.481	.602	.050	-.450	.609	.450	-.525	.591
.600	-.543	.586	.100	-.591	.574	.100	-.521	.592	.600	-.546	.586
.800	-.410	.619	.150	-.603	.571	.150	-.475	.603	.800	-.331	.639
.990	.085	.742	.200	-.636	.563	.200	-.576	.578			
			.300	-.612	.569	.300	-.604	.571			
			.350	-.613	.569	.350	-.592	.574			
			.400	-.595	.573	.400	-.579	.577			
			.450	-.578	.577	.450	-.609	.570			
			.500	-.660	.557	.500	-.652	.559			
			.550	-.655	.559	.550	-.643	.561			
			.600	-.591	.574	.600	-.621	.567			
			.650	-.628	.565	.700	-.456	.608			
			.700	-.576	.579	.800	-.267	.655			
			.800	-.346	.635	.900	-.051	.708			
			.900	-.039	.711	.950	-.021	.715			
			.950	.059	.735	.990	-.007	.719			
			.990	.105	.747						
					LOWER SURFACE						
.100	-.894	.499	.025	-.518	.592	.025	-.389	.624	.100	-1.431	.366
.300	-.785	.526	.050	-1.110	.446	.050	-1.005	.472	.300	-.639	.562
.600	-.277	.652	.100	-1.190	.426	.100	-1.277	.404	.600	-.349	.634
.800	.075	.739	.200	-1.061	.458	.200	-1.241	.414	.800	.127	.752
			.300	-.847	.511	.300	-.779	.528			
			.400	-.777	.528	.400	-.764	.531			
			.500	-.681	.552	.500	-.626	.566			
			.600	-.270	.654	.600	-.312	.643			
			.700	.045	.732	.700	-.002	.720			
			.800	.155	.759	.800	.200	.770			
			.900	.262	.785	.900	.272	.788			
			.950	.293	.793	.950	.305	.796			
			1.000	.115	.749						
CN=				-.0152			-.0296				
CM=				-.1096			-.1058				

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.70. Continued.

$\alpha = -2.44^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.738	.548	0.000	1.105	.994	0.000	.093	.744	.050	-.630	.565
.150	-.692	.549	.012	.146	.757	.012	.152	.758	.150	-.641	.562
.300	-.677	.553	.025	-.249	.659	.025	-.221	.666	.300	-.599	.572
.450	-.544	.586	.050	-.656	.558	.050	-.670	.555	.450	-.549	.585
.600	-.564	.581	.100	-.717	.543	.100	-.639	.562	.600	-.563	.581
.800	-.388	.625	.150	-.706	.546	.150	-.607	.570	.800	-.317	.642
.990	.065	.747	.200	-.720	.542	.200	-.669	.555			
			.300	-.679	.552	.300	-.671	.554			
			.350	-.670	.555	.350	-.636	.563			
			.400	-.646	.560	.400	-.611	.569			
			.450	-.617	.568	.450	-.649	.560			
			.500	-.706	.546	.500	-.685	.551			
			.550	-.689	.550	.550	-.665	.556			
			.600	-.624	.566	.600	-.627	.565			
			.650	-.645	.561	.700	-.455	.608			
			.700	-.592	.574	.800	-.268	.654			
			.800	-.358	.632	.900	-.058	.706			
			.900	-.047	.709	.950	-.031	.713			
			.950	.048	.732	.990	-.026	.714			
			.990	.079	.740						
					LOWER SURFACE						
.100	-.666	.536	.025	-.391	.624	.025	-.255	.657	.100	-1.366	.382
.300	-.740	.537	.050	-.851	.510	.050	-.868	.506	.300	-.684	.551
.600	-.302	.646	.100	-1.016	.469	.100	-1.079	.453	.600	-.339	.637
.800	.101	.746	.200	-.913	.495	.200	-.887	.501	.800	.143	.756
			.300	-.820	.518	.300	-.843	.512			
			.400	-.737	.538	.400	-.746	.536			
			.500	-.684	.551	.500	-.618	.568			
			.600	-.282	.651	.600	-.323	.641			
			.700	.056	.734	.700	-.005	.719			
			.800	.214	.774	.800	.228	.777			
			.900	.332	.803	.900	.289	.792			
			.950	.324	.801	.950	.317	.799			
			1.000	.102	.746						
CN=				.0971			.0794				
CM=				-.1159			-.1008				

(a) M = 0.70. Continued.

$\alpha = -1.60^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.830	.515	0.000	1.116	.997	0.000	.090	.743	.050	-.860	.508
.150	-.789	.525	.012	.037	.730	.012	.014	.724	.150	-.736	.538
.300	-.707	.545	.025	-.435	.613	.025	-.354	.633	.300	-.672	.554
.450	-.553	.584	.050	-.827	.516	.050	-.809	.520	.450	-.571	.579
.600	-.579	.577	.100	-.845	.511	.100	-.783	.527	.600	-.563	.581
.800	-.396	.623	.150	-.802	.522	.150	-.715	.544	.800	-.328	.639
.990	.046	.732	.200	-.829	.515	.200	-.773	.529			
			.300	-.741	.537	.300	-.743	.537			
			.350	-.700	.547	.350	-.705	.546			
			.400	-.691	.549	.400	-.662	.557			
			.450	-.678	.553	.450	-.690	.550			
			.500	-.735	.539	.500	-.714	.544			
			.550	-.710	.545	.550	-.688	.550			
			.600	-.650	.560	.600	-.647	.560			
			.650	-.659	.557	.700	-.464	.606			
			.700	-.593	.574	.800	-.285	.650			
			.800	-.358	.632	.900	-.077	.702			
			.900	-.045	.709	.950	-.038	.711			
			.950	.034	.729	.990	-.032	.713			
			.990	.078	.740						
					LOWER SURFACE						
.100	-.542	.586	.025	-.253	.658	.025	-.168	.679	.100	-1.048	.461
.300	-.690	.550	.050	-.719	.543	.050	-.771	.530	.300	-.669	.555
.600	-.276	.652	.100	-.799	.523	.100	-.780	.527	.600	-.353	.633
.800	.143	.756	.200	-.807	.521	.200	-.791	.525	.800	.171	.763
			.300	-.783	.527	.300	-.805	.521			
			.400	-.716	.543	.400	-.717	.543			
			.500	-.673	.554	.500	-.616	.568			
			.600	-.289	.649	.600	-.325	.640			
			.700	.076	.739	.700	.002	.721			
			.800	.231	.778	.800	.270	.787			
			.900	.341	.805	.900	.330	.802			
			.950	.343	.805	.950	.354	.808			
			1.000	.075	.739						
CN=				.1983			.1882				
CM=				-.1125			-.1035				

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) $M = 0.70$. Continued.

$\alpha = -0.72^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.014	.470	0.000	1.123	.999	0.000	.099	.745	.050	-.980	.478
.150	-.952	.485	.012	-.086	.699	.012	-.165	.680	.150	-.897	.498
.300	-.754	.534	.025	-.545	.586	.025	-.461	.606	.300	-.723	.542
.450	-.599	.572	.050	-.986	.477	.050	-.942	.487	.450	-.600	.572
.600	-.587	.575	.100	-1.207	.422	.100	-1.088	.451	.600	-.577	.578
.800	-.375	.626	.150	-.907	.496	.150	-.867	.506	.800	-.324	.640
.990	.038	.730	.200	-.937	.489	.200	-.857	.508			
			.300	-.835	.514	.300	-.802	.522			
			.350	-.757	.533	.350	-.748	.535			
			.400	-.726	.541	.400	-.687	.550			
			.450	-.708	.545	.450	-.724	.541			
			.500	-.755	.534	.500	-.733	.539			
			.550	-.720	.542	.550	-.693	.549			
			.600	-.664	.556	.600	-.655	.558			
			.650	-.650	.560	.700	-.449	.609			
			.700	-.586	.576	.800	-.263	.655			
			.800	-.335	.638	.900	-.088	.699			
			.900	-.042	.710	.950	-.064	.705			
			.950	.025	.727	.990	-.055	.707			
			.990	.058	.735						
					LOWER SURFACE						
.100	-.429	.614	.025	-.148	.684	.025	-.020	.716	.100	-.884	.502
.300	-.630	.565	.050	-.566	.580	.050	-.592	.574	.300	-.655	.558
.600	-.301	.646	.100	-.649	.560	.100	-.650	.560	.600	-.353	.633
.800	.146	.757	.200	-.691	.549	.200	-.689	.550	.800	.200	.770
			.300	-.709	.545	.300	-.752	.535			
			.400	-.674	.554	.400	-.689	.550			
			.500	-.652	.559	.500	-.587	.575			
			.600	-.270	.654	.600	-.328	.639			
			.700	.078	.740	.700	.016	.725			
			.800	.253	.783	.800	.279	.790			
			.900	.353	.808	.900	.330	.802			
			.950	.348	.807	.950	.349	.807			
			1.000	.067	.737						
CN=				.3054			.2831				
CM=				-.1075			-.0971				

(a) $M = 0.70$. *Continued.*

$\alpha = 0.07^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.178	.429	0.000	1.109	.995	0.000	.088	.742	.050	-1.122	.443
.150	-1.262	.408	.012	-.203	.670	.012	-.312	.643	.150	-1.132	.440
.300	-.763	.532	.025	-.731	.540	.025	-.570	.579	.300	-.742	.537
.450	-.647	.560	.050	-1.124	.442	.050	-1.126	.442	.450	-.604	.571
.600	-.597	.573	.100	-1.336	.390	.100	-1.263	.408	.600	-.574	.579
.800	-.378	.627	.150	-1.255	.410	.150	-1.151	.436	.800	-.326	.640
.990	.043	.731	.200	-1.243	.413	.200	-.904	.497			
			.300	-.759	.533	.300	-.855	.509			
			.350	-.772	.530	.350	-.759	.533			
			.400	-.736	.538	.400	-.717	.543			
			.450	-.745	.536	.450	-.733	.539			
			.500	-.781	.527	.500	-.748	.535			
			.550	-.743	.537	.550	-.693	.549			
			.600	-.683	.551	.600	-.656	.558			
			.650	-.657	.558	.700	-.442	.611			
			.700	-.595	.573	.800	-.237	.662			
			.800	-.329	.639	.900	-.079	.701			
			.900	-.051	.708	.950	-.066	.704			
			.950	.036	.730	.990	-.060	.706			
			.990	.047	.732						
					LOWER SURFACE						
.100	-.355	.633	.025	-.031	.713	.025	.084	.741	.100	-.749	.535
.300	-.595	.573	.050	-.395	.623	.050	-.418	.617	.300	-.605	.571
.600	-.286	.650	.100	-.524	.591	.100	-.573	.579	.600	-.357	.632
.800	.164	.761	.200	-.615	.568	.200	-.634	.564	.800	.223	.776
			.300	-.662	.557	.300	-.677	.553			
			.400	-.639	.562	.400	-.657	.558			
			.500	-.643	.561	.500	-.567	.580			
			.600	-.268	.654	.600	-.324	.640			
			.700	.080	.740	.700	.015	.724			
			.800	.260	.785	.800	.289	.792			
			.900	.361	.810	.900	.349	.807			
			.950	.349	.807	.950	.353	.808			
			1.000	.066	.737						
CN=				.4010			.3612				
CM=				-.1015			-.0897				

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.70. Continued.

$\alpha = 1.05^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.293	.401	0.000	1.081	.988	0.000	.096	.744	.050	-1.317	.394
.150	-1.467	.357	.012	-.348	.634	.012	-.448	.610	.150	-1.502	.349
.300	-.759	.533	.025	-.878	.503	.025	-.717	.543	.300	-.680	.552
.450	-.651	.559	.050	-1.265	.407	.050	-1.248	.411	.450	-.610	.570
.600	-.606	.570	.100	-1.512	.346	.100	-1.428	.367	.600	-.576	.578
.800	-.382	.626	.150	-1.455	.360	.150	-1.412	.371	.800	-.332	.638
.990	.057	.735	.200	-1.462	.359	.200	-1.344	.388			
			.300	-1.060	.458	.300	-1.163	.433			
			.350	-.658	.558	.350	-.653	.559			
			.400	-.647	.560	.400	-.658	.558			
			.450	-.708	.545	.450	-.715	.544			
			.500	-.748	.535	.500	-.745	.536			
			.550	-.744	.536	.550	-.719	.543			
			.600	-.697	.548	.600	-.673	.554			
			.650	-.674	.554	.700	-.482	.601			
			.700	-.610	.569	.800	-.310	.644			
			.800	-.355	.633	.900	-.075	.702			
			.900	-.050	.708	.950	-.032	.713			
			.950	.037	.730	.990	-.008	.719			
			.990	.075	.739						
					LOWER SURFACE						
.100	-.230	.564	.025	.096	.744	.025	.226	.777	.100	-.621	.567
.300	-.521	.592	.050	-.252	.658	.050	-.314	.643	.300	-.576	.578
.600	-.288	.649	.100	-.382	.626	.100	-.447	.610	.600	-.357	.632
.800	.210	.772	.200	-.506	.595	.200	-.502	.596	.800	.243	.781
			.300	-.577	.578	.300	-.606	.570			
			.400	-.577	.578	.400	-.607	.570			
			.500	-.582	.576	.500	-.542	.586			
			.600	-.251	.658	.600	-.303	.645			
			.700	.097	.745	.700	.027	.727			
			.800	.281	.790	.800	.307	.796			
			.900	.396	.819	.900	.363	.810			
			.950	.359	.809	.950	.368	.812			
			1.000	.077	.740						
CN=				.5208			.5035				
CM=				-.1007			-.0889				

(a) M = 0.70. Continued.

$\alpha = 2.06^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.447	.362	0.000	1.069	.985	0.000	.088	.742	.050	-1.416	.370
.150	-1.590	.327	.012	-.497	.597	.012	-.579	.577	.150	-1.698	.300
.300	-1.325	.393	.025	-.998	.473	.025	-.795	.524	.300	-.731	.540
.450	-.608	.570	.050	-1.411	.371	.050	-1.350	.386	.450	-.594	.573
.600	-.593	.574	.100	-1.626	.318	.100	-1.562	.334	.600	-.568	.580
.800	-.393	.623	.150	-1.584	.328	.150	-1.552	.336	.800	-.349	.634
.990	.072	.738	.200	-1.604	.323	.200	-1.481	.354			
			.300	-1.553	.336	.300	-1.484	.353			
			.350	-1.529	.342	.350	-1.160	.433			
			.400	-.794	.524	.400	-.685	.551			
			.450	-.616	.568	.450	-.607	.570			
			.500	-.622	.567	.500	-.626	.566			
			.550	-.651	.559	.550	-.618	.568			
			.600	-.642	.561	.600	-.648	.560			
			.650	-.637	.563	.700	-.478	.602			
			.700	-.591	.574	.800	-.342	.636			
			.800	-.366	.630	.900	-.072	.703			
			.900	-.063	.705	.950	-.007	.719			
			.950	.036	.729	.990	.033	.729			
			.990	.095	.744						
					LOWER SURFACE						
.100	-.168	.679	.025	.218	.775	.025	.349	.807	.100	-.471	.604
.300	-.464	.606	.050	-.089	.698	.050	-.172	.678	.300	-.510	.594
.600	-.264	.635	.100	-.268	.654	.100	-.310	.644	.600	-.347	.635
.800	.231	.778	.200	-.418	.617	.200	-.422	.616	.800	.254	.783
			.300	-.481	.601	.300	-.525	.590			
			.400	-.513	.594	.400	-.554	.583			
			.500	-.543	.586	.500	-.498	.597			
			.600	-.219	.666	.600	-.279	.651			
			.700	.118	.750	.700	.041	.731			
			.800	.300	.795	.800	.333	.803			
			.900	.397	.819	.900	.372	.813			
			.950	.376	.814	.950	.393	.818			
			1.000	.120	.750						
CN=				.6810			.6243				
CM=				-.1023			-.0877				

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(a) M = 0.70. Concluded.

$\alpha = 3.78^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.693	.304	0.000	1.020	.973	0.000	.091	.743	.050	-1.616	.321
.150	-1.795	.276	.012	-.691	.550	.012	-.787	.526	.150	-1.896	.251
.300	-1.647	.313	.025	-1.205	.423	.025	-1.041	.463	.300	-1.665	.309
.450	-.687	.551	.050	-1.578	.330	.050	-1.517	.345	.450	-.609	.570
.600	-.517	.593	.100	-1.778	.281	.100	-1.724	.294	.600	-.532	.589
.800	-.352	.633	.150	-1.739	.290	.150	-1.730	.292	.800	-.363	.631
.990	.066	.737	.200	-1.767	.283	.200	-1.718	.296			
			.300	-1.737	.291	.300	-1.734	.292			
			.350	-1.701	.300	.350	-1.720	.295			
			.400	-1.177	.429	.400	-1.646	.313			
			.450	-1.037	.464	.450	-.954	.485			
			.500	-1.005	.472	.500	-.793	.525			
			.550	-.839	.513	.550	-.609	.570			
			.600	-.633	.564	.600	-.518	.593			
			.650	-.485	.601	.700	-.427	.615			
			.700	-.440	.612	.800	-.336	.638			
			.800	-.270	.654	.900	-.083	.700			
			.900	-.067	.704	.950	.004	.722			
			.950	.025	.727	.990	.058	.735			
			.990	.030	.728						
					LOWER SURFACE						
.100	-.037	.711	.025	.406	.821	.025	.525	.851	.100	-.301	.646
.300	-.357	.632	.050	.084	.742	.050	.022	.726	.300	-.431	.614
.600	-.234	.663	.100	-.105	.695	.100	-.154	.682	.600	-.328	.640
.800	.272	.788	.200	-.270	.654	.200	-.292	.649	.800	.249	.782
			.300	-.384	.626	.300	-.426	.615			
			.400	-.417	.617	.400	-.489	.600			
			.500	-.473	.604	.500	-.443	.611			
			.600	-.194	.673	.600	-.245	.660			
			.700	.128	.752	.700	.061	.736			
			.800	.329	.802	.800	.338	.804			
			.900	.415	.823	.900	.395	.818			
			.950	.398	.819	.950	.418	.824			
			1.000	.093	.744						
C_N=					.8618			.8475			
C_M=					-.1054			-.0934			

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.75

$\alpha = -5.06^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.241	.623	0.000	1.107	.989	0.000	.099	.716	.050	-.233	.625
.150	-.487	.557	.012	.487	.820	.012	.421	.803	.150	-.447	.567
.300	-.547	.540	.025	.104	.717	.025	.155	.731	.300	-.559	.537
.450	-.426	.573	.050	-.239	.624	.050	-.228	.627	.450	-.546	.541
.600	-.558	.537	.100	-.412	.577	.100	-.353	.593	.600	-.589	.529
.800	-.381	.585	.150	-.429	.572	.150	-.342	.596	.800	-.310	.605
.990	.065	.706	.200	-.502	.552	.200	-.479	.559			
			.300	-.558	.537	.300	-.568	.534			
			.350	-.546	.541	.350	-.554	.538			
			.400	-.572	.534	.400	-.561	.537			
			.450	-.558	.537	.450	-.608	.524			
			.500	-.711	.496	.500	-.680	.504			
			.550	-.703	.498	.550	-.702	.498			
			.600	-.593	.528	.600	-.647	.513			
			.650	-.649	.513	.700	-.454	.565			
			.700	-.623	.520	.800	-.203	.634			
			.800	-.328	.600	.900	-.044	.677			
			.900	-.026	.682	.950	-.022	.683			
			.950	.053	.703	.990	-.007	.687			
			.990	.076	.709						
					LOWER SURFACE						
.100	-1.093	.392	.025	-.522	.547	.025	-.445	.568	.100	-1.431	.301
.300	-1.350	.323	.050	-1.103	.389	.050	-1.002	.417	.300	-1.403	.308
.600	-.316	.603	.100	-1.259	.347	.100	-1.294	.338	.600	-.373	.588
.800	.040	.699	.200	-1.330	.328	.200	-1.332	.328	.800	.044	.701
			.300	-1.020	.412	.300	-1.370	.317			
			.400	-.733	.490	.400	-.878	.451			
			.500	-.582	.531	.500	-.619	.521			
			.600	-.428	.573	.600	-.335	.598			
			.700	-.319	.602	.700	-.262	.617			
			.800	-.107	.660	.800	-.068	.670			
			.900	.224	.749	.900	.053	.703			
			.950	.175	.736	.950	.094	.714			
			1.000	.114	.720						
CN=				-.1896			-.2448				
CM=				-.0798			-.0562				

(b) M = 0.75. Continued.

$\alpha = -3.44^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.510	.550	0.000	1.128	.994	0.000	.102	.716	.050	-.483	.558
.150	-.625	.519	.012	.360	.786	.012	.281	.765	.150	-.597	.527
.300	-.631	.518	.025	-.055	.674	.025	-.006	.687	.300	-.629	.518
.450	-.510	.550	.050	-.478	.559	.050	-.462	.563	.450	-.569	.534
.600	-.580	.531	.100	-.565	.535	.100	-.562	.536	.600	-.594	.528
.800	-.361	.591	.150	-.593	.528	.150	-.517	.548	.800	-.307	.605
.990	.069	.707	.200	-.758	.483	.200	-.623	.520			
			.300	-.724	.492	.300	-.683	.503			
			.350	-.654	.511	.350	-.639	.515			
			.400	-.646	.514	.400	-.616	.522			
			.450	-.618	.521	.450	-.680	.504			
			.500	-.774	.479	.500	-.744	.487			
			.550	-.789	.475	.550	-.811	.469			
			.600	-.613	.522	.600	-.649	.513			
			.650	-.658	.510	.700	-.425	.573			
			.700	-.588	.529	.800	-.221	.629			
			.800	-.315	.603	.900	-.051	.675			
			.900	-.010	.686	.950	-.034	.679			
			.950	.048	.702	.990	-.024	.682			
			.990	.089	.713						
					LOWER SURFACE						
.100	-.902	.444	.025	-.368	.589	.025	-.284	.612	.100	-1.284	.341
.300	-1.131	.387	.050	-.945	.432	.050	-.860	.455	.300	-1.330	.328
.600	-.252	.620	.100	-1.085	.394	.100	-1.153	.376	.600	-.343	.596
.800	.032	.697	.200	-1.161	.374	.200	-1.205	.362	.800	.187	.739
			.300	-1.241	.352	.300	-1.254	.349			
			.400	-1.306	.335	.400	-1.364	.319			
			.500	-.558	.537	.500	-.590	.529			
			.600	-.218	.630	.600	-.263	.617			
			.700	.054	.703	.700	.015	.693			
			.800	.231	.751	.800	.257	.758			
			.900	.342	.781	.900	.301	.770			
			.950	.336	.780	.950	.330	.778			
			1.000	.094	.714						
CN=				-.0313			-.0650				
CM=				-.1195			-.1029				

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.75. Continued.

$\alpha = -2.60^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.581	.541	0.000	1.132	.995	0.000	.099	.716	.050	-.611	.523
.150	-.769	.480	.012	.207	.745	.012	.211	.746	.150	-.789	.475
.300	-.722	.493	.025	-.174	.642	.025	-.114	.658	.300	-.820	.466
.450	-.555	.538	.050	-.562	.536	.050	-.567	.535	.450	-.595	.527
.600	-.580	.531	.100	-.675	.506	.100	-.696	.500	.600	-.611	.523
.800	-.354	.593	.150	-.672	.507	.150	-.645	.514	.800	-.290	.610
.990	.060	.705	.200	-.799	.472	.200	-.724	.492			
			.300	-.777	.478	.300	-.806	.470			
			.350	-.759	.483	.350	-.767	.481			
			.400	-.659	.510	.400	-.628	.518			
			.450	-.642	.515	.450	-.689	.502			
			.500	-.805	.471	.500	-.754	.484			
			.550	-.850	.458	.550	-.855	.457			
			.600	-.674	.506	.600	-.677	.505			
			.650	-.653	.512	.700	-.424	.574			
			.700	-.542	.542	.800	-.224	.628			
			.800	-.294	.609	.900	-.062	.672			
			.900	-.017	.684	.950	-.044	.677			
			.950	.038	.699	.990	-.042	.677			
			.990	.069	.707						
					LOWER SURFACE						
.100	-.742	.488	.025	-.287	.611	.025	-.207	.632	.100	-1.213	.360
.300	-1.045	.405	.050	-.773	.479	.050	-.769	.480	.300	-1.140	.380
.600	-.727	.627	.100	-.980	.423	.100	-1.052	.403	.600	-.349	.594
.800	.058	.704	.200	-1.025	.411	.200	-1.097	.391	.800	.188	.740
			.300	-1.118	.386	.300	-1.162	.374			
			.400	-1.154	.376	.400	-1.258	.348			
			.500	-.543	.541	.500	-.525	.546			
			.600	-.229	.626	.600	-.262	.618			
			.700	.059	.705	.700	.039	.699			
			.800	.215	.747	.800	.256	.758			
			.900	.341	.781	.900	.306	.772			
			.950	.336	.780	.950	.326	.777			
			1.000	.093	.714						
CN=				.0583			.0393				
CM=				-.1165			-.1049				

(b) M = 0.75. Continued.

$\alpha = -1.58^{\circ}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.767	.481	0.000	1.131	.995	0.000	.093	.714	.050	-.737	.489
.150	-.937	.445	.012	.118	.720	.012	.039	.699	.150	-1.014	.414
.300	-.741	.488	.025	-.327	.600	.025	-.218	.629	.300	-.843	.460
.450	-.603	.525	.050	-.730	.490	.050	-.690	.501	.450	-.616	.521
.600	-.593	.528	.100	-.975	.424	.100	-.858	.456	.600	-.607	.524
.800	-.356	.592	.150	-.950	.431	.150	-.845	.459	.800	-.283	.612
.990	.060	.705	.200	-.882	.449	.200	-.761	.482			
			.300	-.926	.437	.300	-.934	.435			
			.350	-.954	.430	.350	-.898	.445			
			.400	-.821	.466	.400	-.861	.455			
			.450	-.685	.503	.450	-.740	.488			
			.500	-.750	.485	.500	-.708	.496			
			.550	-.811	.469	.550	-.798	.472			
			.600	-.678	.505	.600	-.698	.499			
			.650	-.644	.514	.700	-.422	.574			
			.700	-.574	.533	.800	-.235	.625			
			.800	-.294	.609	.900	-.059	.672			
			.900	-.010	.686	.950	-.051	.675			
			.950	.051	.702	.990	-.042	.677			
			.990	.076	.709						
					LOWER SURFACE						
.100	-.587	.529	.025	-.199	.635	.025	-.081	.667	.100	-1.119	.385
.300	-.941	.433	.050	-.646	.513	.050	-.657	.510	.300	-.709	.496
.600	-.229	.626	.100	-.840	.461	.100	-.950	.431	.600	-.346	.595
.800	.088	.713	.200	-.914	.441	.200	-.875	.451	.800	.169	.734
			.300	-.942	.433	.300	-1.041	.406			
			.400	-.976	.424	.400	-1.151	.376			
			.500	-.654	.511	.500	-.564	.536			
			.600	-.232	.625	.600	-.291	.610			
			.700	.074	.709	.700	.020	.694			
			.800	.232	.752	.800	.275	.763			
			.900	.334	.779	.900	.327	.777			
			.950	.327	.777	.950	.345	.782			
			1.000	.088	.712						
CN=				.1887			.1553				
CM=				-.1093			-.1017				

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Continued

(b) M = 0.75. Continued.

$\alpha = -0.59^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.870	.453	0.000	1.138	.997	0.000	.104	.717	.050	-.878	.450
.150	-1.094	.392	.012	.019	.694	.012	-.060	.672	.150	-1.216	.359
.300	-1.032	.409	.025	-.466	.562	.025	-.378	.586	.300	-.953	.430
.450	-.579	.532	.050	-.848	.459	.050	-.841	.461	.450	-.649	.513
.600	-.582	.531	.100	-1.105	.389	.100	-1.015	.413	.600	-.607	.524
.800	-.357	.592	.150	-1.058	.402	.150	-.997	.418	.800	-.282	.612
.990	.060	.705	.200	-1.089	.393	.200	-.978	.423			
			.300	-1.085	.395	.300	-1.063	.400			
			.350	-1.115	.386	.350	-1.043	.406			
			.400	-1.035	.408	.400	-1.057	.402			
			.450	-1.021	.412	.450	-1.104	.389			
			.500	-1.006	.416	.500	-.820	.466			
			.550	-.598	.527	.550	-.693	.501			
			.600	-.568	.535	.600	-.607	.524			
			.650	-.620	.521	.700	-.418	.575			
			.700	-.538	.543	.800	-.239	.624			
			.800	-.312	.604	.900	-.059	.673			
			.900	-.025	.682	.950	-.037	.679			
			.950	.043	.700	.990	-.034	.679			
			.990	.069	.707						
					LOWER SURFACE						
.100	-.423	.574	.025	-.065	.671	.025	.068	.707	.100	-.954	.430
.300	-.762	.482	.050	-.507	.551	.050	-.577	.532	.300	-.694	.500
.600	-.238	.624	.100	-.649	.513	.100	-.667	.508	.600	-.353	.593
.800	.121	.721	.200	-.759	.483	.200	-.791	.474	.800	.172	.735
			.300	-.849	.458	.300	-.928	.437			
			.400	-.783	.476	.400	-.792	.474			
			.500	-.705	.498	.500	-.624	.519			
			.600	-.242	.623	.600	-.296	.608			
			.700	.080	.710	.700	.023	.695			
			.800	.239	.753	.800	.290	.767			
			.900	.361	.786	.900	.337	.780			
			.950	.350	.783	.950	.354	.785			
			1.000	.105	.717						
CN=				.3348			.3175				
CM=				-.1090			-.1007				

(b) M = 0.75. Continued.

$\alpha = 0.59^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.046	.405	0.000	1.129	.995	0.000	.109	.718	.050	-1.034	.408
.150	-1.232	.355	.012	-.122	.655	.012	-.211	.631	.150	-1.299	.336
.300	-1.212	.360	.025	-.626	.519	.025	-.510	.550	.300	-1.248	.350
.450	-1.071	.398	.050	-1.004	.416	.050	-.983	.422	.450	-.682	.504
.600	-.520	.547	.100	-1.224	.357	.100	-1.167	.372	.600	-.597	.527
.800	-.352	.593	.150	-1.204	.362	.150	-1.173	.371	.800	-.284	.612
.990	.088	.712	.200	-1.252	.349	.200	-1.155	.375			
			.300	-1.238	.353	.300	-1.210	.360			
			.350	-1.243	.351	.350	-1.225	.356			
			.400	-1.253	.349	.400	-1.259	.347			
			.450	-1.249	.350	.450	-1.280	.341			
			.500	-1.280	.341	.500	-1.277	.342			
			.550	-.930	.436	.550	-.791	.474			
			.600	-.670	.507	.600	-.617	.521			
			.650	-.512	.550	.700	-.394	.582			
			.700	-.441	.569	.800	-.259	.618			
			.800	-.274	.614	.900	-.047	.676			
			.900	-.040	.678	.950	-.007	.687			
			.950	.059	.704	.990	.012	.692			
			.990	.097	.715						
					LOWER SURFACE						
.100	-.323	.601	.025	.056	.704	.025	.146	.728	.100	-.766	.481
.300	-.612	.522	.050	-.331	.599	.050	-.414	.576	.300	-.681	.504
.600	-.230	.626	.100	-.511	.550	.100	-.488	.556	.600	-.362	.591
.800	.164	.733	.200	-.646	.513	.200	-.651	.512	.800	.214	.746
			.300	-.698	.499	.300	-.845	.459			
			.400	-.672	.506	.400	-.684	.503			
			.500	-.657	.510	.500	-.631	.517			
			.600	-.224	.628	.600	-.291	.610			
			.700	.103	.717	.700	.035	.698			
			.800	.263	.760	.800	.301	.770			
			.900	.369	.789	.900	.366	.788			
			.950	.380	.792	.950	.377	.791			
			1.000	.116	.720						
CN=				.5045			.4820				
CM=				-.1164			-.1059				

[redacted]

TABLE VI.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL OFF; WAKE RAKE ON; AILERON UNSEALED - Concluded

(b) M = 0.75. Concluded.

$\alpha = 1.34^{o}$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.145	.478	0.000	1.122	.993	0.000	.096	.715	.050	-1.095	.392
.150	-1.318	.331	.012	-.198	.635	.012	-.278	.613	.150	-1.382	.314
.300	-1.232	.355	.025	-.679	.505	.025	-.533	.544	.300	-1.412	.306
.450	-1.155	.376	.050	-1.059	.402	.050	-1.058	.402	.450	-.700	.499
.600	-.510	.551	.100	-1.304	.335	.100	-1.230	.355	.600	-.556	.538
.800	-.336	.598	.150	-1.292	.339	.150	-1.251	.350	.800	-.269	.616
.990	.082	.711	.200	-1.321	.331	.200	-1.238	.353			
			.300	-1.323	.330	.300	-1.292	.338			
			.350	-1.337	.326	.350	-1.310	.334			
			.400	-1.332	.328	.400	-1.297	.337			
			.450	-1.299	.337	.450	-1.351	.323			
			.500	-1.343	.325	.500	-1.373	.316			
			.550	-.803	.471	.550	-.848	.459			
			.600	-.665	.508	.600	-.671	.507			
			.650	-.571	.534	.700	-.396	.581			
			.700	-.450	.567	.800	-.276	.614			
			.800	-.216	.630	.900	-.071	.669			
			.900	-.056	.673	.950	-.001	.689			
			.950	-.017	.684	.990	.030	.697			
			.990	.005	.690						
					LOWER SURFACE						
.100	-.229	.627	.025	.120	.721	.025	.269	.762	.100	-.660	.510
.300	-.559	.537	.050	-.232	.626	.050	-.303	.606	.300	-.639	.515
.600	-.247	.622	.100	-.405	.579	.100	-.457	.565	.600	-.363	.590
.800	.172	.735	.200	-.551	.539	.200	-.545	.541	.800	.232	.751
			.300	-.629	.518	.300	-.753	.485			
			.400	-.642	.515	.400	-.693	.501			
			.500	-.647	.513	.500	-.619	.521			
			.600	-.236	.625	.600	-.287	.611			
			.700	.104	.717	.700	.044	.701			
			.800	.273	.763	.800	.312	.773			
			.900	.370	.789	.900	.369	.789			
			.950	.355	.785	.950	.387	.793			
			1.000	.045	.701						
CN=				.5758			.5652				
CM=				-.1154			-.1107				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED

(a) M = 0.70

$\alpha = -4.64^{\circ}$; $C_L = -0.192$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.297	.647	0.000	1.080	.988	0.000	.078	.740	.050	-.312	.643
.150	-.508	.595	.012	.477	.839	.012	.394	.818	.150	-.409	.619
.300	-.525	.591	.025	.084	.742	.025	.099	.745	.300	-.535	.588
.450	-.427	.615	.050	-.303	.646	.050	-.235	.663	.450	-.541	.587
.600	-.522	.591	.100	-.395	.623	.100	-.351	.634	.600	-.575	.578
.800	-.409	.620	.150	-.456	.608	.150	-.363	.631	.800	-.381	.627
.990	.078	.740	.200	-.501	.597	.200	-.482	.601			
			.300	-.537	.588	.300	-.540	.587			
			.350	-.540	.587	.350	-.546	.586			
			.400	-.534	.589	.400	-.538	.588			
			.450	-.545	.586	.450	-.595	.574			
			.500	-.636	.563	.500	-.645	.561			
			.550	-.654	.559	.550	-.645	.561			
			.600	-.566	.581	.600	-.647	.561			
			.650	-.635	.564	.700	-.542	.587			
			.700	-.588	.575	.800	-.333	.638			
			.800	-.368	.630	.900	-.022	.715			
			.900	-.043	.710	.950	.043	.731			
			.950	.069	.738	.990	.065	.737			
			.990	.105	.747						
					LOWER SURFACE						
.100	-1.241	.414	.025	-.682	.552	.025	-.588	.575	.100	-1.631	.317
.300	-.794	.524	.050	-1.268	.407	.050	-1.200	.424	.300	-.617	.568
.600	-.254	.658	.100	-1.423	.369	.100	-1.436	.365	.600	-.272	.653
.800	.064	.736	.200	-1.413	.371	.200	-1.470	.357	.800	.070	.738
			.300	-.833	.515	.300	-1.117	.444			
			.400	-.710	.545	.400	-.629	.565			
			.500	-.682	.552	.500	-.567	.580			
			.600	-.280	.651	.600	-.269	.654			
			.700	.056	.735	.700	.030	.728			
			.800	.198	.770	.800	.205	.772			
			.900	.307	.797	.900	.265	.786			
			.950	.321	.800	.950	.291	.793			
			1.000	.115	.749						
CN=				-.1221			-.1219				
CM=				-.1299			-.1233				

(a) M = 0.70. Continued.

$\alpha = -3.09^{\circ}$; $C_L = -0.033$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.521	.592	0.000	1.106	.994	0.000	.079	.740	.050	-.589	.575
.150	-.644	.561	.012	.277	.789	.012	.228	.777	.150	-.594	.574
.300	-.524	.566	.025	-.171	.679	.025	-.062	.705	.300	-.611	.569
.450	-.506	.595	.050	-.501	.597	.050	-.516	.593	.450	-.583	.576
.600	-.551	.584	.100	-.597	.575	.100	-.570	.580	.600	-.591	.574
.800	-.393	.624	.150	-.610	.570	.150	-.505	.596	.800	-.368	.630
.990	.072	.738	.200	-.651	.560	.200	-.612	.569			
			.300	-.640	.562	.300	-.639	.563			
			.350	-.634	.564	.350	-.618	.568			
			.400	-.618	.568	.400	-.604	.571			
			.450	-.623	.567	.450	-.639	.563			
			.500	-.690	.550	.500	-.696	.549			
			.550	-.688	.550	.550	-.684	.552			
			.600	-.614	.569	.600	-.671	.555			
			.650	-.639	.563	.700	-.537	.588			
			.700	-.578	.578	.800	-.297	.647			
			.800	-.349	.634	.900	-.022	.715			
			.900	-.028	.714	.950	.035	.729			
			.950	.056	.735	.990	.053	.734			
			.990	.098	.745						
					LOWER SURFACE						
.100	-.996	.474	.025	-.498	.597	.025	-.363	.631	.100	-1.421	.369
.300	-.784	.527	.050	-1.039	.464	.050	-.966	.482	.300	-.658	.558
.600	-.288	.649	.100	-1.183	.428	.100	-1.256	.410	.600	-.286	.650
.800	.059	.738	.200	-.945	.487	.200	-.969	.481	.800	.084	.742
			.300	-.881	.503	.300	-.865	.507			
			.400	-.760	.533	.400	-.744	.537			
			.500	-.681	.552	.500	-.588	.575			
			.600	-.261	.656	.600	-.264	.656			
			.700	.034	.729	.700	.022	.726			
			.800	.148	.757	.800	.148	.757			
			.900	.251	.783	.900	.204	.771			
			.950	.276	.789	.950	.267	.787			
			1.000	.102	.746						
CN=				.0050			.0235				
CM=				-.1088			-.1031				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(a) M = 0.70. Continued.

$\alpha = -2.20^{\circ}$; $C_L = 0.074$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.693	.550	0.000	1.113	.996	0.000	.084	.741	.050	-.730	.540
.150	-.775	.529	.012	.151	.758	.012	.037	.730	.150	-.682	.552
.300	-.663	.557	.025	-.297	.647	.025	-.244	.660	.300	-.662	.557
.450	-.543	.586	.050	-.722	.542	.050	-.682	.552	.450	-.600	.572
.600	-.565	.581	.100	-.729	.540	.100	-.698	.548	.600	-.606	.571
.800	-.337	.625	.150	-.716	.544	.150	-.623	.567	.800	-.359	.632
.990	.055	.737	.200	-.765	.532	.200	-.712	.545			
			.300	-.728	.541	.300	-.714	.544			
			.350	-.674	.554	.350	-.690	.550			
			.400	-.675	.554	.400	-.658	.558			
			.450	-.659	.558	.450	-.690	.550			
			.500	-.714	.544	.500	-.733	.539			
			.550	-.712	.545	.550	-.707	.546			
			.600	-.639	.563	.600	-.684	.552			
			.650	-.653	.559	.700	-.536	.588			
			.700	-.588	.575	.800	-.294	.648			
			.800	-.336	.638	.900	-.019	.716			
			.900	-.021	.715	.950	.018	.725			
			.950	.040	.731	.990	.034	.729			
			.990	.084	.741						
					LOWER SURFACE						
.100	-.787	.526	.025	-.365	.630	.025	-.246	.660	.100	-1.265	.468
.300	-.729	.540	.050	-.823	.517	.050	-.838	.513	.300	-.670	.555
.600	-.231	.649	.100	-.895	.499	.100	-.577	.479	.600	-.286	.650
.800	.104	.746	.200	-.894	.499	.200	-.855	.509	.800	.086	.742
			.300	-.824	.517	.300	-.839	.513			
			.400	-.741	.537	.400	-.722	.542			
			.500	-.677	.553	.500	-.592	.574			
			.600	-.268	.654	.600	-.265	.655			
			.700	.057	.735	.700	.031	.728			
			.800	.175	.764	.800	.170	.763			
			.900	.285	.791	.900	.240	.780			
			.950	.299	.795	.950	.299	.795			
			1.000	.102	.746						
CN=				.1215			.1288				
CM=				-.1059			-.1009				

(a) M = 0.70. Continued.

$\alpha = -1.38^{\circ}$; $C_L = 0.174$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.903	.497	0.000	1.113	.996	0.000	.087	.742	.050	-.969	.481
.150	-.849	.510	.012	.021	.726	.012	-.072	.703	.150	-.777	.528
.300	-.740	.538	.025	-.413	.618	.025	-.327	.640	.300	-.733	.539
.450	-.553	.581	.050	-.874	.504	.050	-.780	.528	.450	-.635	.564
.600	-.580	.577	.100	-.925	.492	.100	-.824	.517	.600	-.616	.568
.800	-.342	.626	.150	-.831	.515	.150	-.723	.542	.800	-.348	.634
.990	.051	.733	.200	-.858	.508	.200	-.788	.526			
			.300	-.780	.528	.300	-.794	.524			
			.350	-.734	.539	.350	-.719	.543			
			.400	-.704	.546	.400	-.703	.547			
			.450	-.687	.551	.450	-.725	.541			
			.500	-.738	.538	.500	-.772	.530			
			.550	-.736	.539	.550	-.734	.539			
			.600	-.668	.555	.600	-.693	.549			
			.650	-.657	.558	.700	-.536	.588			
			.700	-.587	.576	.800	-.294	.648			
			.800	-.332	.638	.900	-.036	.712			
			.900	-.018	.716	.950	.000	.721			
			.950	.041	.731	.990	.020	.726			
			.990	.067	.737						
					LOWER SURFACE						
.100	-.641	.562	.025	-.236	.662	.025	-.115	.692	.100	-1.028	.466
.300	-.635	.551	.050	-.665	.556	.050	-.686	.551	.300	-.653	.559
.600	-.301	.646	.100	-.703	.547	.100	-.766	.531	.600	-.257	.647
.800	.113	.749	.200	-.747	.536	.200	-.757	.533	.800	.104	.746
			.300	-.739	.538	.300	-.779	.528			
			.400	-.717	.543	.400	-.695	.549			
			.500	-.664	.556	.500	-.567	.580			
			.600	-.262	.656	.600	-.274	.653			
			.700	.059	.735	.700	.044	.732			
			.800	.214	.774	.800	.199	.770			
			.900	.302	.795	.900	.267	.787			
			.950	.312	.798	.950	.314	.798			
			1.000	.049	.738						
CN=				.2299			.2247				
CM=				-.1032			-.1014				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(a) M = 0.70. Continued.

$\alpha = 1.26^{\circ}$; $C_L = 0.498$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.362	.383	0.000	1.082	.988	0.000	.097	.745	.050	-1.419	.370
.150	-1.478	.355	.012	-.325	.640	.012	-.456	.608	.150	-1.552	.336
.300	-.750	.535	.025	-.899	.498	.025	-.696	.548	.300	-.665	.556
.450	-.639	.562	.050	-1.287	.402	.050	-1.285	.403	.450	-.660	.557
.600	-.605	.571	.100	-1.558	.335	.100	-1.474	.356	.600	-.626	.566
.800	-.392	.624	.150	-1.467	.358	.150	-1.425	.368	.800	-.387	.625
.990	.065	.737	.200	-1.491	.352	.200	-1.404	.373			
			.300	-1.443	.364	.300	-1.331	.391			
			.350	-.929	.491	.350	-.727	.541			
			.400	-.634	.564	.400	-.665	.556			
			.450	-.662	.557	.450	-.731	.540			
			.500	-.737	.538	.500	-.770	.530			
			.550	-.742	.537	.550	-.756	.534			
			.600	-.695	.549	.600	-.705	.546			
			.650	-.677	.553	.700	-.546	.585			
			.700	-.602	.572	.800	-.306	.645			
			.800	-.342	.636	.900	-.043	.710			
			.900	-.041	.711	.950	-.003	.720			
			.550	.033	.729	.990	.011	.723			
			.990	.069	.738						
					LOWER SURFACE						
.100	-.312	.644	.025	.115	.749	.025	.261	.785	.100	-.538	.587
.300	-.502	.597	.050	-.205	.670	.050	-.278	.652	.300	-.532	.589
.600	-.280	.651	.100	-.364	.631	.100	-.398	.622	.600	-.288	.649
.800	.192	.768	.200	-.489	.600	.200	-.486	.600	.800	.188	.767
			.300	-.563	.581	.300	-.560	.582			
			.400	-.572	.579	.400	-.576	.578			
			.500	-.578	.577	.500	-.499	.597			
			.600	-.230	.664	.600	-.258	.657			
			.700	.101	.746	.700	.074	.739			
			.800	.270	.787	.800	.251	.783			
			.900	.373	.813	.900	.299	.795			
			.950	.347	.807	.950	.337	.804			
			1.000	.078	.740						
CN=				.5705			.5548				
CM=				-.0998			-.0884				

(a) M = 0.70. Concluded.

$\alpha = 3.81^{\circ}$; $C_L = 0.812$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.681	.305	0.000	.998	.968	0.000	.094	.744	.050	-1.671	.308
.150	-1.798	.276	.012	-.634	.564	.012	-.823	.517	.150	-1.891	.253
.300	-1.674	.307	.025	-1.191	.426	.025	-1.077	.455	.300	-1.697	.301
.450	-.732	.547	.050	-1.582	.330	.050	-1.513	.347	.450	-.599	.573
.600	-.519	.592	.100	-1.783	.280	.100	-1.759	.286	.600	-.586	.576
.800	-.355	.633	.150	-1.741	.290	.150	-1.712	.297	.800	-.324	.641
.990	.073	.739	.200	-1.754	.287	.200	-1.713	.297			
			.300	-1.753	.287	.300	-1.720	.295			
			.350	-1.730	.293	.350	-1.726	.294			
			.400	-1.196	.425	.400	-1.672	.307			
			.450	-1.068	.457	.450	-1.029	.466			
			.500	-.971	.481	.500	-.873	.505			
			.550	-.834	.515	.550	-.668	.556			
			.600	-.628	.566	.600	-.573	.579			
			.650	-.486	.601	.700	-.470	.605			
			.700	-.418	.617	.800	-.306	.645			
			.800	-.264	.656	.900	-.074	.703			
			.900	-.060	.706	.950	.015	.725			
			.550	.030	.728	.990	.067	.737			
			.990	.080	.741						
					LOWER SURFACE						
.100	-.059	.706	.025	.395	.818	.025	.512	.848	.100	-.276	.653
.300	-.353	.633	.050	.135	.754	.050	.048	.733	.300	-.435	.613
.600	-.236	.662	.100	-.092	.698	.100	-.144	.685	.600	-.269	.654
.800	.253	.784	.200	-.253	.658	.200	-.292	.649	.800	.208	.772
			.300	-.374	.628	.300	-.400	.622			
			.400	-.424	.616	.400	-.467	.605			
			.500	-.479	.602	.500	-.411	.619			
			.600	-.193	.673	.600	-.211	.669			
			.700	.124	.751	.700	.095	.744			
			.800	.325	.801	.800	.290	.793			
			.900	.426	.826	.900	.347	.807			
			.950	.396	.819	.950	.380	.815			
			1.000	.087	.742						
CN=				.8596			.8696				
CM=				-.1020			-.0937				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(b) M = 0.73

$\alpha = -4.68^{\circ}$; $C_L = -0.216$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.283	.627	0.000	1.097	.988	0.000	.089	.724	.050	-.313	.619
.150	-.515	.566	.012	.474	.825	.012	.413	.809	.150	-.453	.582
.300	-.551	.557	.025	.110	.730	.025	.147	.740	.300	-.565	.553
.450	-.430	.588	.050	-.295	.624	.050	-.233	.640	.450	-.565	.553
.600	-.545	.558	.100	-.399	.596	.100	-.362	.606	.600	-.618	.539
.800	-.401	.596	.150	-.448	.584	.150	-.379	.602	.800	-.351	.609
.990	.074	.721	.200	-.542	.559	.200	-.482	.575			
			.250	-.577	.550	.300	-.568	.552			
			.350	-.568	.552	.350	-.579	.549			
			.400	-.554	.556	.400	-.566	.553			
			.450	-.582	.549	.450	-.624	.538			
			.500	-.679	.523	.500	-.695	.519			
			.550	-.704	.517	.550	-.708	.516			
			.600	-.591	.546	.600	-.690	.520			
			.650	-.663	.527	.700	-.551	.557			
			.700	-.595	.545	.800	-.287	.626			
			.800	-.346	.610	.900	-.018	.696			
			.900	-.025	.695	.950	.041	.712			
			.950	.067	.719	.990	.058	.716			
			.990	.095	.726						
					LOWER SURFACE						
.100	-1.157	.398	.025	-.548	.558	.025	-.479	.576	.100	-1.450	.321
.300	-1.317	.356	.050	-1.151	.399	.050	-1.082	.418	.300	-1.349	.348
.600	-.236	.639	.100	-1.339	.350	.100	-1.345	.349	.600	-.254	.634
.800	.071	.720	.200	-1.349	.348	.200	-1.404	.333	.800	.074	.721
			.300	-1.414	.331	.300	-1.476	.314			
			.400	-1.032	.431	.400	-.984	.443			
			.500	-.501	.570	.500	-.588	.547			
			.600	-.246	.637	.600	-.213	.645			
			.700	.060	.717	.700	.049	.714			
			.800	.252	.767	.800	.212	.757			
			.900	.329	.787	.900	.276	.774			
			.950	.302	.780	.950	.303	.780			
			1.000	.107	.729						
CN=				-.1517			-.1520				
CM=				-.1304			-.1182				

(b) M = 0.73. Continued.

$\alpha = -3.08^{\circ}$; $C_L = -0.037$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.532	.562	0.000	1.115	.993	0.000	.093	.726	.050	-.574	.551
.150	-.658	.526	.012	.303	.781	.012	.238	.764	.150	-.628	.537
.300	-.657	.529	.025	-.138	.665	.025	-.034	.692	.300	-.651	.531
.450	-.518	.566	.050	-.485	.574	.050	-.452	.583	.450	-.619	.539
.600	-.568	.552	.100	-.617	.539	.100	-.607	.542	.600	-.638	.534
.800	-.375	.603	.150	-.631	.536	.150	-.519	.565	.800	-.352	.609
.990	.056	.718	.200	-.697	.519	.200	-.635	.535			
			.300	-.694	.519	.300	-.700	.518			
			.350	-.675	.524	.350	-.658	.529			
			.400	-.647	.532	.400	-.637	.534			
			.450	-.655	.530	.450	-.690	.521			
			.500	-.744	.506	.500	-.765	.501			
			.550	-.743	.507	.550	-.763	.501			
			.600	-.634	.535	.600	-.704	.517			
			.650	-.665	.527	.700	-.544	.559			
			.700	-.588	.547	.800	-.272	.630			
			.800	-.319	.617	.900	-.022	.695			
			.900	-.016	.697	.950	.012	.704			
			.950	.054	.715	.990	.020	.707			
			.990	.072	.720						
					LOWER SURFACE						
.100	-.948	.453	.025	-.438	.586	.025	-.277	.629	.100	-1.347	.348
.300	-.872	.473	.050	-.942	.454	.050	-.884	.470	.300	-.774	.498
.600	-.246	.637	.100	-1.138	.403	.100	-1.169	.395	.600	-.279	.628
.800	.090	.722	.200	-1.145	.401	.200	-1.174	.394	.800	.115	.731
			.300	-1.146	.401	.300	-1.224	.381			
			.400	-.682	.522	.400	-.625	.537			
			.500	-.686	.521	.500	-.550	.557			
			.600	-.267	.631	.600	-.257	.634			
			.700	.059	.717	.700	.052	.715			
			.800	.217	.758	.800	.215	.757			
			.900	.335	.789	.900	.286	.776			
			.950	.327	.787	.950	.310	.782			
			1.000	.092	.725						
CN=				.0121			.0355				
CM=				-.1225			-.1175				

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(b) M = 0.73. Continued.

$\alpha = -1.42^{\circ}$; $C_L = 0.156$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.874	.472	0.000	1.132	.998	0.000	.088	.724	.050	-.898	.466
.150	-.988	.442	.012	.120	.733	.012	.029	.709	.150	-.990	.468
.300	-.786	.495	.025	-.387	.600	.025	-.277	.629	.300	-.803	.491
.450	-.579	.549	.050	-.769	.500	.050	-.767	.500	.450	-.648	.531
.600	-.586	.548	.100	-.970	.447	.100	-.894	.467	.600	-.649	.531
.800	-.374	.603	.150	-.780	.497	.150	-.737	.508	.800	-.307	.621
.990	.055	.716	.200	-.906	.464	.200	-.789	.495			
			.300	-.855	.477	.300	-.917	.461			
			.350	-.813	.488	.350	-.859	.476			
			.400	-.710	.515	.400	-.660	.528			
			.450	-.710	.515	.450	-.725	.511			
			.500	-.824	.485	.500	-.804	.490			
			.550	-.803	.491	.550	-.804	.490			
			.600	-.674	.525	.600	-.700	.518			
			.650	-.657	.529	.700	-.520	.565			
			.700	-.570	.552	.800	-.263	.632			
			.800	-.286	.626	.900	-.040	.691			
			.900	-.026	.694	.950	-.006	.699			
			.950	.033	.710	.990	.009	.704			
			.990	.058	.716						
					LOWER SURFACE						
.100	-.690	.520	.025	-.189	.652	.025	-.077	.681	.100	-1.137	.403
.300	-.764	.501	.050	-.667	.526	.050	-.676	.524	.300	-.675	.524
.600	-.292	.624	.100	-.835	.482	.100	-.878	.471	.600	-.287	.626
.800	.087	.724	.200	-.854	.477	.200	-.873	.472	.800	.085	.723
			.300	-.820	.486	.300	-.974	.446			
			.400	-.761	.502	.400	-.705	.517			
			.500	-.693	.520	.500	-.602	.543			
			.600	-.262	.633	.600	-.271	.630			
			.700	.056	.716	.700	.050	.714			
			.800	.210	.756	.800	.187	.750			
			.900	.323	.786	.900	.260	.769			
			.950	.334	.789	.950	.321	.785			
			1.000	.076	.721						
CN=				.2004			.1994				
CM=				-.1094			-.1017				

(b) M = 0.73. Continued.

$\alpha = -0.46^{\circ}$; $C_L = 0.279$.

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.968	.448	0.000	1.121	.995	0.000	.087	.724	.050	-1.106	.412
.150	-1.171	.394	.012	-.042	.690	.012	-.175	.655	.150	-1.143	.402
.300	-.743	.507	.025	-.498	.571	.025	-.394	.598	.300	-.694	.519
.450	-.638	.534	.050	-.921	.460	.050	-.922	.460	.450	-.667	.526
.600	-.537	.545	.100	-1.185	.391	.100	-1.126	.406	.600	-.654	.530
.800	-.364	.606	.150	-1.110	.410	.150	-1.028	.432	.800	-.332	.614
.990	.052	.717	.200	-1.144	.401	.200	-1.027	.432			
			.300	-1.063	.423	.300	-.955	.451			
			.350	-.754	.504	.350	-1.070	.421			
			.400	-.625	.537	.400	-.678	.523			
			.450	-.703	.517	.450	-.718	.513			
			.500	-.818	.487	.500	-.809	.489			
			.550	-.806	.490	.550	-.814	.488			
			.600	-.699	.518	.600	-.713	.514			
			.650	-.671	.525	.700	-.524	.564			
			.700	-.575	.550	.800	-.249	.636			
			.800	-.305	.621	.900	-.045	.689			
			.900	-.020	.696	.950	-.005	.700			
			.950	.042	.712	.990	.006	.703			
			.990	.056	.716						
					LOWER SURFACE						
.100	-.572	.551	.025	-.092	.677	.025	-.010	.698	.100	-.882	.470
.300	-.649	.531	.050	-.522	.564	.050	-.542	.559	.300	-.651	.531
.600	-.282	.627	.100	-.613	.541	.100	-.664	.527	.600	-.291	.625
.800	.141	.738	.200	-.734	.509	.200	-.761	.502	.800	.101	.728
			.300	-.754	.504	.300	-.867	.474			
			.400	-.699	.518	.400	-.695	.519			
			.500	-.679	.523	.500	-.603	.543			
			.600	-.263	.632	.600	-.267	.631			
			.700	.079	.722	.700	.063	.718			
			.800	.241	.764	.800	.205	.755			
			.900	.341	.791	.900	.271	.772			
			.950	.346	.792	.950	.318	.784			
			1.000	.066	.718						
CN=				.3319			.3206				
CM=				-.1038			-.0945				

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(b) M = 0.73. Continued.

$\alpha = 0.52^{o}$; $C_L = 0.419$.

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.126	.406	0.000	1.118	.994	0.000	.089	.725	.050	-1.209	.385
.150	-1.303	.360	.012	-.126	.668	.012	-.276	.629	.150	-1.376	.341
.300	-1.154	.396	.025	-.615	.540	.025	-.507	.568	.300	-.698	.519
.450	-.590	.547	.050	-1.064	.423	.050	-1.071	.421	.450	-.648	.531
.600	-.536	.548	.100	-1.299	.361	.100	-1.257	.372	.600	-.635	.535
.800	-.372	.604	.150	-1.271	.368	.150	-1.180	.392	.800	-.362	.606
.990	.055	.718	.200	-1.277	.367	.200	-1.202	.386			
			.300	-1.297	.361	.300	-1.228	.379			
			.350	-1.298	.361	.350	-1.283	.365			
			.400	-1.235	.378	.400	-1.231	.379			
			.450	-.725	.511	.450	-.748	.505			
			.500	-.621	.539	.500	-.675	.524			
			.550	-.638	.534	.550	-.714	.514			
			.600	-.620	.539	.600	-.688	.521			
			.650	-.631	.536	.700	-.516	.566			
			.700	-.566	.553	.800	-.281	.628			
			.800	-.326	.616	.900	-.034	.692			
			.900	-.036	.692	.950	-.006	.700			
			.950	.047	.714	.990	.038	.711			
			.990	.076	.721						
					LOWER SURFACE						
.100	-.397	.600	.025	.032	.710	.025	.148	.740	.100	-.712	.515
.300	-.530	.549	.050	-.322	.617	.050	-.419	.591	.300	-.621	.539
.600	-.275	.629	.100	-.545	.559	.100	-.524	.564	.600	-.303	.622
.800	.157	.745	.200	-.606	.542	.200	-.609	.542	.800	.144	.739
			.300	-.656	.529	.300	-.738	.508			
			.400	-.647	.532	.400	-.667	.527			
			.500	-.638	.534	.500	-.574	.551			
			.600	-.243	.637	.600	-.257	.634			
			.700	.096	.726	.700	.067	.719			
			.800	.274	.773	.800	.219	.759			
			.900	.362	.796	.900	.296	.779			
			.950	.365	.797	.950	.337	.789			
			1.000	.098	.727						
CN=				.4788			.4650				
CM=				-.1078			-.0932				

(b) M = 0.73. Continued.

$\alpha = 1.55^{o}$; $C_L = 0.568$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.276	.367	0.000	1.104	.990	0.000	.104	.729	.050	-1.310	.358
.150	-1.421	.329	.012	-.278	.629	.012	-.394	.598	.150	-1.492	.311
.300	-1.235	.352	.025	-.792	.494	.025	-.627	.537	.300	-1.486	.312
.450	-.765	.501	.050	-1.209	.385	.050	-1.160	.398	.450	-.665	.527
.600	-.531	.562	.100	-1.427	.328	.100	-1.357	.346	.600	-.640	.534
.800	-.365	.606	.150	-1.407	.333	.150	-1.352	.347	.800	-.343	.611
.990	.037	.724	.200	-1.411	.332	.200	-1.377	.341			
			.300	-1.433	.326	.300	-1.367	.343			
			.350	-1.406	.333	.350	-1.396	.336			
			.400	-1.407	.333	.400	-1.382	.339			
			.450	-1.383	.339	.450	-1.419	.330			
			.500	-.900	.466	.500	-.926	.459			
			.550	-.714	.514	.550	-.683	.522			
			.600	-.563	.554	.600	-.591	.547			
			.650	-.527	.564	.700	-.468	.579			
			.700	-.438	.571	.800	-.288	.626			
			.800	-.301	.623	.900	-.037	.692			
			.900	-.042	.690	.950	.026	.708			
			.950	.054	.716	.990	.059	.717			
			.990	.106	.729						
					LOWER SURFACE						
.100	-.279	.628	.025	.156	.742	.025	.256	.768	.100	-.589	.547
.300	-.526	.564	.050	-.177	.655	.050	-.262	.633	.300	-.557	.555
.600	-.264	.632	.100	-.378	.603	.100	-.380	.602	.600	-.294	.624
.800	.205	.755	.200	-.492	.573	.200	-.536	.561	.800	.181	.749
			.300	-.591	.547	.300	-.610	.542			
			.400	-.589	.547	.400	-.615	.540			
			.500	-.596	.545	.500	-.530	.563			
			.600	-.221	.644	.600	-.237	.639			
			.700	.112	.731	.700	.094	.726			
			.800	.294	.778	.800	.246	.766			
			.900	.392	.804	.900	.303	.781			
			.950	.385	.802	.950	.349	.793			
			1.000	.118	.732						
CN=				.6150			.6150				
CM=				-.1086			-.0987				

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(b) M = 0.73. Concluded.

$\alpha = 2.36^{\circ}$; $C_L = 0.657$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.324	.355	0.000	1.089	.986	0.000	.092	.725	.050	-1.369	.343
.150	-1.521	.303	.012	-.343	.611	.012	-.522	.564	.150	-1.562	.292
.300	-1.416	.330	.025	-.875	.472	.025	-.689	.521	.300	-1.614	.278
.450	-1.013	.436	.050	-1.286	.364	.050	-1.216	.383	.450	-.680	.523
.600	-.498	.571	.100	-1.487	.312	.100	-1.438	.324	.600	-.622	.538
.800	-.346	.611	.150	-1.468	.317	.150	-1.421	.329	.800	-.302	.622
.990	.085	.723	.200	-1.478	.314	.200	-1.412	.331			
			.300	-1.499	.309	.300	-1.453	.321			
			.350	-1.465	.317	.350	-1.458	.319			
			.400	-1.470	.316	.400	-1.475	.315			
			.450	-1.463	.318	.450	-1.497	.309			
			.500	-.940	.455	.500	-1.219	.382			
			.550	-.824	.485	.550	-.784	.496			
			.600	-.705	.516	.600	-.676	.524			
			.650	-.581	.549	.700	-.453	.583			
			.700	-.433	.588	.800	-.289	.626			
			.800	-.224	.642	.900	-.059	.686			
			.900	-.050	.688	.950	.028	.709			
			.950	.034	.710	.950	.078	.722			
			.950	.040	.712						
					LOWER SURFACE						
.100	-.225	.642	.025	.211	.756	.025	.346	.792	.100	-.509	.568
.300	-.480	.576	.050	-.071	.683	.050	-.144	.663	.300	-.539	.560
.600	-.259	.633	.100	-.277	.629	.100	-.321	.617	.600	-.295	.624
.800	.230	.762	.200	-.420	.591	.200	-.435	.587	.800	.186	.750
			.300	-.519	.565	.300	-.559	.555			
			.400	-.541	.559	.400	-.574	.551			
			.500	-.566	.553	.500	-.518	.565			
			.600	-.222	.643	.600	-.242	.638			
			.700	.118	.732	.700	.095	.726			
			.800	.301	.780	.800	.258	.769			
			.900	.394	.805	.900	.313	.783			
			.950	.375	.799	.950	.359	.795			
			1.000	.067	.719						
CN=				.6884			.7096				
CM=				-.1080			-.1057				

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(c) M = 0.75

$\alpha = -4.70^{\circ}$; $C_L = -0.237$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.238	.625	0.000	1.109	.989	0.000	.090	.713	.050	-.316	.603
.150	-.533	.545	.012	.478	.819	.012	.418	.802	.150	-.462	.564
.300	-.555	.538	.025	.119	.721	.025	.105	.717	.300	-.598	.527
.450	-.452	.564	.050	-.272	.615	.050	-.249	.621	.450	-.586	.530
.600	-.567	.535	.100	-.387	.584	.100	-.362	.591	.600	-.656	.511
.800	-.373	.588	.150	-.467	.562	.150	-.381	.586	.800	-.344	.596
.990	.060	.705	.200	-.556	.538	.200	-.495	.555			
			.300	-.594	.528	.300	-.604	.525			
			.350	-.584	.531	.350	-.591	.529			
			.400	-.578	.532	.400	-.584	.531			
			.450	-.568	.535	.450	-.650	.513			
			.500	-.735	.490	.500	-.724	.493			
			.550	-.758	.484	.550	-.827	.465			
			.600	-.627	.519	.600	-.747	.487			
			.650	-.696	.500	.700	-.542	.542			
			.700	-.593	.528	.800	-.243	.623			
			.800	-.325	.601	.900	-.025	.682			
			.900	-.009	.686	.950	.018	.694			
			.950	.063	.706	.990	.035	.698			
			.990	.097	.715						
					LOWER SURFACE						
.100	-1.080	.396	.025	-.501	.553	.025	-.415	.577	.100	-1.397	.311
.300	-1.311	.334	.050	-1.097	.392	.050	-1.009	.416	.300	-1.448	.297
.600	-.278	.614	.100	-1.248	.351	.100	-1.278	.343	.600	-.265	.617
.800	.046	.701	.200	-1.294	.338	.200	-1.315	.333	.800	.040	.700
			.300	-1.239	.353	.300	-1.208	.362			
			.400	-.761	.483	.400	-.719	.494			
			.500	-.628	.519	.500	-.665	.509			
			.600	-.381	.586	.600	-.442	.569			
			.700	-.195	.636	.700	-.336	.598			
			.800	.058	.705	.800	-.053	.675			
			.900	.213	.747	.900	.037	.699			
			.950	.175	.736	.950	.182	.738			
			1.000	.108	.718						
CN=				-.1656			-.1821				
CM=				-.0927			-.0671				

(c) M = 0.75. Continued.

$\alpha = -0.29^{\circ}$; $C_L = 0.316$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-.930	.437	0.000	1.130	.995	0.000	.090	.713	.050	-1.056	.403
.150	-1.148	.378	.012	.009	.692	.012	-.096	.663	.150	-1.236	.354
.300	-1.040	.407	.025	-.453	.566	.025	-.344	.596	.300	-.780	.478
.450	-.653	.512	.050	-.880	.451	.050	-.877	.452	.450	-.689	.503
.600	-.570	.535	.100	-1.146	.379	.100	-1.086	.395	.600	-.664	.509
.800	-.355	.593	.150	-1.071	.399	.150	-1.032	.410	.800	-.323	.601
.990	.070	.708	.200	-1.121	.385	.200	-1.054	.403			
			.300	-1.164	.374	.300	-1.059	.402			
			.350	-1.127	.384	.350	-1.143	.380			
			.400	-1.068	.400	.400	-1.135	.382			
			.450	-1.028	.411	.450	-1.148	.378			
			.500	-1.182	.369	.500	-.982	.423			
			.550	-.640	.516	.550	-.798	.473			
			.600	-.566	.536	.600	-.657	.511			
			.650	-.586	.530	.700	-.488	.557			
			.700	-.536	.544	.800	-.238	.625			
			.800	-.288	.611	.900	-.032	.680			
			.900	-.020	.684	.950	.000	.689			
			.950	.045	.701	.990	.015	.693			
			.990	.084	.712						
					LOWER SURFACE						
.100	-.549	.540	.025	-.045	.677	.025	.063	.706	.100	-.931	.437
.300	-.703	.499	.050	-.435	.571	.050	-.544	.542	.300	-.666	.509
.600	-.256	.620	.100	-.675	.506	.100	-.659	.511	.600	-.294	.609
.800	.122	.722	.200	-.761	.483	.200	-.734	.490	.800	.094	.714
			.300	-.754	.485	.300	-.902	.445			
			.400	-.779	.478	.400	-.687	.503			
			.500	-.692	.502	.500	-.606	.525			
			.600	-.257	.619	.600	-.249	.622			
			.700	.079	.710	.700	.063	.706			
			.800	.233	.752	.800	.208	.745			
			.900	.364	.788	.900	.270	.762			
			.950	.354	.785	.950	.317	.775			
			1.000	.102	.717						
CN=				.3660			.3750				
CM=				-.1111			-.1012				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Continued

(c) M = 0.75. Continued.

$\alpha = 0.68^{\circ}$; $C_L = 0.452$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.038	.408	0.000	1.121	.993	0.000	.102	.717	.050	-1.137	.381
.150	-1.257	.349	.012	-.111	.659	.012	-.220	.630	.150	-1.319	.332
.300	-1.198	.365	.025	-.566	.536	.025	-.468	.562	.300	-1.392	.312
.450	-1.062	.401	.050	-1.010	.416	.050	-.948	.432	.450	-.694	.501
.600	-.521	.548	.100	-1.251	.350	.100	-1.178	.370	.600	-.650	.513
.800	-.346	.595	.150	-1.222	.358	.150	-1.138	.381	.800	-.328	.600
.990	.088	.713	.200	-1.259	.348	.200	-1.158	.375			
			.300	-1.261	.348	.300	-1.218	.359			
			.350	-1.242	.353	.350	-1.232	.355			
			.400	-1.252	.350	.400	-1.222	.358			
			.450	-1.224	.358	.450	-1.307	.335			
			.500	-1.306	.335	.500	-1.307	.335			
			.550	-.971	.426	.550	-.895	.447			
			.600	-.645	.514	.600	-.619	.521			
			.650	-.508	.552	.700	-.451	.567			
			.700	-.457	.565	.800	-.257	.620			
			.800	-.265	.617	.900	-.033	.680			
			.900	-.023	.683	.950	.021	.695			
			.950	.054	.704	.990	.027	.696			
			.990	.095	.715						
					LOWER SURFACE						
.100	-.408	.578	.025	.047	.702	.025	.177	.737	.100	-.766	.482
.300	-.603	.526	.050	-.296	.609	.050	-.407	.579	.300	-.669	.508
.600	-.268	.617	.100	-.479	.559	.100	-.535	.544	.600	-.301	.608
.800	.135	.726	.200	-.618	.522	.200	-.619	.521	.800	.141	.727
			.300	-.693	.501	.300	-.832	.464			
			.400	-.679	.505	.400	-.682	.504			
			.500	-.677	.506	.500	-.592	.529			
			.600	-.235	.625	.600	-.254	.620			
			.700	.099	.716	.700	.070	.708			
			.800	.264	.761	.800	.231	.752			
			.900	.374	.790	.900	.284	.766			
			.550	.362	.787	.950	.344	.782			
			1.000	.103	.717						
CN=				.5146			.4893				
CM=				-.1145			-.1051				

(c) M = 0.75. Continued.

$\alpha = 1.39^{\circ}$; $C_L = 0.521$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.121	.386	0.000	1.115	.991	0.000	.100	.716	.050	-1.194	.366
.150	-1.322	.331	.012	-.173	.642	.012	-.322	.602	.150	-1.366	.319
.300	-1.271	.345	.025	-.675	.506	.025	-.513	.550	.300	-1.447	.297
.450	-1.154	.376	.050	-1.077	.397	.050	-1.046	.406	.450	-.762	.483
.600	-.492	.556	.100	-1.321	.331	.100	-1.258	.348	.600	-.614	.523
.800	-.330	.600	.150	-1.283	.342	.150	-1.225	.357	.800	-.310	.605
.990	.087	.713	.200	-1.322	.331	.200	-1.219	.359			
			.300	-1.331	.329	.300	-1.285	.341			
			.350	-1.331	.328	.350	-1.286	.341			
			.400	-1.313	.333	.400	-1.299	.337			
			.450	-1.295	.338	.450	-1.356	.322			
			.500	-1.035	.409	.500	-1.389	.313			
			.550	-.769	.481	.550	-.932	.437			
			.600	-.683	.504	.600	-.673	.507			
			.650	-.562	.537	.700	-.461	.564			
			.700	-.432	.572	.800	-.279	.613			
			.800	-.220	.629	.900	-.056	.674			
			.900	-.112	.659	.950	.020	.694			
			.950	-.017	.684	.990	.059	.705			
			.990	.054	.704						
					LOWER SURFACE						
.100	-.340	.597	.025	.109	.719	.025	.238	.754	.100	-.664	.509
.300	-.565	.536	.050	-.253	.620	.050	-.303	.607	.300	-.640	.516
.600	-.210	.632	.100	-.401	.580	.100	-.442	.569	.600	-.300	.608
.800	.171	.735	.200	-.549	.540	.200	-.566	.536	.800	.150	.730
			.300	-.653	.512	.300	-.712	.496			
			.400	-.659	.511	.400	-.673	.507			
			.500	-.674	.507	.500	-.586	.530			
			.600	-.248	.622	.600	-.245	.623			
			.700	.075	.709	.700	.075	.709			
			.800	.266	.761	.800	.226	.750			
			.900	.382	.793	.900	.296	.769			
			.950	.373	.790	.950	.353	.785			
			1.000	-.016	.685						
CN=				.5422			.5706				
CM=				-.1078			-.1083				

[redacted]

TABLE VII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON SEALED - Concluded

(c) M = 0.75. Concluded.

$\alpha = 2.01^{\circ}$; $C_L = 0.553$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.171	.372	0.000	1.103	.988	0.000	.100	.716	.050	-1.239	.354
.150	-1.367	.319	.012	-.241	.624	.012	-.344	.596	.150	-1.434	.301
.300	-1.313	.334	.025	-.719	.494	.025	-.551	.540	.300	-1.507	.281
.450	-1.034	.409	.050	-1.131	.383	.050	-1.086	.395	.450	-.745	.487
.600	-.456	.563	.100	-1.372	.318	.100	-1.290	.340	.600	-.582	.532
.800	-.312	.605	.150	-1.337	.327	.150	-1.302	.337	.800	-.292	.610
.990	.006	.691	.200	-1.376	.317	.200	-1.279	.343			
			.300	-1.381	.315	.300	-1.340	.326			
			.350	-1.374	.317	.350	-1.347	.325			
			.400	-1.276	.344	.400	-1.357	.322			
			.450	-.959	.429	.450	-1.422	.304			
			.500	-.780	.478	.500	-1.259	.348			
			.550	-.703	.499	.550	-.781	.478			
			.600	-.638	.516	.600	-.685	.504			
			.650	-.533	.545	.700	-.463	.564			
			.700	-.425	.574	.800	-.300	.608			
			.800	-.265	.617	.900	-.080	.667			
			.900	-.169	.643	.950	-.009	.687			
			.550	-.078	.668	.990	.065	.707			
			.990	-.166	.644						
					LOWER SURFACE						
.100	-.260	.619	.025	.167	.734	.025	.299	.770	.100	-.599	.527
.300	-.545	.542	.050	-.164	.645	.050	-.224	.628	.300	-.596	.528
.600	-.333	.607	.100	-.351	.594	.100	-.394	.582	.600	-.300	.608
.800	.164	.734	.200	-.491	.556	.200	-.508	.552	.800	.172	.736
			.300	-.593	.529	.300	-.669	.508			
			.400	-.639	.516	.400	-.652	.513			
			.500	-.679	.505	.500	-.607	.525			
			.600	-.258	.619	.600	-.245	.623			
			.700	.083	.712	.700	.080	.711			
			.800	.274	.763	.800	.233	.752			
			.900	.371	.790	.900	.301	.771			
			.550	.322	.776	.950	.353	.785			
			1.000	-.070	.670						
CN=				.5668			.6090				
CM=				-.1070			-.1070				

TABLE VIII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED; HIGH ANGLE-OF-ATTACK RANGE

(a) M = 0.30

$\alpha = 2.40^{\circ}$; $C_L = 0.518$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-1.584	.845	0.000	.831	.989	0.000	.066	.943	.050	-1.553	.847
.150	-.936	.884	.012	-1.278	.864	.012	-1.260	.865	.150	-.688	.899
.300	-.715	.907	.025	-1.606	.844	.025	-1.309	.862	.300	-.666	.900
.450	-.547	.907	.050	-1.485	.851	.050	-1.425	.855	.450	-.556	.906
.600	-.531	.908	.100	-1.121	.873	.100	-1.069	.876	.600	-.510	.909
.800	-.398	.916	.150	-.948	.883	.150	-.866	.888	.800	-.349	.919
.990	.029	.941	.200	-.883	.887	.200	-.807	.892			
			.300	-.754	.895	.300	-.742	.895			
			.350	-.711	.897	.350	-.685	.899			
			.400	-.668	.900	.400	-.637	.902			
			.450	-.625	.902	.450	-.634	.902			
			.500	-.649	.901	.500	-.630	.902			
			.550	-.645	.901	.550	-.602	.904			
			.600	-.578	.905	.600	-.579	.905			
			.650	-.595	.904	.700	-.472	.911			
			.700	-.548	.907	.800	-.322	.920			
			.800	-.379	.917	.900	-.093	.934			
			.900	-.108	.933	.950	-.036	.937			
			.950	-.003	.939	.990	-.030	.938			
			.990	.052	.943						
					LOWER SURFACE						
.100	-.099	.934	.025	.294	.957	.025	.399	.963	.100	-.262	.924
.300	-.299	.922	.050	.042	.942	.050	-.053	.936	.300	-.322	.920
.600	-.236	.925	.100	-.123	.932	.100	-.148	.931	.600	-.217	.927
.800	.246	.954	.200	-.212	.927	.200	-.235	.926	.800	.232	.953
			.300	-.298	.922	.300	-.284	.923			
			.400	-.318	.921	.400	-.310	.921			
			.500	-.332	.920	.500	-.301	.922			
			.600	-.147	.931	.600	-.172	.929			
			.700	.089	.945	.700	.067	.943			
			.800	.286	.956	.800	.301	.957			
			.900	.364	.961	.900	.303	.957			
			.950	.344	.960	.950	.342	.960			
			1.000	.074	.944						
CN=				.5902			.5645				
CM=				-.1015			-.0905				

(a) M = 0.30. Continued.

$\alpha = 8.81^{\circ}$; $C_L = 1.053$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.551	.788	0.000	-.237	.925	0.000	.078	.944	.050	-3.106	.755
.150	-1.467	.853	.012	-3.747	.717	.012	-3.867	.710	.150	-1.191	.869
.300	-.966	.882	.025	-3.783	.715	.025	-3.341	.742	.300	-.895	.886
.450	-.687	.899	.050	-3.031	.760	.050	-2.818	.773	.450	-.661	.900
.600	-.570	.906	.100	-1.939	.825	.100	-1.827	.831	.600	-.570	.906
.800	-.314	.921	.150	-1.572	.846	.150	-1.433	.855	.800	-.378	.917
.990	-.023	.938	.200	-1.339	.860	.200	-1.286	.863			
			.300	-1.060	.877	.300	-1.027	.879			
			.350	-.952	.883	.350	-.921	.885			
			.400	-.872	.888	.400	-.837	.890			
			.450	-.786	.893	.450	-.787	.893			
			.500	-.775	.894	.500	-.758	.895			
			.550	-.739	.896	.550	-.683	.899			
			.600	-.646	.901	.600	-.623	.902			
			.650	-.609	.903	.700	-.431	.914			
			.700	-.527	.908	.800	-.239	.925			
			.800	-.306	.921	.900	-.136	.931			
			.900	-.078	.935	.950	-.127	.932			
			.950	-.048	.937	.990	-.137	.931			
			.990	-.038	.937						
					LOWER SURFACE						
.100	.411	.964	.025	.871	.991	.025	.957	.996	.100	.300	.957
.300	-.028	.938	.050	.671	.979	.050	.625	.976	.300	-.077	.935
.600	-.192	.933	.100	.391	.963	.100	.360	.961	.600	-.141	.931
.800	.298	.957	.200	.144	.948	.200	.143	.948	.800	.254	.954
			.300	.028	.941	.300	.001	.939			
			.400	-.086	.934	.400	-.092	.934			
			.500	-.161	.930	.500	-.127	.932			
			.600	-.041	.937	.600	-.068	.935			
			.700	.155	.949	.700	.127	.947			
			.800	.323	.959	.800	.314	.958			
			.900	.385	.962	.900	.322	.958			
			.950	.323	.959	.950	.323	.959			
			1.000	-.020	.938						
CN=				1.1097			1.0746				
CM=				-.0703			-.0572				

TABLE VIII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED; HIGH ANGLE-OF-ATTACK RANGE - Continued

(a) M = 0.30. Continued.

$\alpha = 10.90^{\circ}$; $C_L = 1.220$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.739	.774	0.000	-.816	.891	0.000	.071	.944	.050	-3.707	.720
.150	-1.615	.844	.012	-4.663	.663	.012	-4.753	.658	.150	-1.335	.860
.300	-1.033	.878	.025	-4.565	.669	.025	-4.021	.701	.300	-.936	.884
.450	-.712	.897	.050	-3.399	.738	.050	-3.297	.744	.450	-.711	.897
.600	-.571	.906	.100	-2.207	.808	.100	-2.139	.813	.600	-.604	.904
.800	-.355	.924	.150	-1.751	.836	.150	-1.622	.843	.800	-.395	.916
.990	-.053	.936	.200	-1.478	.852	.200	-1.427	.855			
			.300	-1.139	.872	.300	-1.103	.874			
			.350	-1.013	.879	.350	-.988	.881			
			.400	-.928	.884	.400	-.895	.886			
			.450	-.821	.891	.450	-.827	.890			
			.500	-.814	.891	.500	-.775	.893			
			.550	-.747	.895	.550	-.692	.898			
			.600	-.649	.901	.600	-.615	.903			
			.650	-.594	.904	.700	-.404	.915			
			.700	-.494	.910	.800	-.242	.925			
			.800	-.272	.923	.900	-.167	.929			
			.900	-.106	.933	.950	-.166	.930			
			.950	-.083	.934	.990	-.168	.929			
			.990	-.082	.934						
					LOWER SURFACE						
.100	.549	.972	.025	.936	.995	.025	.996	.998	.100	.433	.965
.300	.055	.943	.050	.798	.987	.050	.764	.985	.300	.006	.940
.600	-.038	.934	.100	.542	.971	.100	.491	.968	.600	-.110	.933
.800	.310	.958	.200	.271	.955	.200	.229	.953	.800	.254	.954
			.300	.110	.946	.300	.085	.944			
			.400	-.013	.939	.400	-.017	.938			
			.500	-.101	.933	.500	-.069	.935			
			.600	-.002	.939	.600	-.025	.938			
			.700	.176	.950	.700	.144	.948			
			.800	.334	.959	.800	.316	.958			
			.900	.399	.963	.900	.314	.958			
			.950	.327	.959	.950	.323	.959			
			1.000	-.074	.935						
CN=				1.2681			1.2279				
CM=				-.0617			-.0491				

(a) M = 0.30. Continued.

$\alpha = 13.03^{\circ}$; $C_L = 1.376$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.281	.745	0.000	-1.427	.855	0.000	.078	.944	.050	-4.364	.681
.150	-1.762	.835	.012	-5.654	.604	.012	-5.864	.592	.150	-1.446	.854
.300	-1.094	.875	.025	-5.493	.614	.025	-4.997	.643	.300	-.975	.882
.450	-.722	.897	.050	-3.841	.712	.050	-3.721	.719	.450	-.802	.892
.600	-.543	.907	.100	-2.449	.794	.100	-2.364	.799	.600	-.624	.902
.800	-.201	.927	.150	-1.911	.826	.150	-1.780	.834	.800	-.410	.915
.990	-.100	.933	.200	-1.613	.844	.200	-1.541	.848			
			.300	-1.199	.868	.300	-1.164	.870			
			.350	-1.064	.876	.350	-1.031	.878			
			.400	-.961	.882	.400	-.925	.885			
			.450	-.841	.890	.450	-.849	.889			
			.500	-.805	.892	.500	-.782	.893			
			.550	-.733	.896	.550	-.708	.897			
			.600	-.630	.902	.600	-.603	.904			
			.650	-.549	.907	.700	-.379	.917			
			.700	-.456	.912	.800	-.253	.924			
			.800	-.222	.926	.900	-.208	.927			
			.900	-.136	.931	.950	-.228	.926			
			.950	-.126	.932	.990	-.192	.928			
			.990	-.118	.932						
					LOWER SURFACE						
.100	.634	.977	.025	.970	.997	.025	.985	.998	.100	.546	.972
.300	.128	.947	.050	.903	.993	.050	.872	.991	.300	.083	.944
.600	-.048	.937	.100	.640	.977	.100	.632	.977	.600	-.079	.935
.800	.315	.958	.200	.366	.961	.200	.353	.960	.800	.261	.955
			.300	.197	.951	.300	.161	.949			
			.400	.056	.943	.400	.049	.942			
			.500	-.040	.937	.500	-.021	.938			
			.600	.030	.941	.600	.006	.940			
			.700	.193	.951	.700	.159	.949			
			.800	.345	.960	.800	.325	.959			
			.900	.383	.962	.900	.328	.959			
			.950	.323	.959	.950	.315	.958			
			1.000	-.074	.935						
CN=				1.4034			1.3761				
CM=				-.0475			-.0402				

TABLE VIII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED; HIGH ANGLE-OF-ATTACK RANGE - Continued

(a) M = 0.30. Continued.

$\alpha = 14.12^{\circ}$; $C_L = 1.448$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.487	.733	C.CCO	-1.802	.833	C.000	.083	.944	.050	-4.744	.658
.150	-1.802	.833	.012	-6.341	.563	.012	-6.459	.557	.150	-1.494	.851
.300	-1.105	.874	.025	-6.026	.582	.025	-5.418	.618	.300	-1.043	.878
.450	-.715	.897	.050	-4.134	.694	.050	-3.960	.705	.450	-.805	.892
.600	-.503	.910	.100	-2.601	.785	.100	-2.481	.792	.600	-.663	.900
.800	-.181	.929	.150	-1.986	.822	.150	-1.874	.828	.800	-.420	.914
.990	-.121	.932	.200	-1.676	.840	.200	-1.579	.846			
			.300	-1.236	.866	.300	-1.190	.869			
			.350	-1.079	.875	.350	-1.051	.877			
			.400	-.963	.882	.400	-.925	.885			
			.450	-.847	.889	.450	-.850	.889			
			.500	-.791	.892	.500	-.763	.894			
			.550	-.711	.897	.550	-.676	.899			
			.600	-.594	.904	.600	-.554	.907			
			.650	-.503	.910	.700	-.380	.917			
			.700	-.394	.916	.800	-.255	.924			
			.800	-.215	.927	.900	-.214	.927			
			.900	-.151	.930	.950	-.232	.926			
			.550	-.148	.931	.990	-.214	.927			
			.990	-.151	.930						
					LOWER SURFACE						
.100	.700	.981	.025	.965	.997	.025	.972	.997	.100	.620	.976
.300	.169	.949	.050	.939	.995	.050	.926	.994	.300	.114	.946
.600	-.039	.937	.100	.702	.981	.100	.683	.980	.600	-.063	.936
.800	.320	.958	.200	.407	.964	.200	.388	.962	.800	.268	.955
			.300	.242	.954	.300	.212	.952			
			.400	.095	.945	.400	.086	.944			
			.500	-.017	.938	.500	.003	.940			
			.600	.045	.942	.600	.029	.941			
			.700	.201	.951	.700	.168	.949			
			.800	.356	.960	.800	.336	.959			
			.900	.387	.962	.900	.328	.959			
			.950	.312	.958	.950	.322	.958			
			1.000	-.124	.932						
CN=				1.4752			1.4412				
CM=				-.0367			-.0348				

(a) M = 0.30. Continued.

$\alpha = 14.92^{\circ}$; $C_L = 1.293$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.328	.742	C.CCO	-1.839	.830	C.000	-.083	.934	.050	-4.856	.652
.150	-1.734	.837	.012	-6.287	.567	.012	-6.698	.542	.150	-1.476	.852
.300	-1.035	.878	.025	-5.928	.588	.025	-5.556	.610	.300	-1.116	.873
.450	-.707	.897	.050	-4.084	.697	.050	-4.053	.699	.450	-.833	.890
.600	-.556	.906	.100	-2.596	.786	.100	-2.491	.792	.600	-.676	.899
.800	-.247	.925	.150	-1.951	.824	.150	-1.878	.828	.800	-.420	.914
.990	-.129	.932	.200	-1.652	.841	.200	-1.590	.845			
			.300	-1.212	.868	.300	-1.183	.869			
			.350	-1.064	.876	.350	-1.052	.877			
			.400	-.945	.883	.400	-.926	.884			
			.450	-.853	.889	.450	-.833	.890			
			.500	-.790	.893	.500	-.755	.895			
			.550	-.701	.898	.550	-.661	.900			
			.600	-.587	.905	.600	-.562	.906			
			.650	-.520	.909	.700	-.351	.919			
			.700	-.411	.915	.800	-.257	.924			
			.800	-.226	.926	.900	-.206	.927			
			.900	-.157	.930	.950	-.248	.925			
			.950	-.141	.931	.990	-.220	.926			
			.990	-.149	.931						
					LOWER SURFACE						
.100	.701	.981	.025	.958	.996	.025	.970	.997	.100	.644	.978
.300	.155	.949	.050	.937	.995	.050	.925	.994	.300	.122	.947
.600	-.048	.937	.100	.712	.982	.100	.691	.980	.600	-.044	.937
.800	.308	.958	.200	.417	.964	.200	.418	.964	.800	.275	.956
			.300	.246	.954	.300	.235	.953			
			.400	.099	.945	.400	.089	.945			
			.500	-.007	.939	.500	.014	.940			
			.600	.056	.943	.600	.032	.941			
			.700	.202	.951	.700	.178	.950			
			.800	.359	.961	.800	.338	.959			
			.900	.387	.962	.900	.321	.958			
			.950	.315	.958	.950	.327	.959			
			1.000	-.135	.931						
CN=				1.4717			1.4587				
CM=				-.0399			-.0324				

TABLE VIII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED; HIGH ANGLE-OF-ATTACK RANGE - Continued

(a) M = 0.30. Continued.

$\alpha = 15.94^{o}$; $C_L = 1.279$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.338	.743	0.000	-2.052	.817	C.000	-.163	.930	.050	-5.024	.641
.150	-1.736	.836	.012	-6.680	.543	.C12	-7.134	.516	.150	-1.512	.850
.300	-1.018	.878	.025	-6.254	.568	.C25	-5.975	.585	.300	-1.076	.875
.450	-.735	.896	.050	-4.206	.690	.050	-4.203	.690	.450	-.892	.886
.600	-.576	.905	.100	-2.625	.783	.100	-2.589	.786	.600	-.650	.901
.800	-.327	.920	.150	-2.028	.819	.150	-1.927	.825	.800	-.484	.911
.990	-.138	.932	.200	-1.661	.841	.200	-1.614	.844			
			.300	-1.233	.866	.300	-1.180	.869			
			.350	-1.072	.876	.350	-1.045	.877			
			.400	-.953	.883	.400	-.920	.885			
			.450	-.836	.890	.450	-.813	.891			
			.500	-.778	.893	.500	-.732	.896			
			.550	-.683	.899	.550	-.584	.905			
			.600	-.580	.905	.600	-.538	.907			
			.650	-.506	.909	.700	-.368	.917			
			.700	-.367	.918	.800	-.295	.922			
			.800	-.206	.927	.900	-.303	.921			
			.900	-.179	.929	.950	-.282	.923			
			.950	-.160	.930	.990	-.249	.925			
			.990	-.163	.930						
					LOWER SURFACE						
.100	.736	.983	.025	.955	.996	.C25	.923	.994	.100	.673	.979
.300	.137	.950	.050	.971	.997	.050	.936	.995	.300	.157	.949
.600	-.061	.937	.100	.743	.983	.100	.734	.983	.600	-.062	.936
.800	.301	.957	.200	.461	.967	.200	.433	.965	.800	.261	.955
			.300	.277	.956	.300	.265	.955			
			.400	.114	.946	.400	.109	.946			
			.500	.007	.940	.500	.008	.940			
			.600	.065	.943	.600	.035	.941			
			.700	.223	.953	.700	.178	.950			
			.800	.346	.960	.800	.337	.959			
			.900	.400	.963	.900	.314	.958			
			.950	.310	.958	.950	.326	.959			
			1.000	-.155	.930						
CN=				1.5101			1.5035				
CM=				-.0345			-.0334				

(a) M = 0.30. Continued.

$\alpha = 16.94^{o}$; $C_L = 1.318$

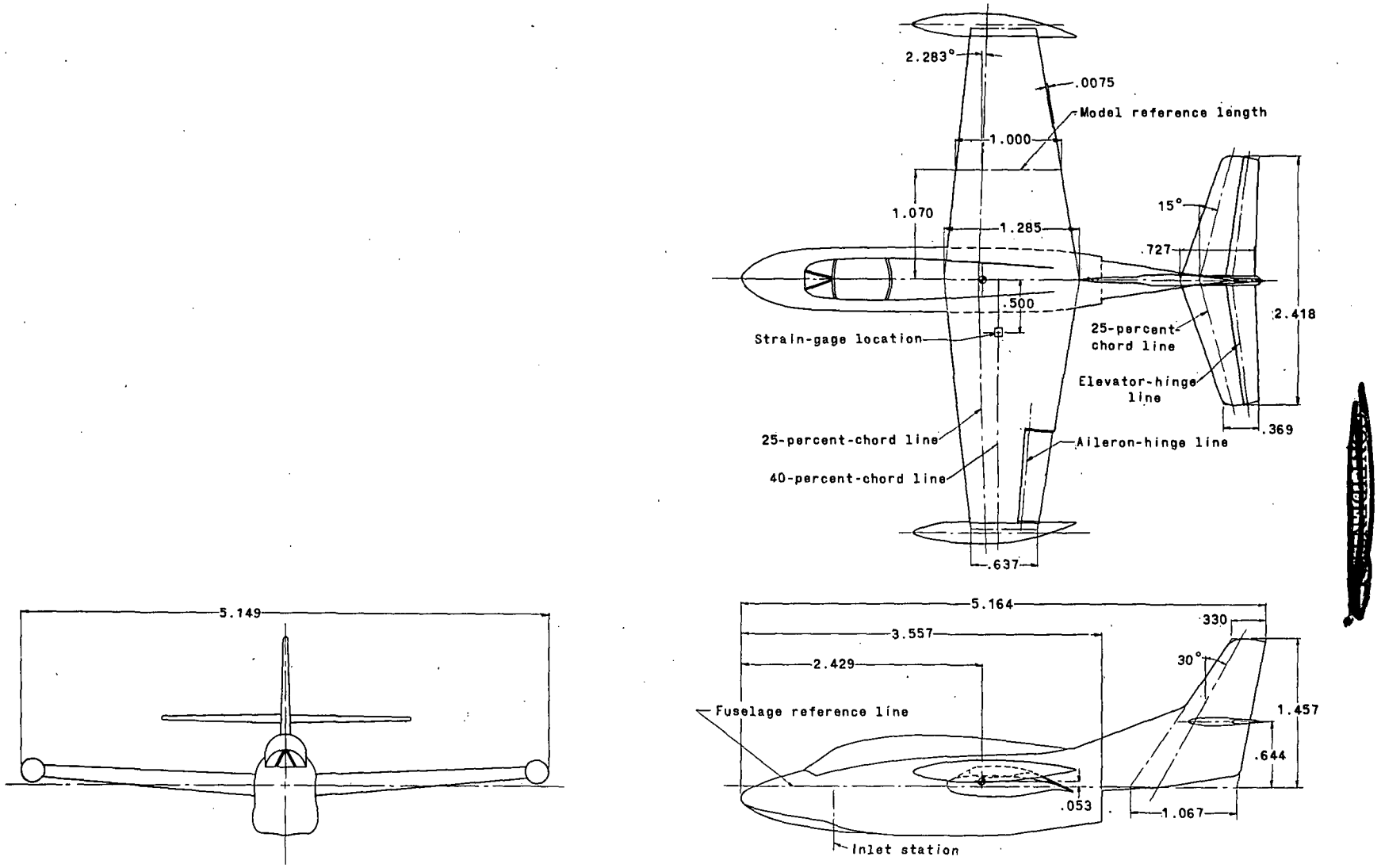
STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-3.513	.731	0.000	-2.272	.805	C.000	-.181	.929	.050	-5.278	.627
.150	-1.758	.835	.012	-6.937	.528	.C12	-7.428	.499	.150	-1.498	.851
.300	-1.055	.877	.025	-6.597	.548	.C25	-6.246	.569	.300	-1.120	.873
.450	-.677	.899	.050	-4.321	.683	.050	-4.318	.684	.450	-.836	.890
.600	-.554	.907	.100	-2.663	.782	.100	-2.616	.784	.600	-.657	.900
.800	-.216	.927	.150	-2.024	.819	.150	-1.954	.824	.800	-.475	.911
.990	-.138	.928	.200	-1.654	.841	.200	-1.617	.844			
			.300	-1.210	.868	.300	-1.182	.869			
			.350	-1.037	.878	.350	-.992	.881			
			.400	-.894	.886	.400	-.898	.886			
			.450	-.748	.895	.450	-.753	.895			
			.500	-.734	.896	.500	-.685	.899			
			.550	-.624	.902	.550	-.584	.905			
			.600	-.483	.911	.600	-.466	.912			
			.650	-.413	.915	.700	-.376	.917			
			.700	-.330	.920	.800	-.342	.919			
			.800	-.255	.924	.900	-.335	.920			
			.900	-.225	.926	.950	-.324	.920			
			.950	-.240	.925	.990	-.276	.923			
			.990	-.175	.929						
					LOWER SURFACE						
.100	.758	.984	.025	.934	.995	.C25	.899	.993	.100	.699	.981
.300	.226	.953	.050	.981	.998	.050	.970	.997	.300	.188	.951
.600	-.023	.939	.100	.784	.986	.100	.767	.985	.600	-.032	.937
.800	.267	.957	.200	.483	.968	.200	.481	.968	.800	.260	.955
			.300	.295	.957	.300	.283	.956			
			.400	.142	.948	.400	.136	.947			
			.500	.017	.940	.500	.044	.942			
			.600	.064	.943	.600	.052	.943			
			.700	.204	.951	.700	.188	.951			
			.800	.338	.959	.800	.339	.960			
			.900	.376	.962	.900	.298	.957			
			.950	.284	.956	.950	.318	.958			
			1.000	-.216	.927						
CN=				1.5220			1.5357				
CM=				-.0273			-.0340				

TABLE VIII.- PRESSURE COEFFICIENTS FOR CONFIGURATION 2; HORIZONTAL TAIL ON; WAKE RAKE OFF; AILERON UNSEALED; HIGH ANGLE-OF-ATTACK RANGE - Concluded

(a) M = 0.30. Concluded.

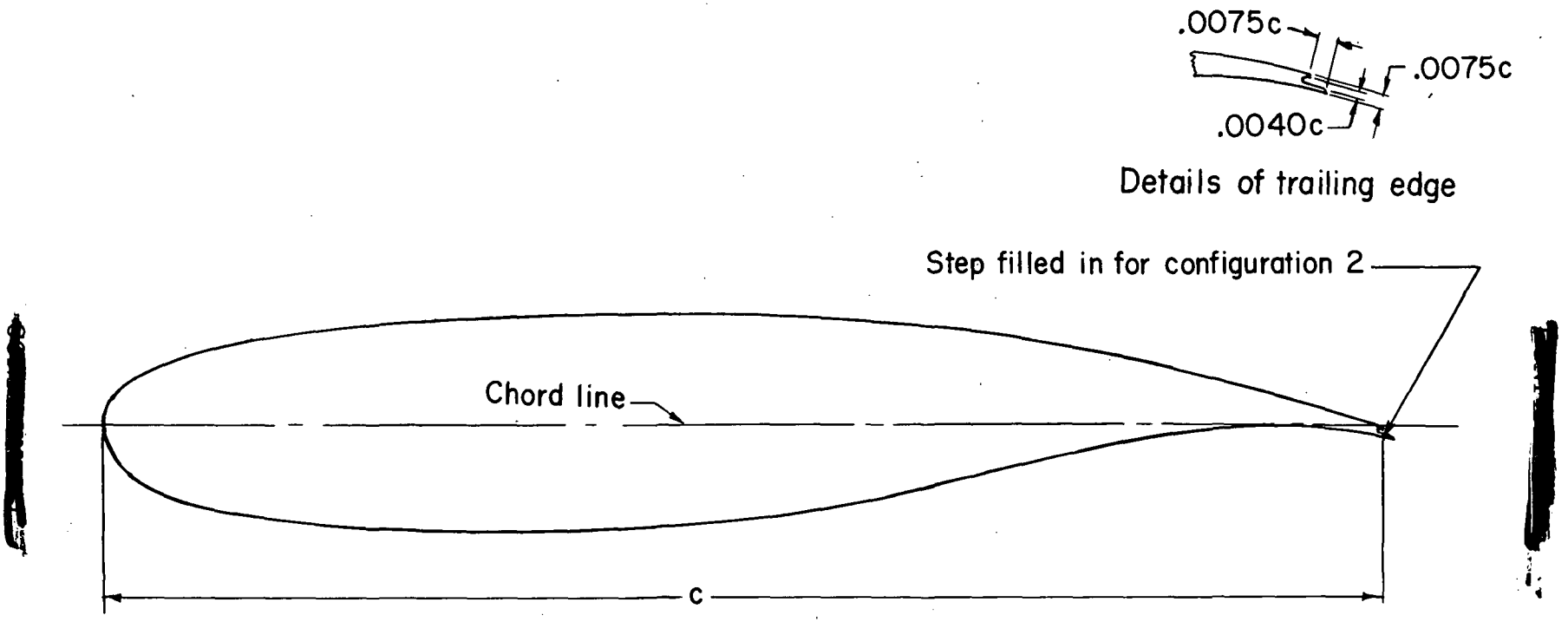
$\alpha = 18.77^{\circ}$; $C_L = 1.085$

STATION .1592			STATION .4245			STATION .7325			STATION .9025		
X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF	X/C	CP	P/PTINF
					UPPER SURFACE						
.050	-2.718	.767	0.000	-.539	.908	C.000	-.132	.932	.050	-3.899	.709
.150	-1.031	.878	.012	-2.091	.816	.012	-.666	.900	.150	-1.121	.873
.300	-.715	.897	.025	-1.498	.851	.025	-.510	.909	.300	-.695	.898
.450	-.455	.913	.050	-.687	.899	.050	-.614	.903	.450	-.473	.911
.600	-.539	.906	.100	-.527	.908	.100	-.486	.911	.600	-.565	.906
.800	-.739	.896	.150	-.793	.893	.150	-.583	.905	.800	-.624	.903
.990	-.839	.890	.200	-.513	.909	.200	-.623	.903			
			.300	-.643	.901	.300	-.653	.901			
			.350	-.686	.899	.350	-.691	.899			
			.400	-1.010	.880	.400	-.666	.900			
			.450	-.597	.904	.450	-.728	.896			
			.500	-.633	.902	.500	-.668	.900			
			.550	-.673	.900	.550	-.670	.900			
			.600	-.851	.889	.600	-.716	.897			
			.650	-.798	.892	.700	-.761	.894			
			.700	-.661	.900	.800	-.722	.897			
			.800	-.560	.906	.900	-.785	.893			
			.900	-.489	.911	.950	-.720	.897			
			.950	-.488	.911	.990	-.662	.900			
			.980	-.787	.893						
					LOWER SURFACE						
.100	.709	.981	.025	.953	.996	.025	.975	.997	.100	.575	.974
.300	.133	.947	.050	.855	.990	.050	.808	.987	.300	.057	.943
.600	-.197	.929	.100	.616	.976	.100	.579	.974	.600	-.169	.929
.800	.246	.954	.200	.347	.960	.200	.303	.957	.800	.191	.951
			.300	.156	.949	.300	.140	.948			
			.400	-.004	.939	.400	-.008	.939			
			.500	-.134	.932	.500	-.128	.932			
			.600	-.100	.934	.600	-.119	.932			
			.700	.049	.942	.700	-.015	.939			
			.800	.222	.953	.800	.204	.952			
			.900	.254	.954	.900	.123	.947			
			.950	.166	.949	.950	.084	.944			
			1.000	-.465	.912						
CN=				.6790			.8437				
CM=				-.1612			-.1786				



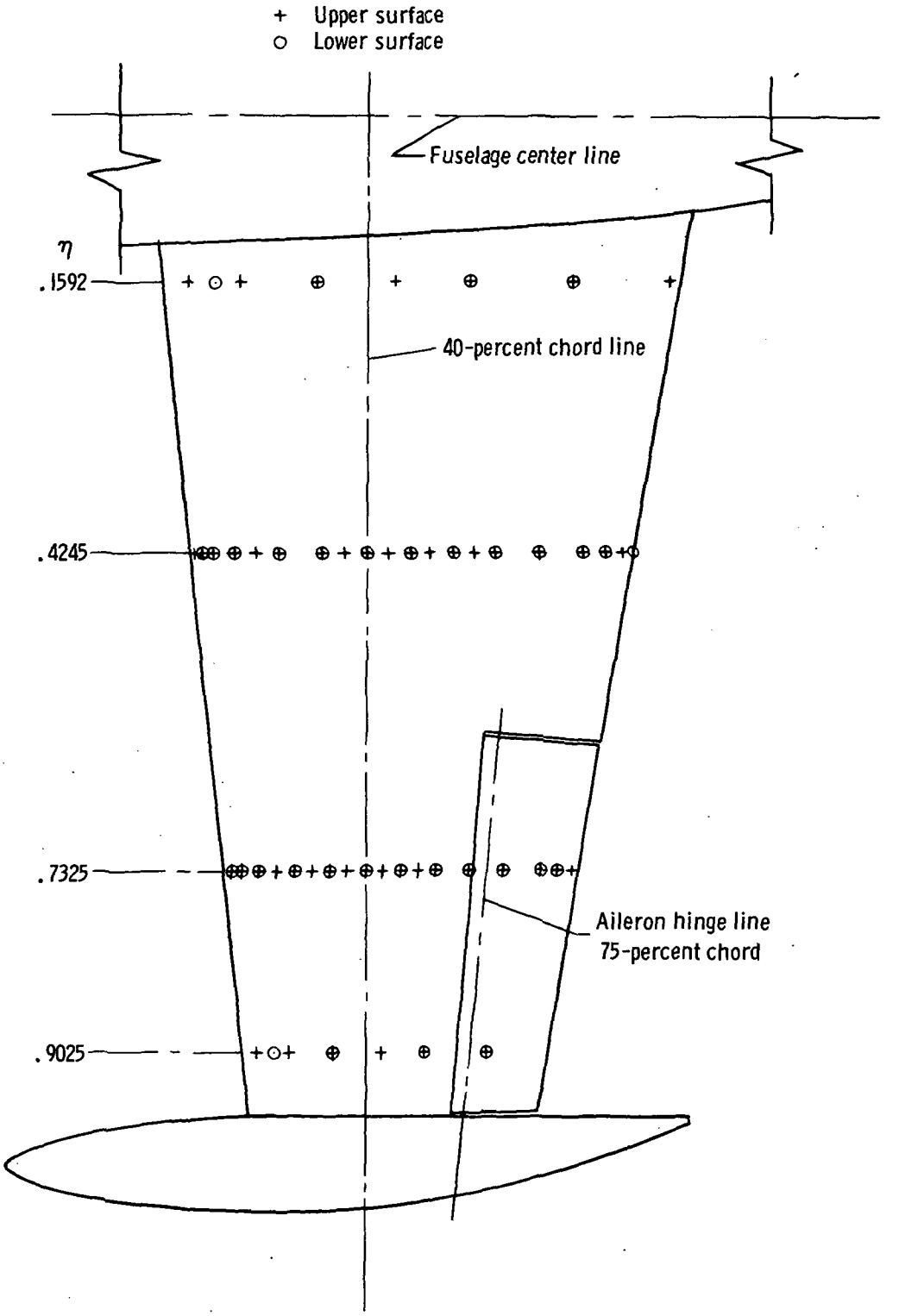
(a) General arrangement of model.

Figure 1.- Drawings of the wind-tunnel model. All dimensions are in terms of model mean geometric chord 20.318 cm.



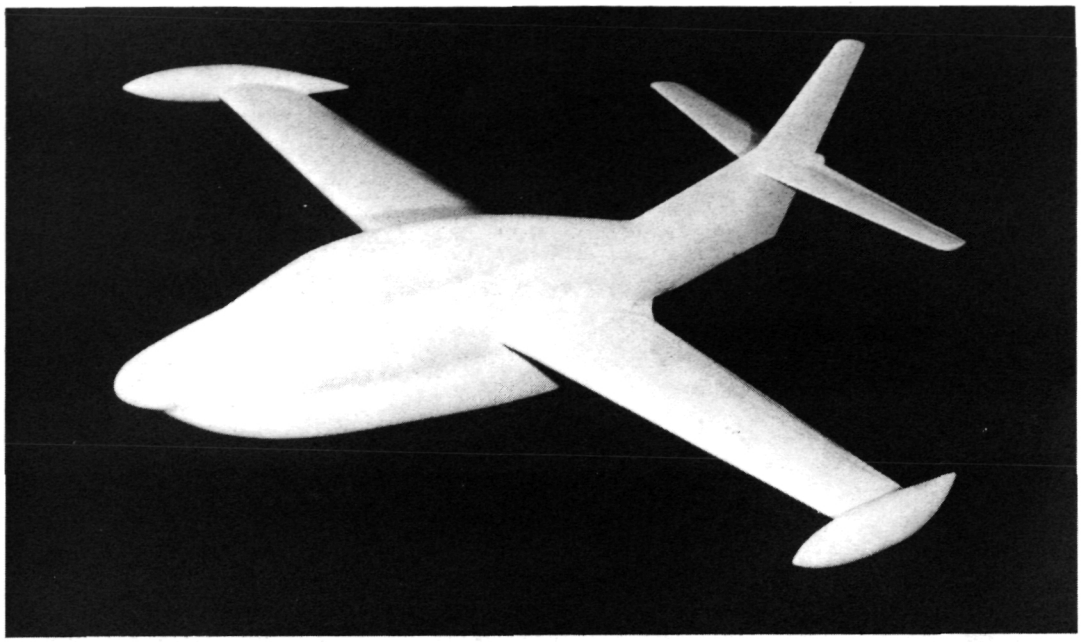
(b) 17-percent-thick supercritical airfoil.

Figure 1.- Continued.

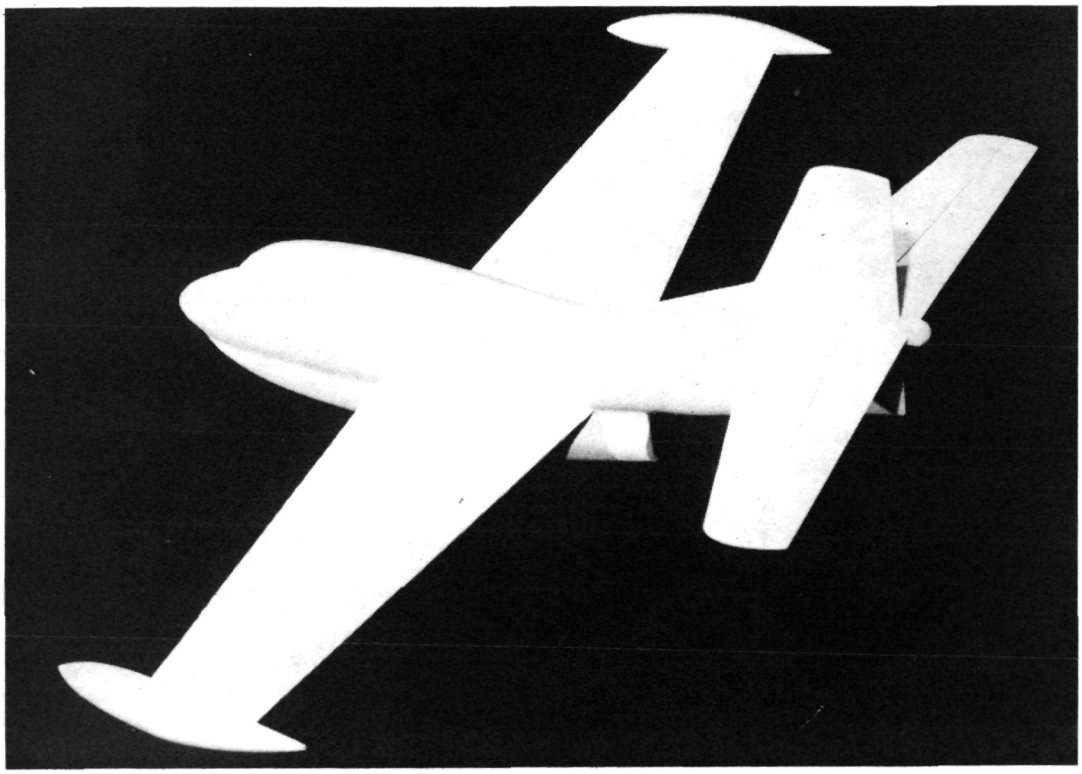


(c) Location of pressure orifices on wing.

Figure 1.- Concluded.



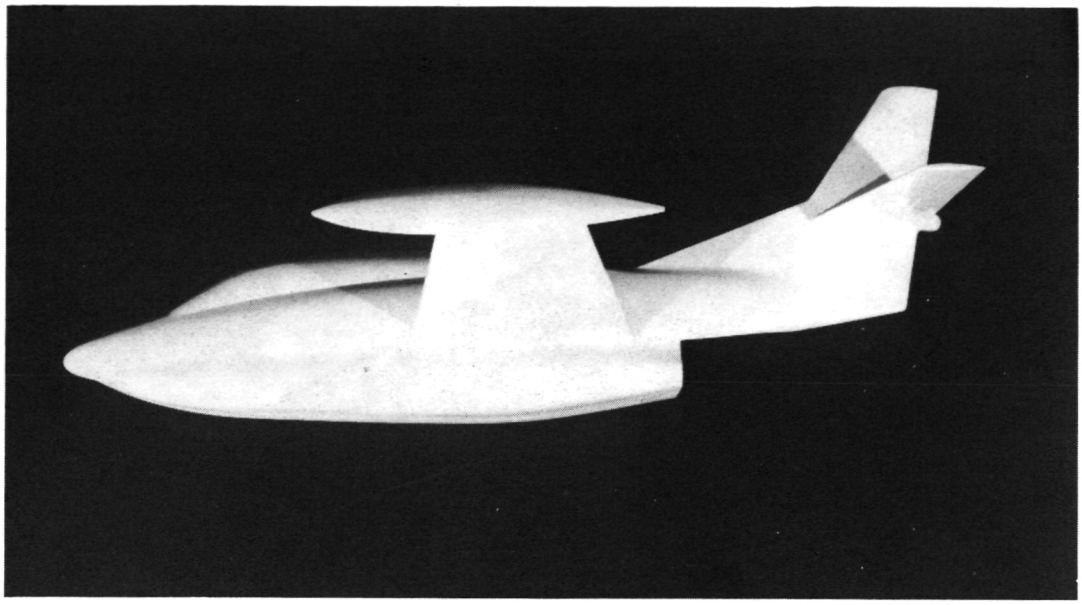
Three-quarter front L-70-6044



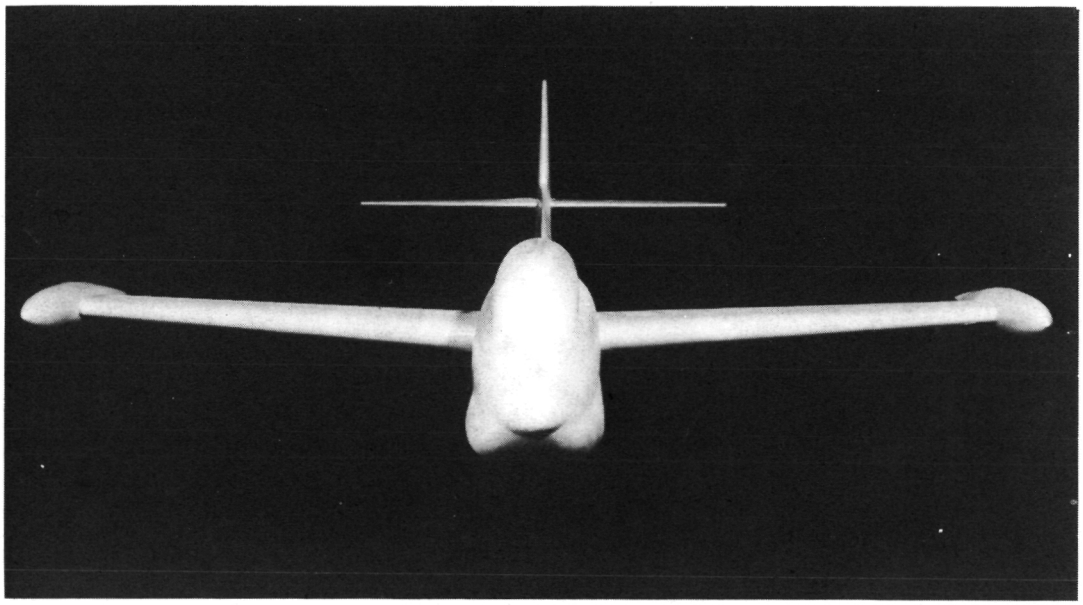
Three-quarter rear L-70-6042

(a) Photographs of wind-tunnel model.

Figure 2.- Model photographs.



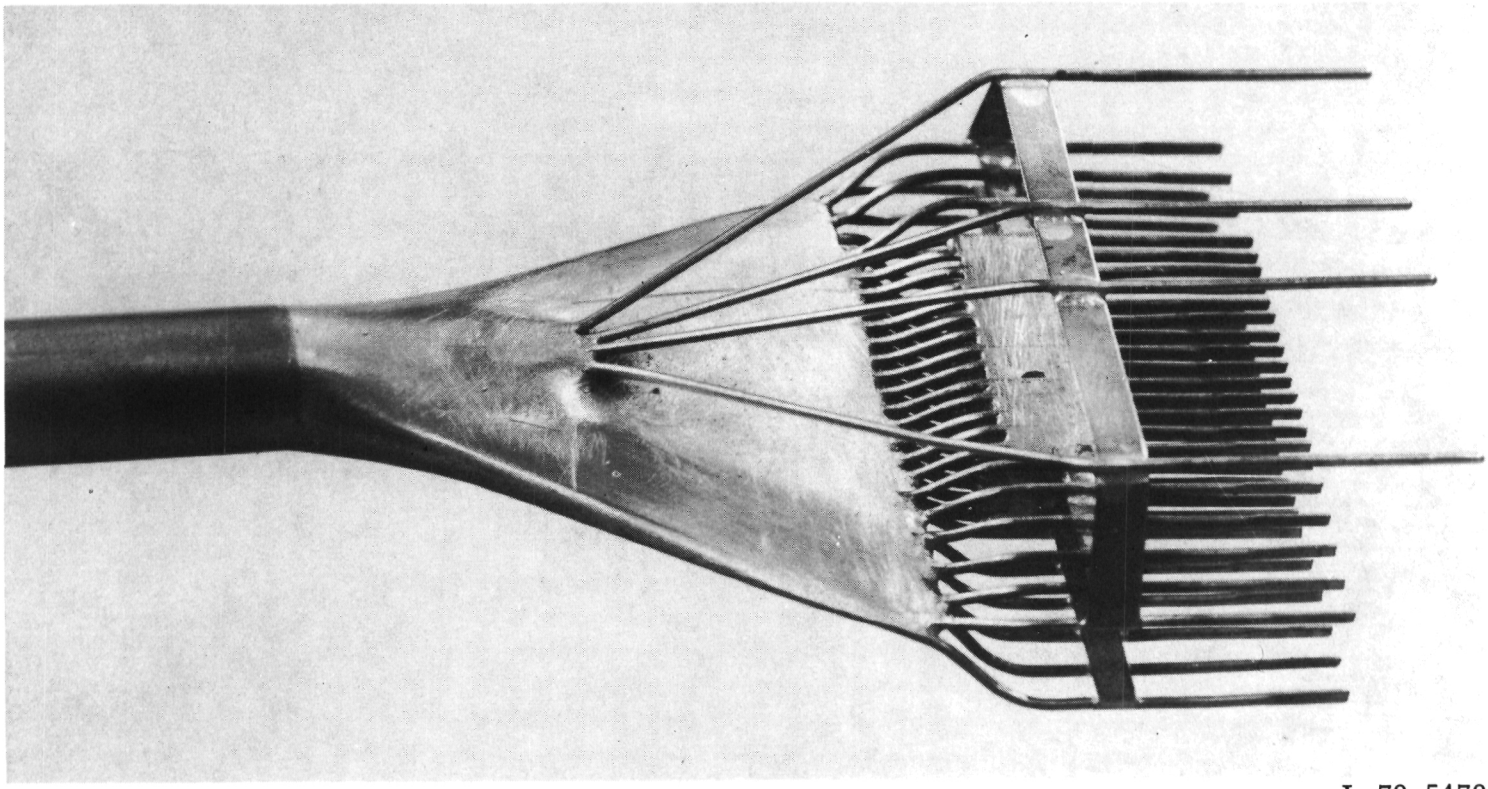
Lower side view L-70-6041



Front view L-70-6040

(a) Concluded.

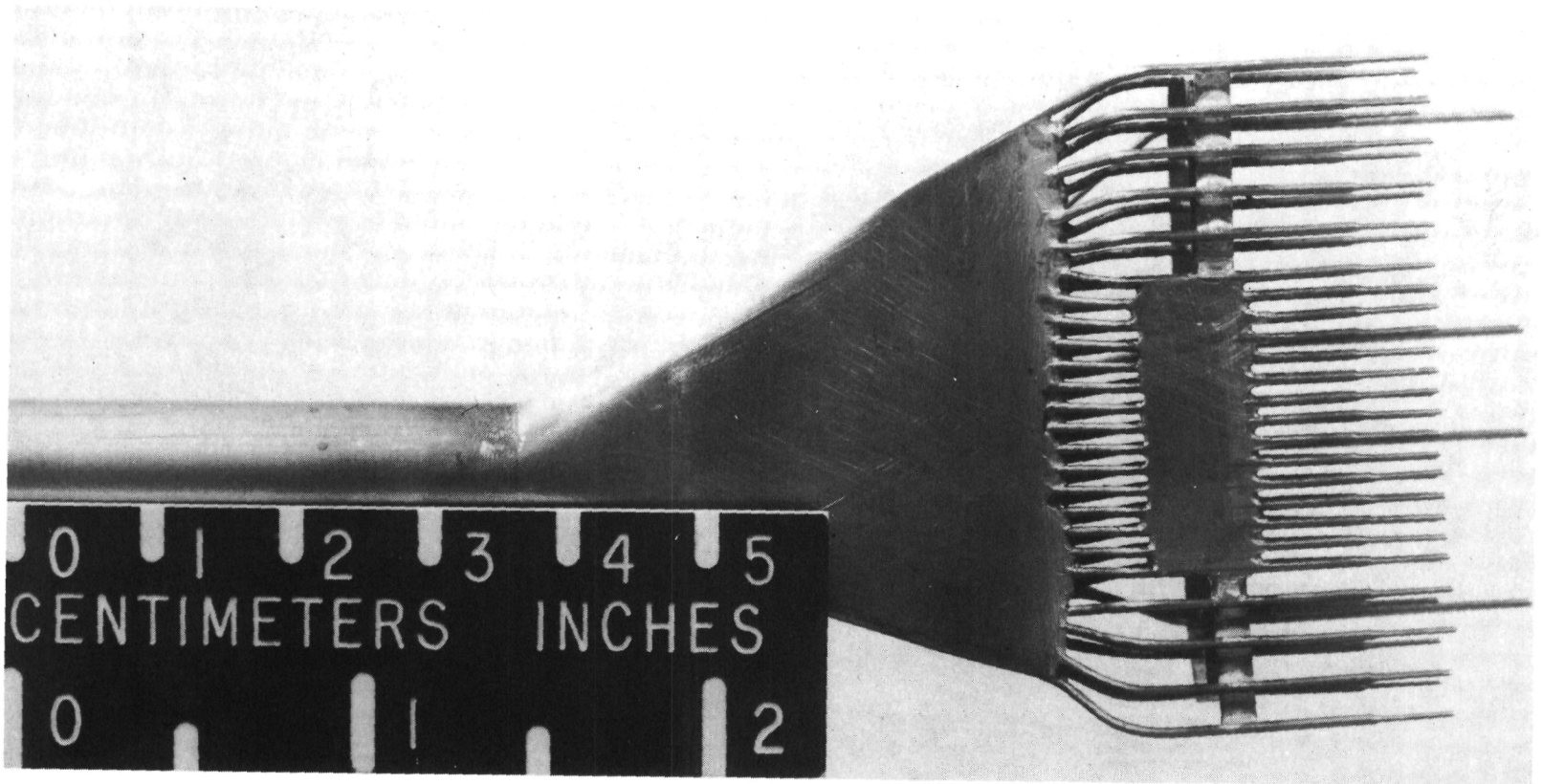
Figure 2.- Continued.



L-70-5470

(b) Photographs of profile drag rake.

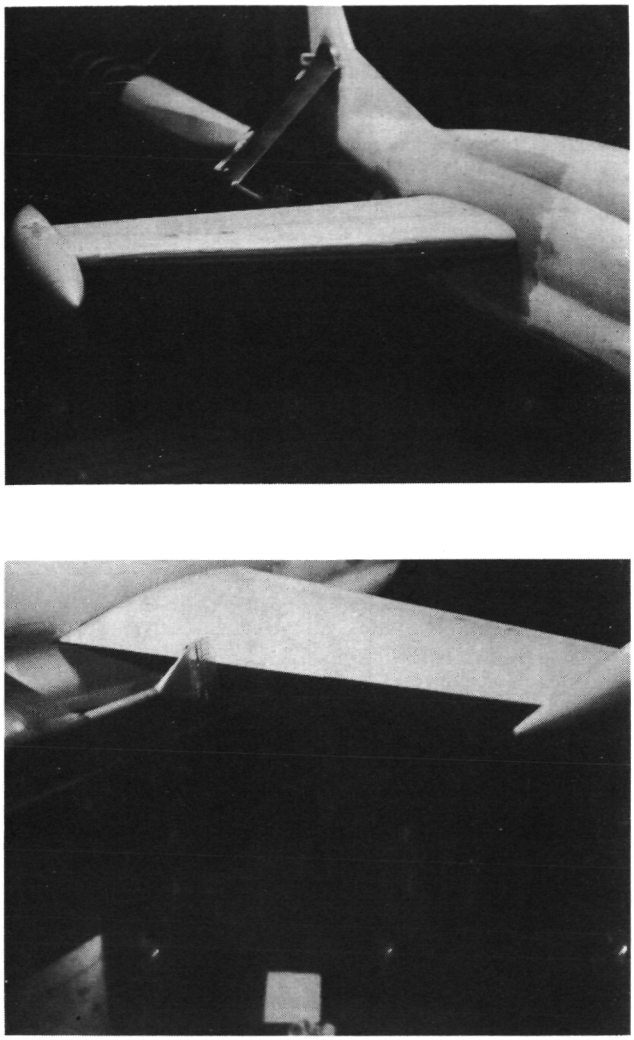
Figure 2.- Continued.



L-70-5471

(b) Concluded.

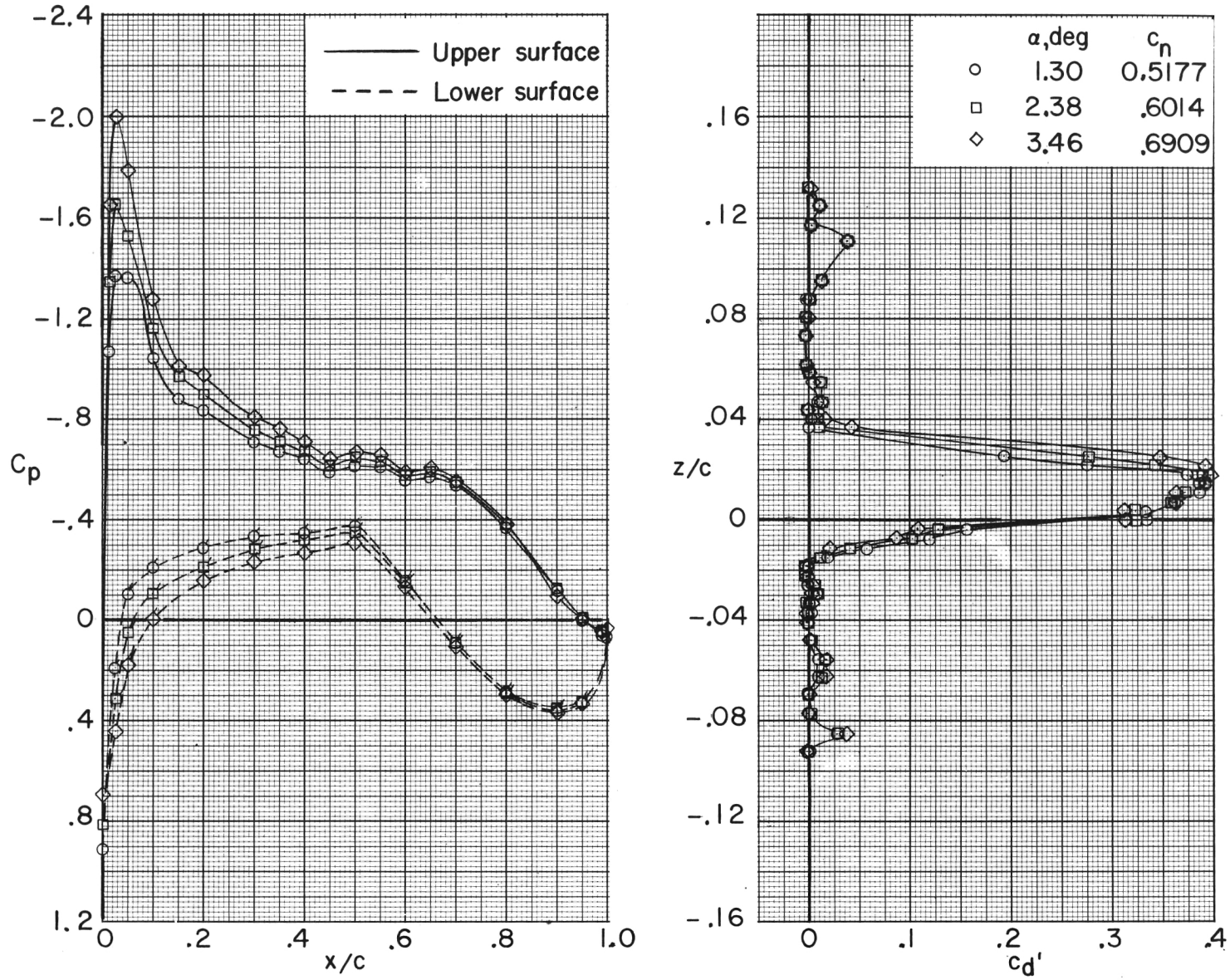
Figure 2.- Continued.



L-73-3042

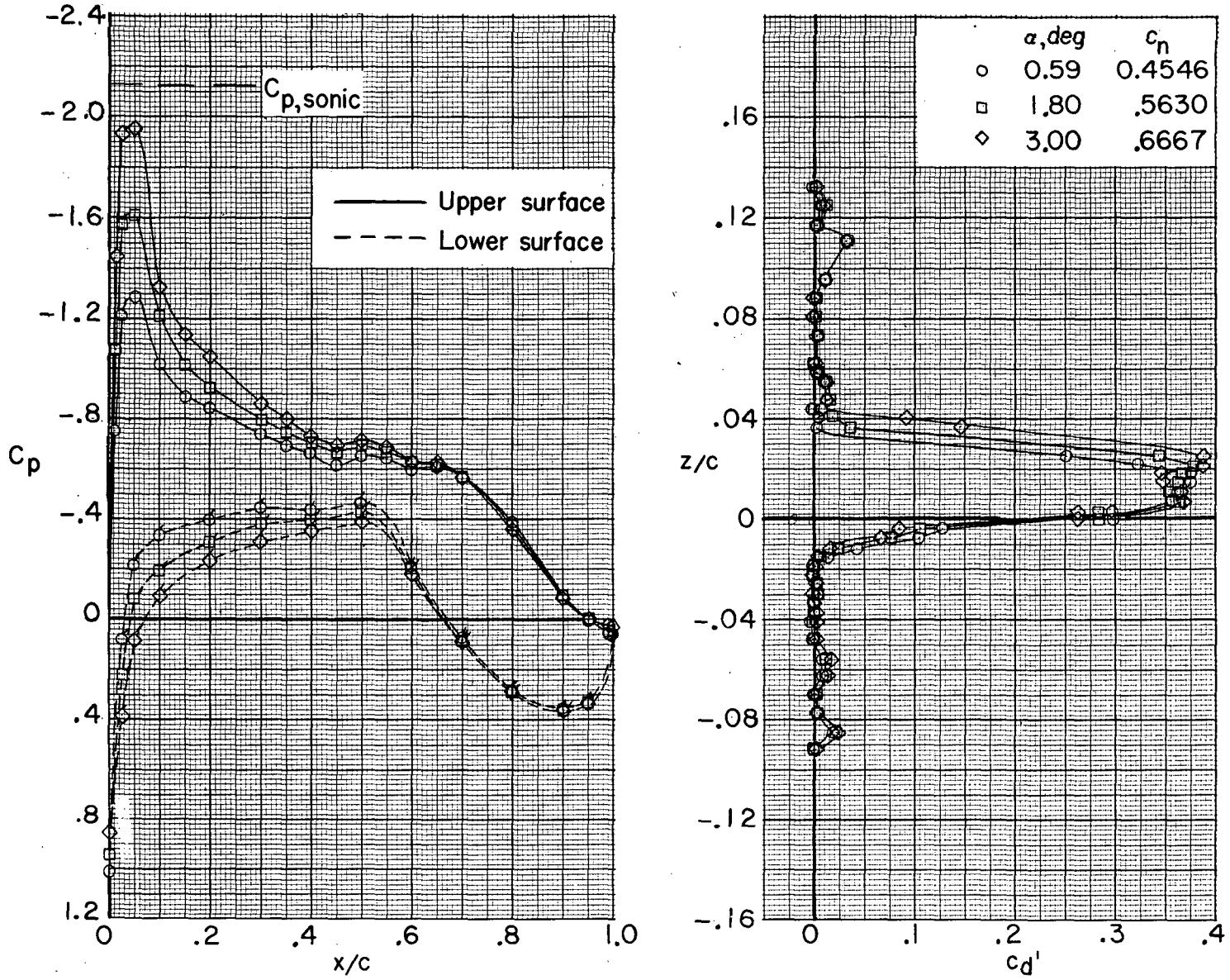
(c) Photographs of profile drag rake and support system mounted on model.

Figure 2.- Concluded.



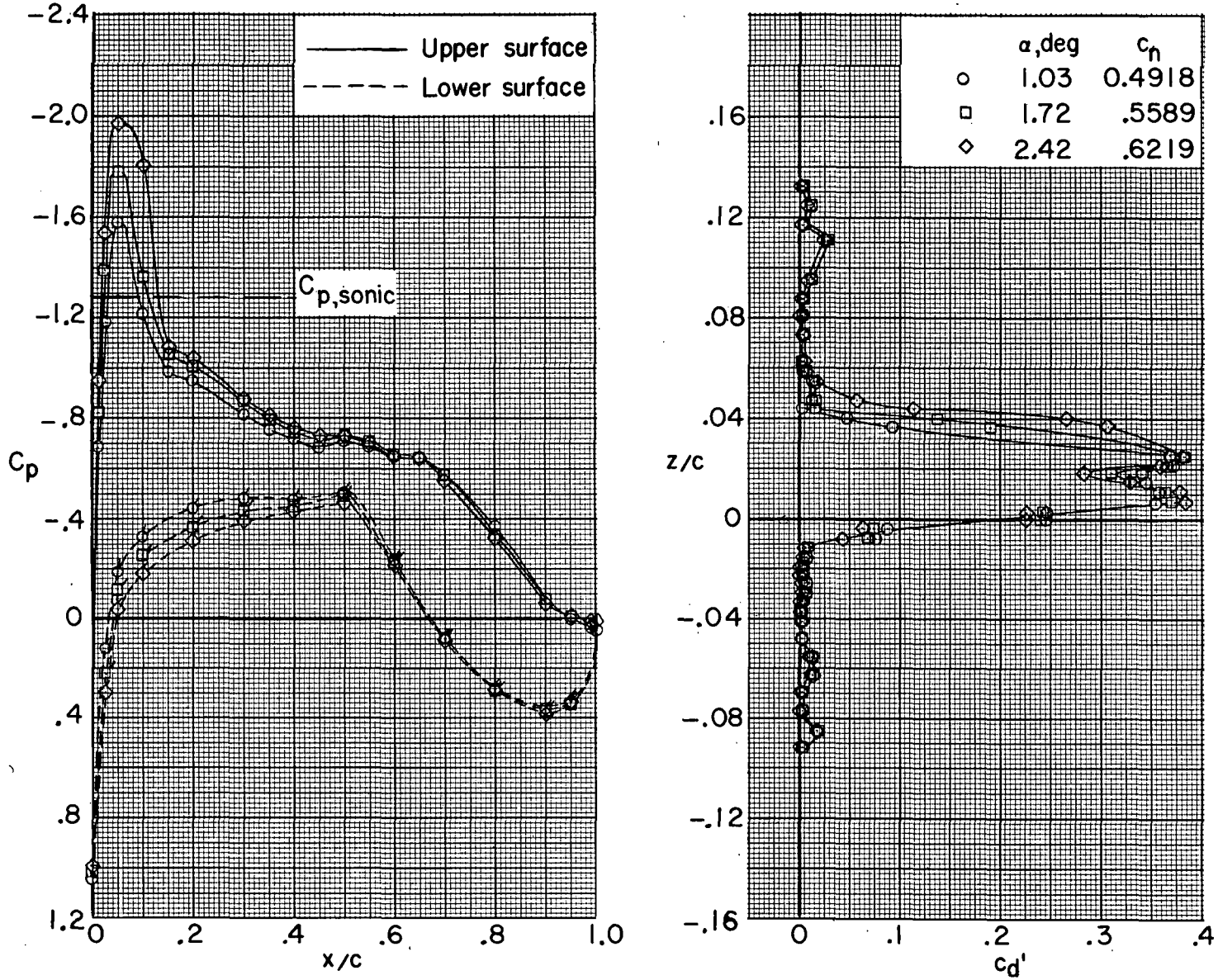
(a) M = 0.30.

Figure 3.- Chordwise pressure distributions with corresponding wake profile. η = 0.4245. Symbols without flags for pressure distributions correspond to upper surface; symbol with flags correspond to lower surface.



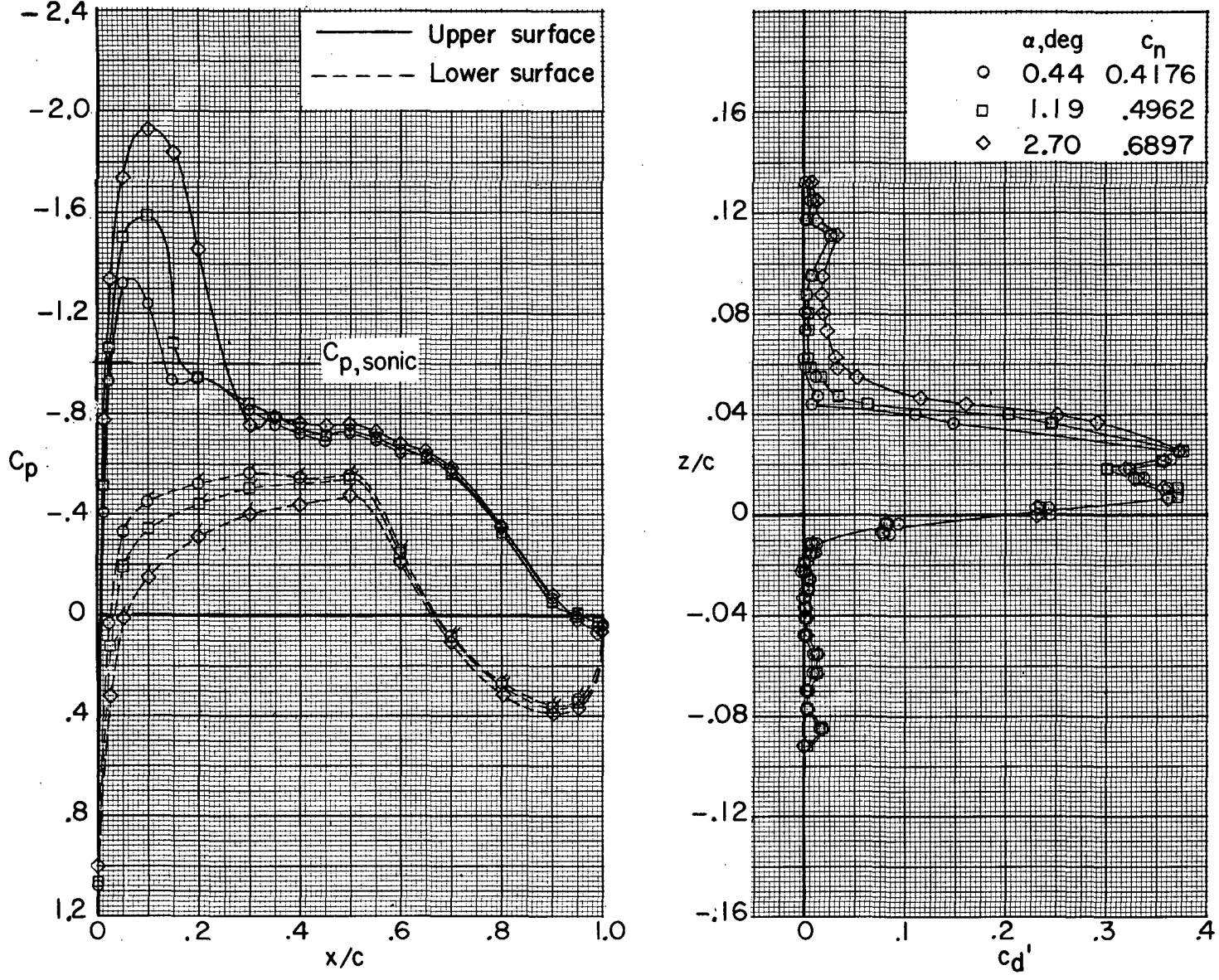
(b) M = 0.50.

Figure 3.- Continued.



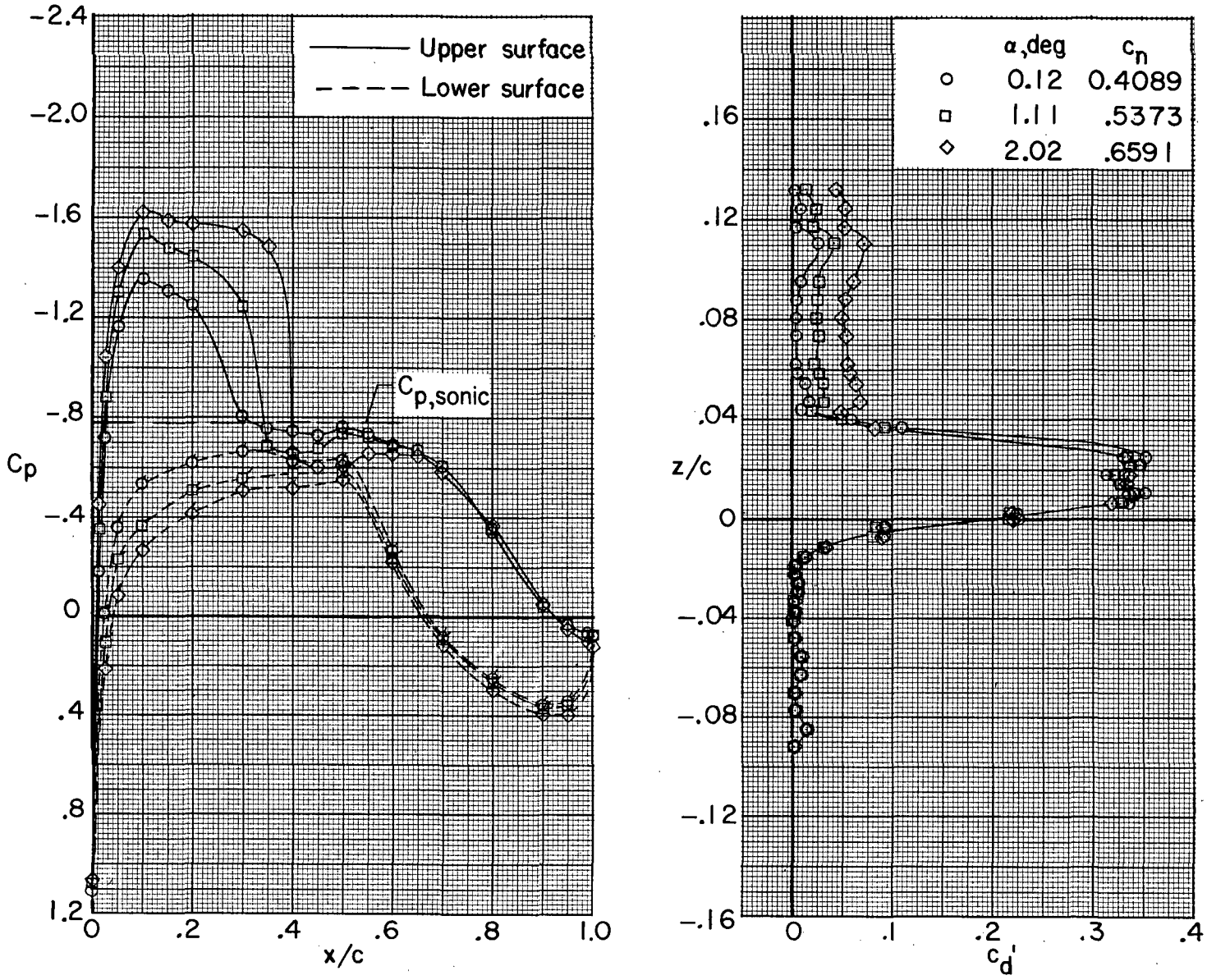
(c) M = 0.60.

Figure 3.- Continued.



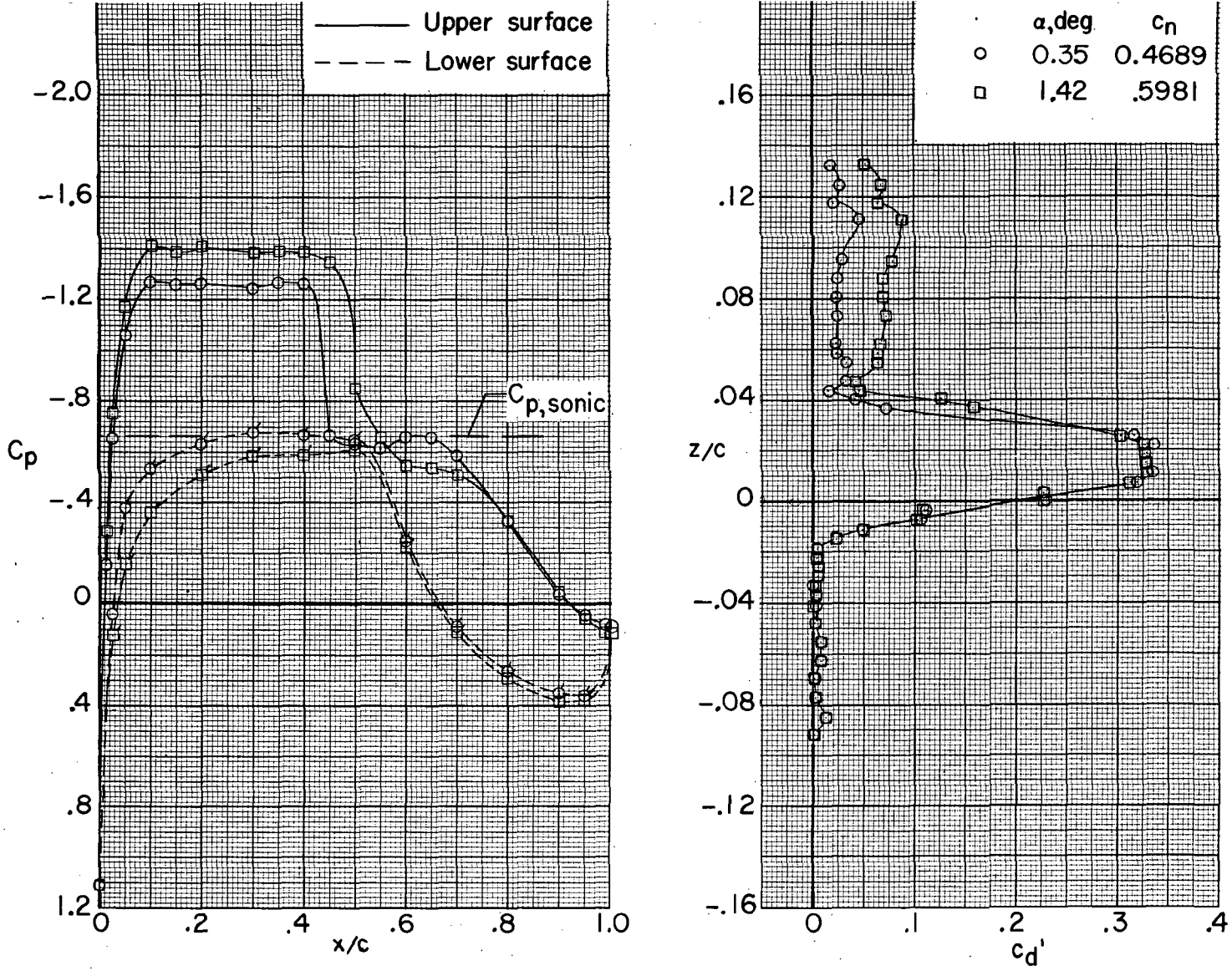
(d) M = 0.65.

Figure 3.- Continued.



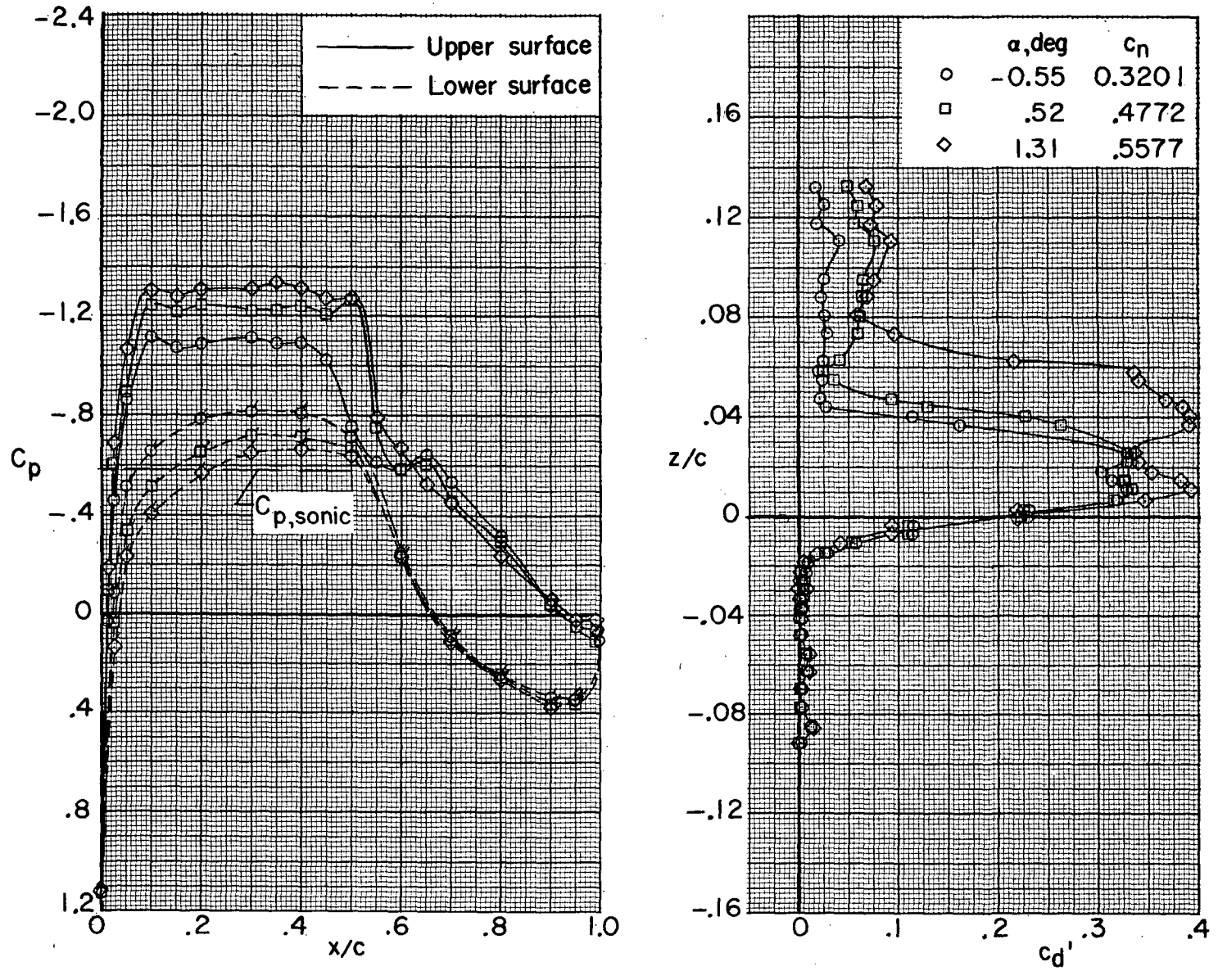
(e) M = 0.70.

Figure 3.- Continued.



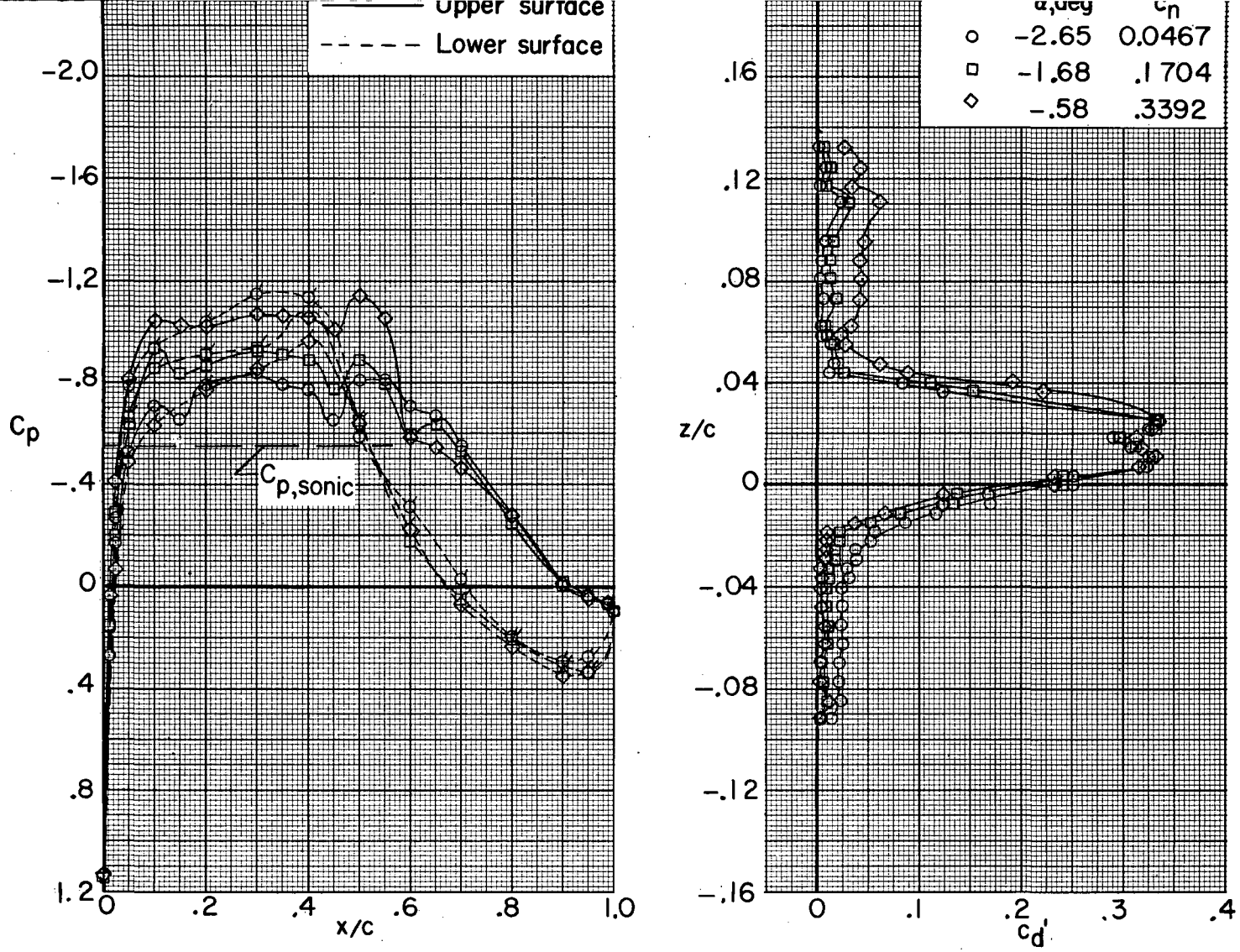
(f) M = 0.73.

Figure 3.- Continued.



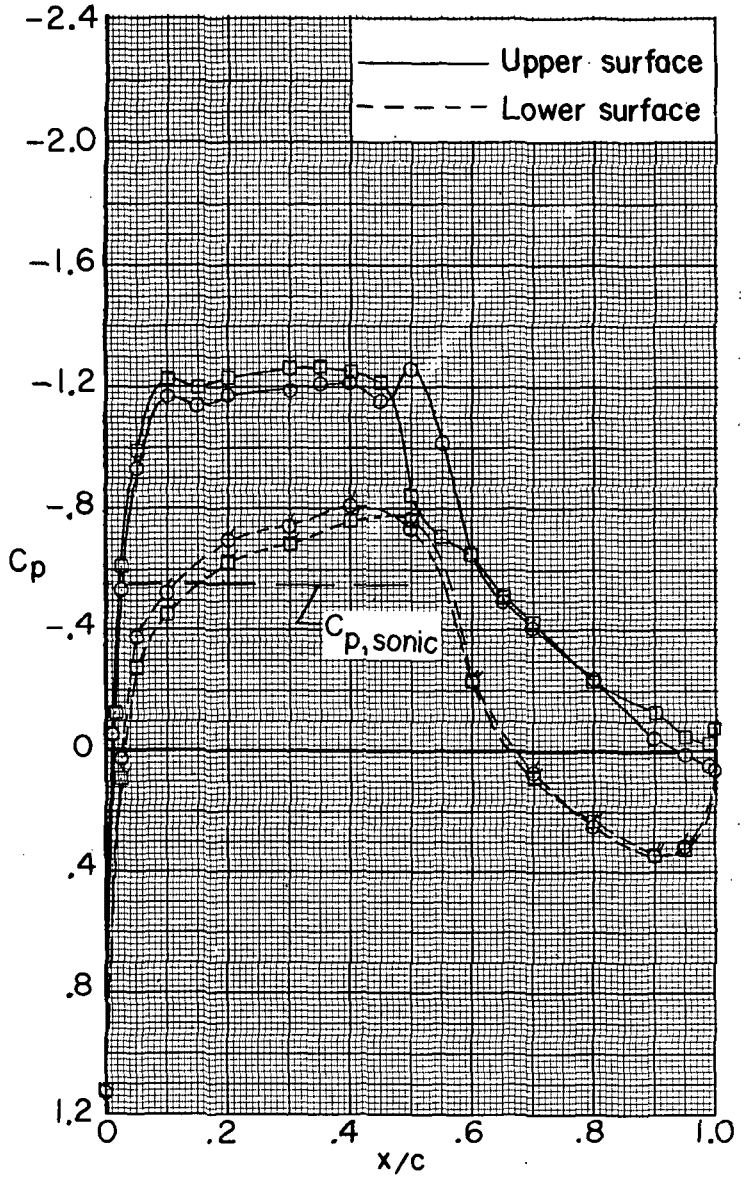
(g) M = 0.75.

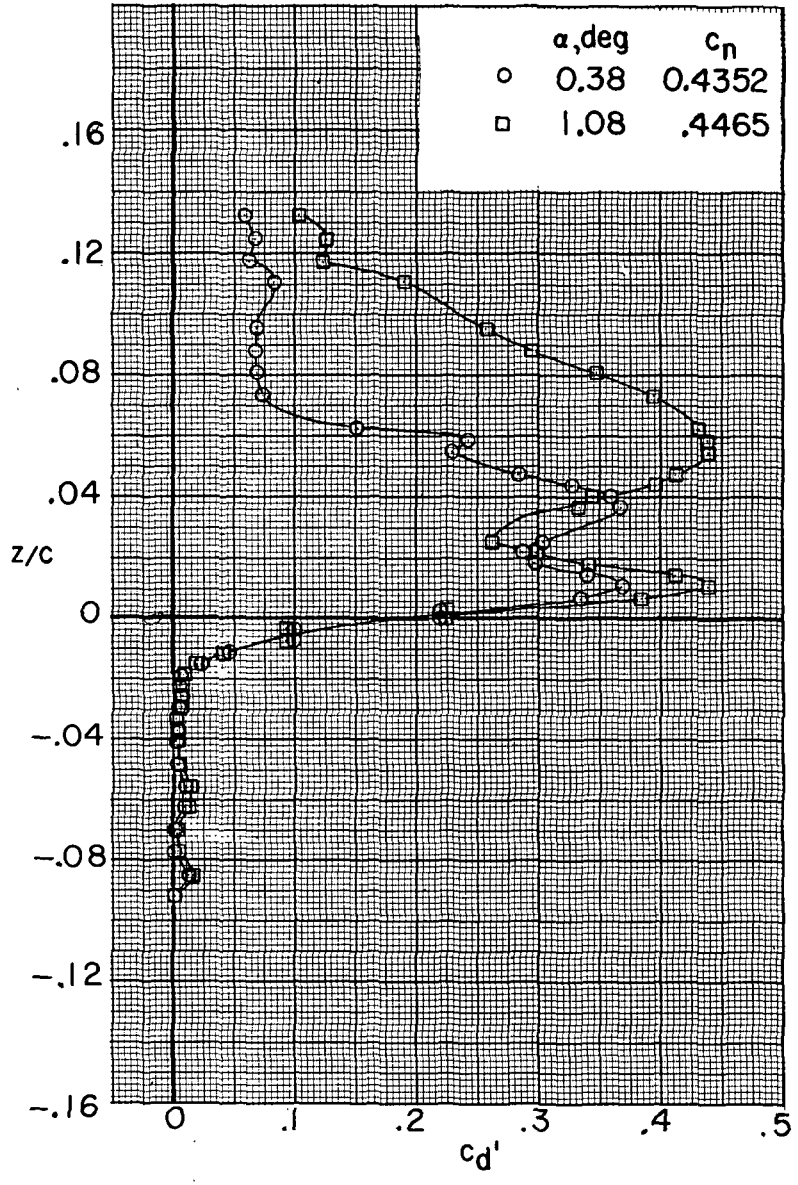
Figure 3.- Continued.



(h) M = 0.76.

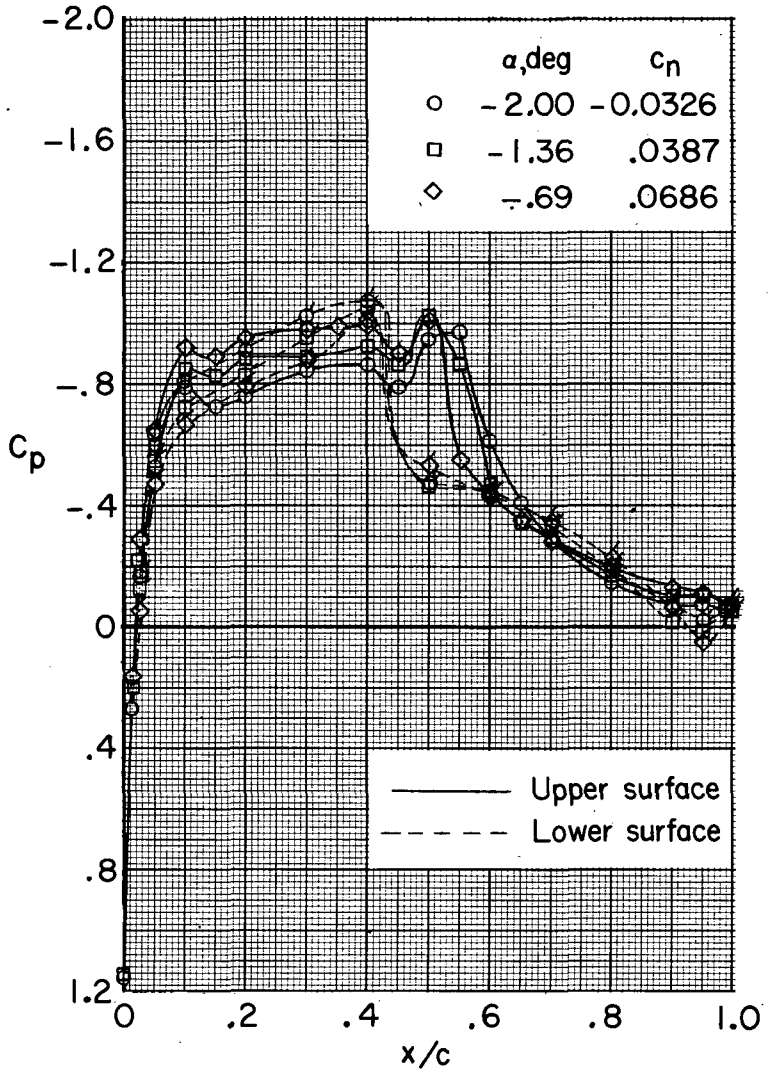
Figure 3.- Continued.





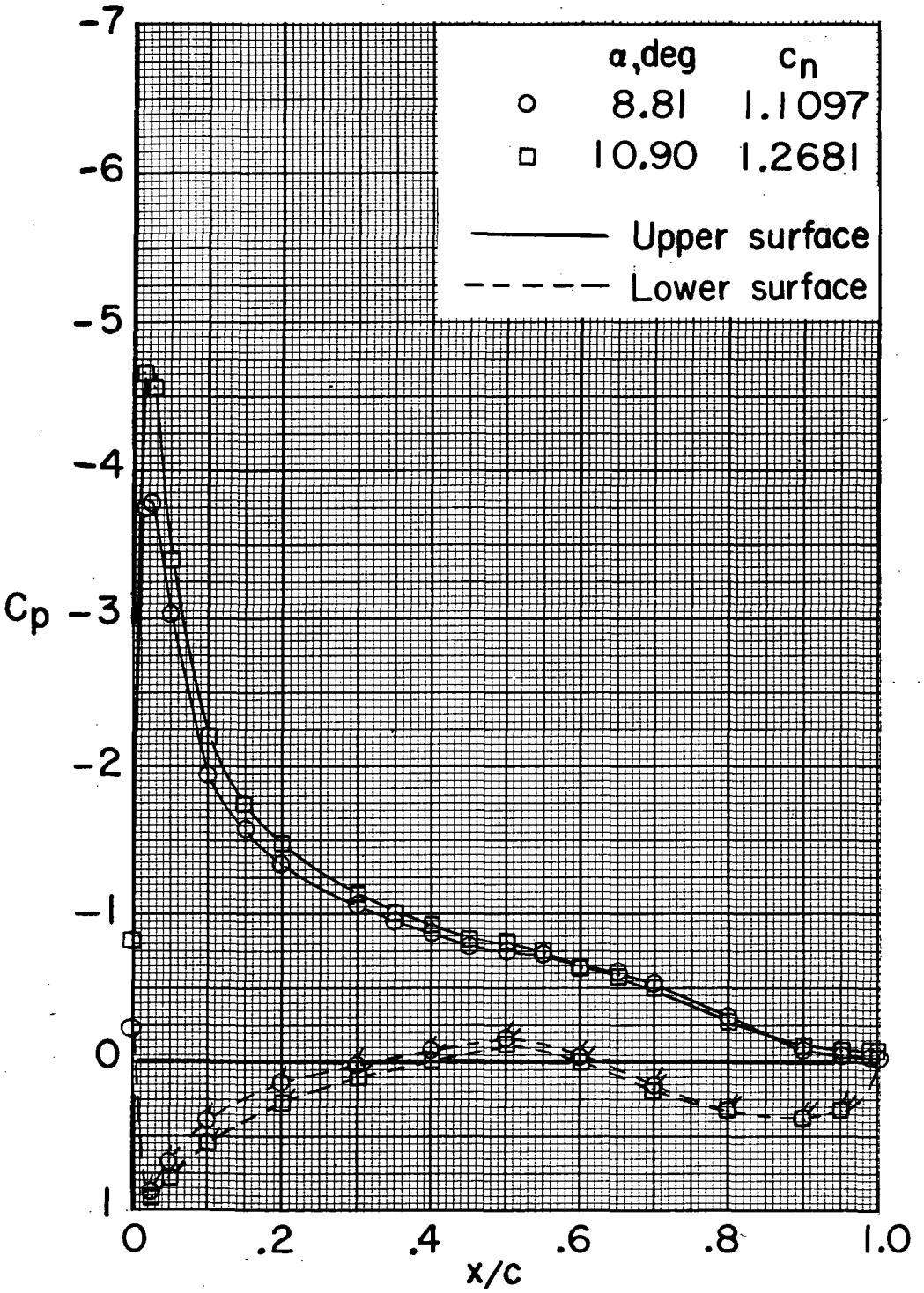
(h) M = 0.76. Concluded.

Figure 3 - Continued



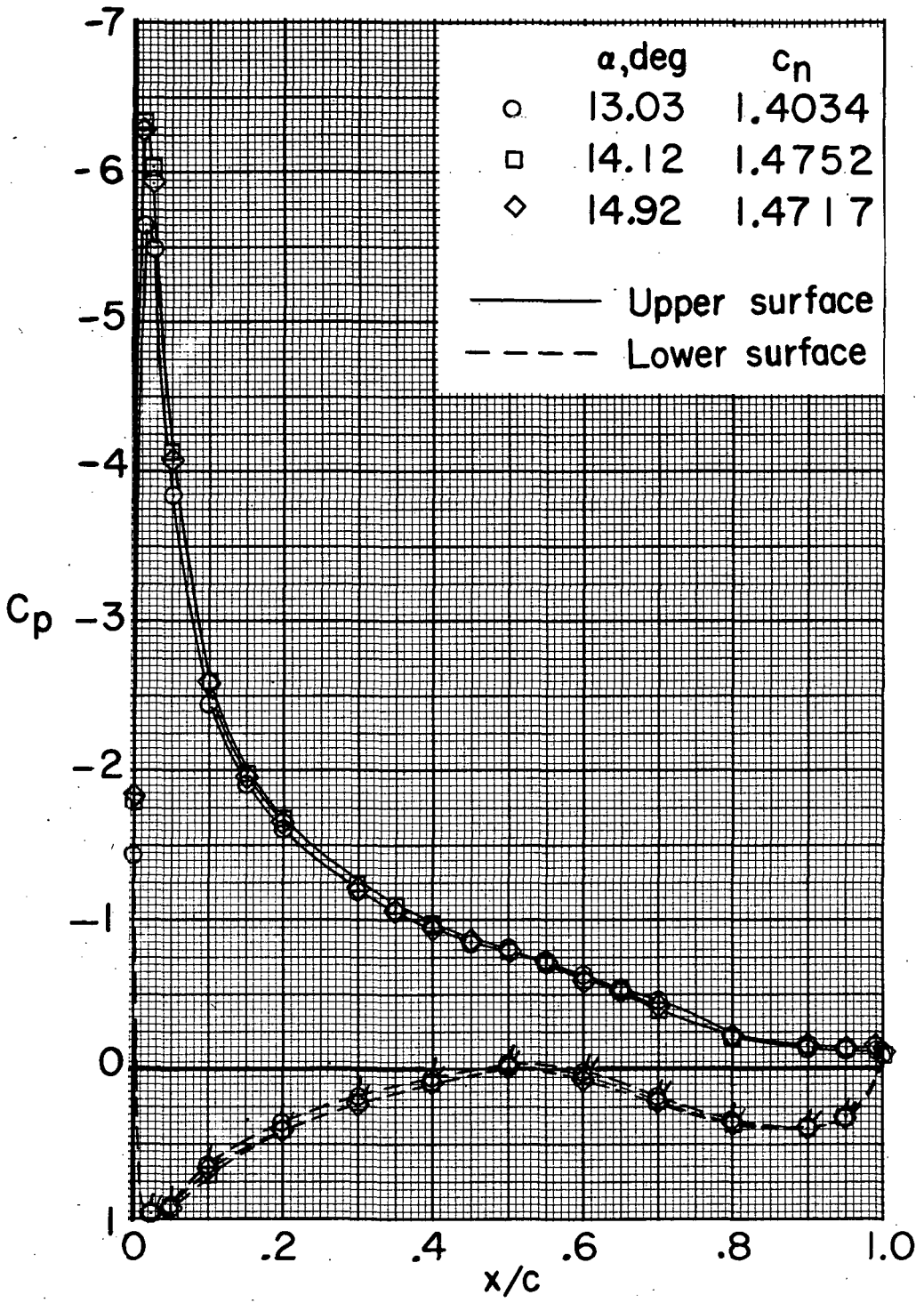
(i) M = 0.80.

Figure 3.- Concluded.



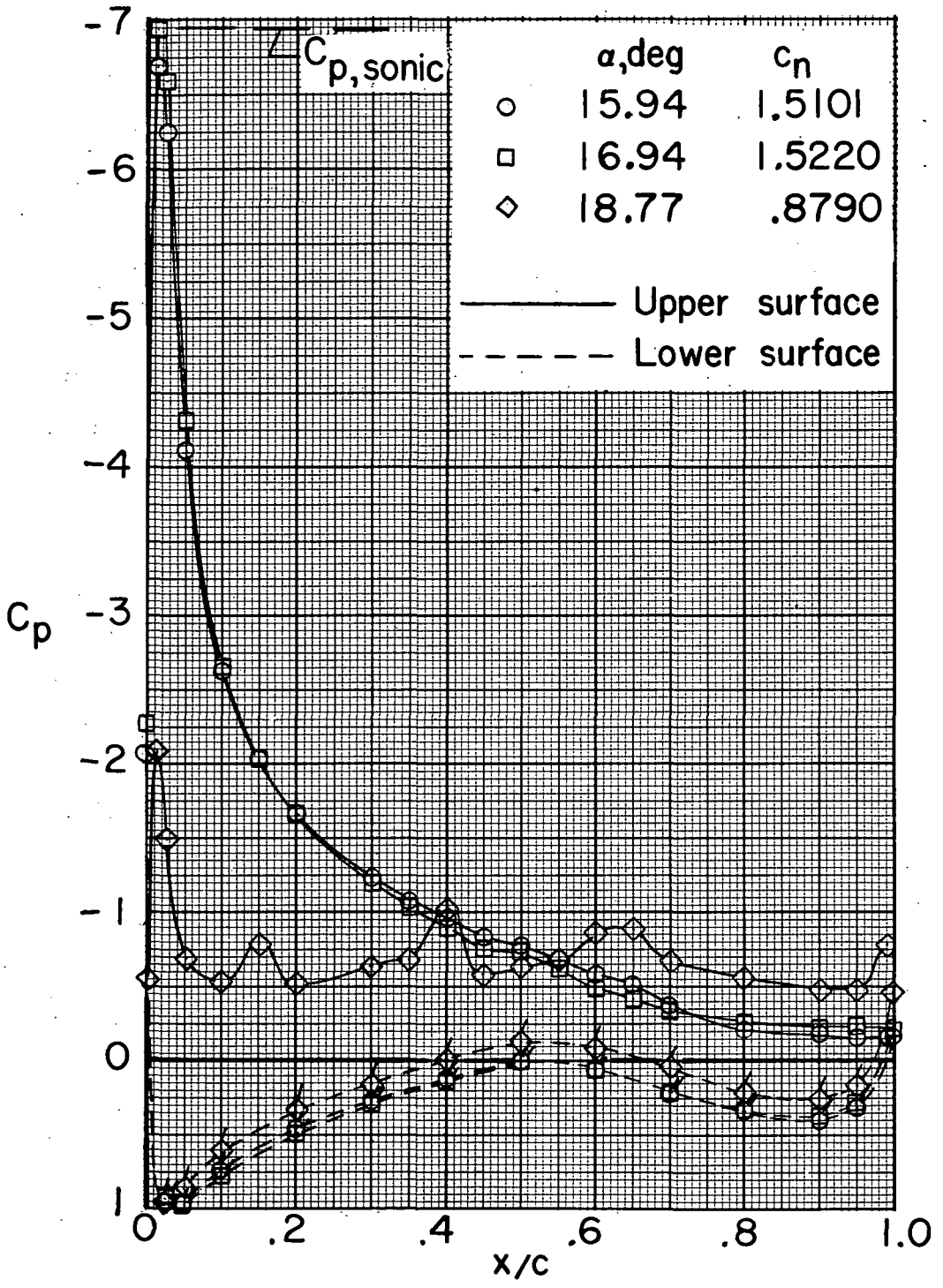
(a) M = 0.30.

Figure 4.- Chordwise pressure distribution through extended angle-of-attack range. $\eta = 0.4245$; $i_h = 0^o$; $\delta_e = 0^o$. Symbols without flags correspond to upper surface; symbols with flags correspond to lower surface.



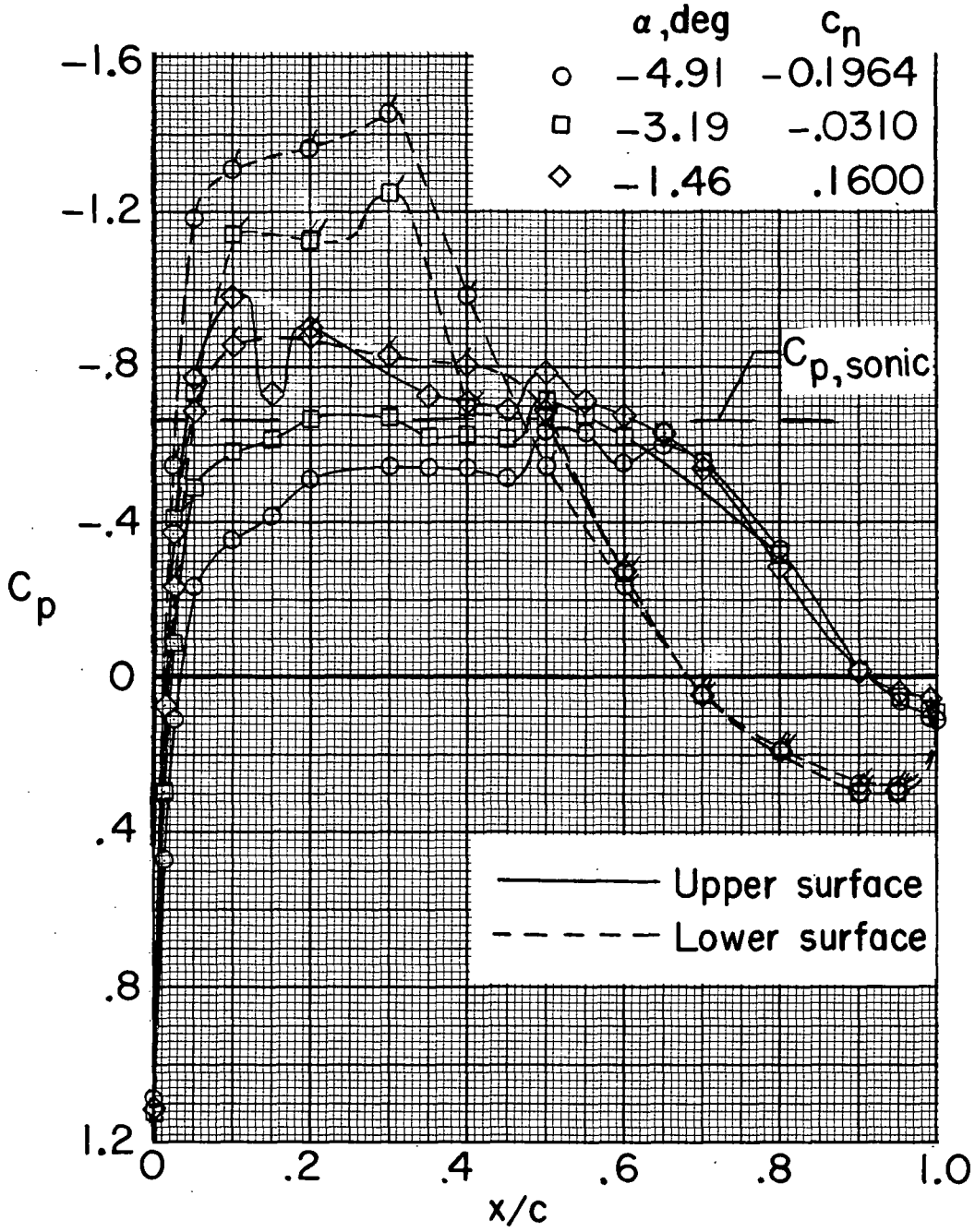
(a) M = 0.30. Continued.

Figure 4.- Continued.



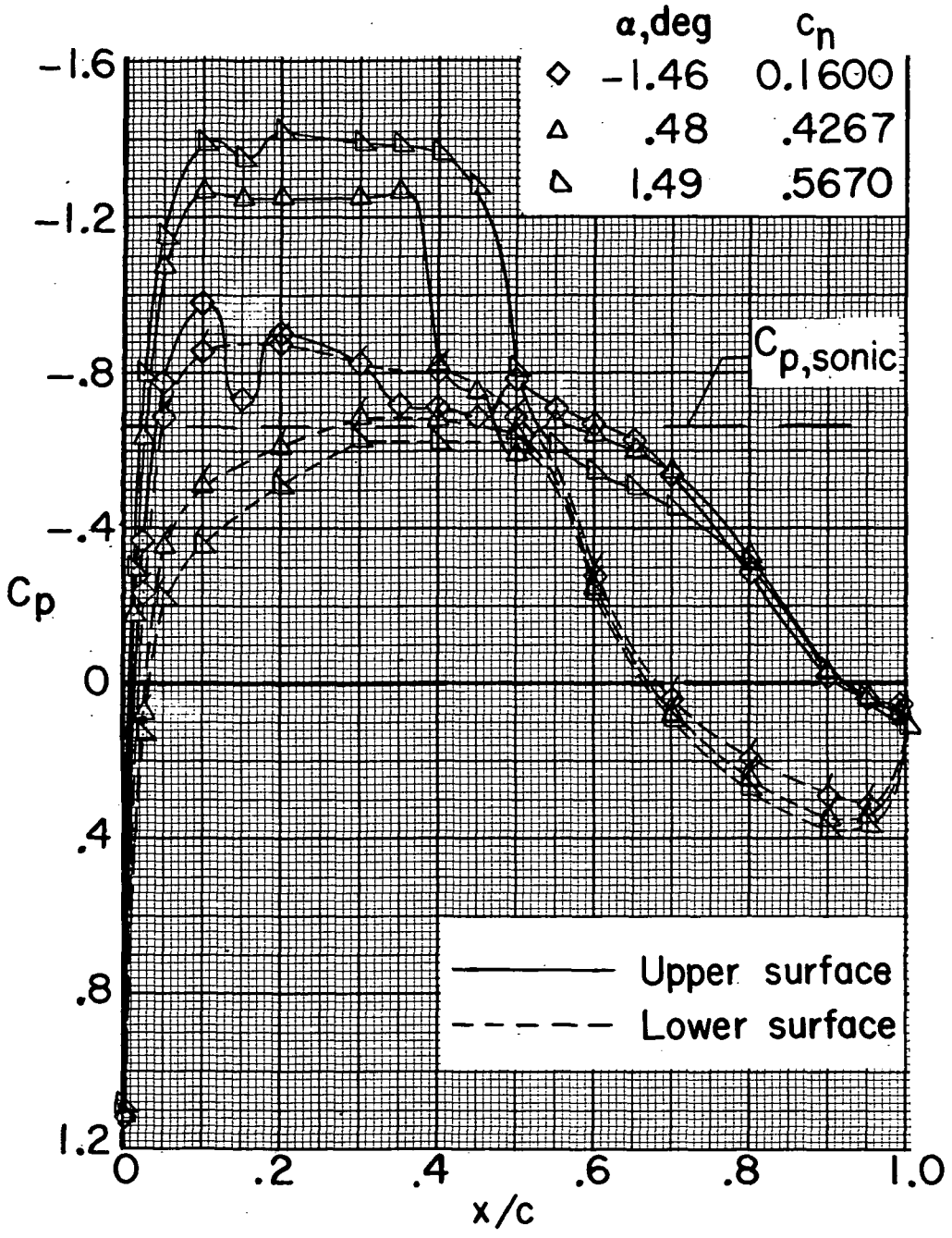
(a) M = 0.30. Concluded.

Figure 4.- Continued.



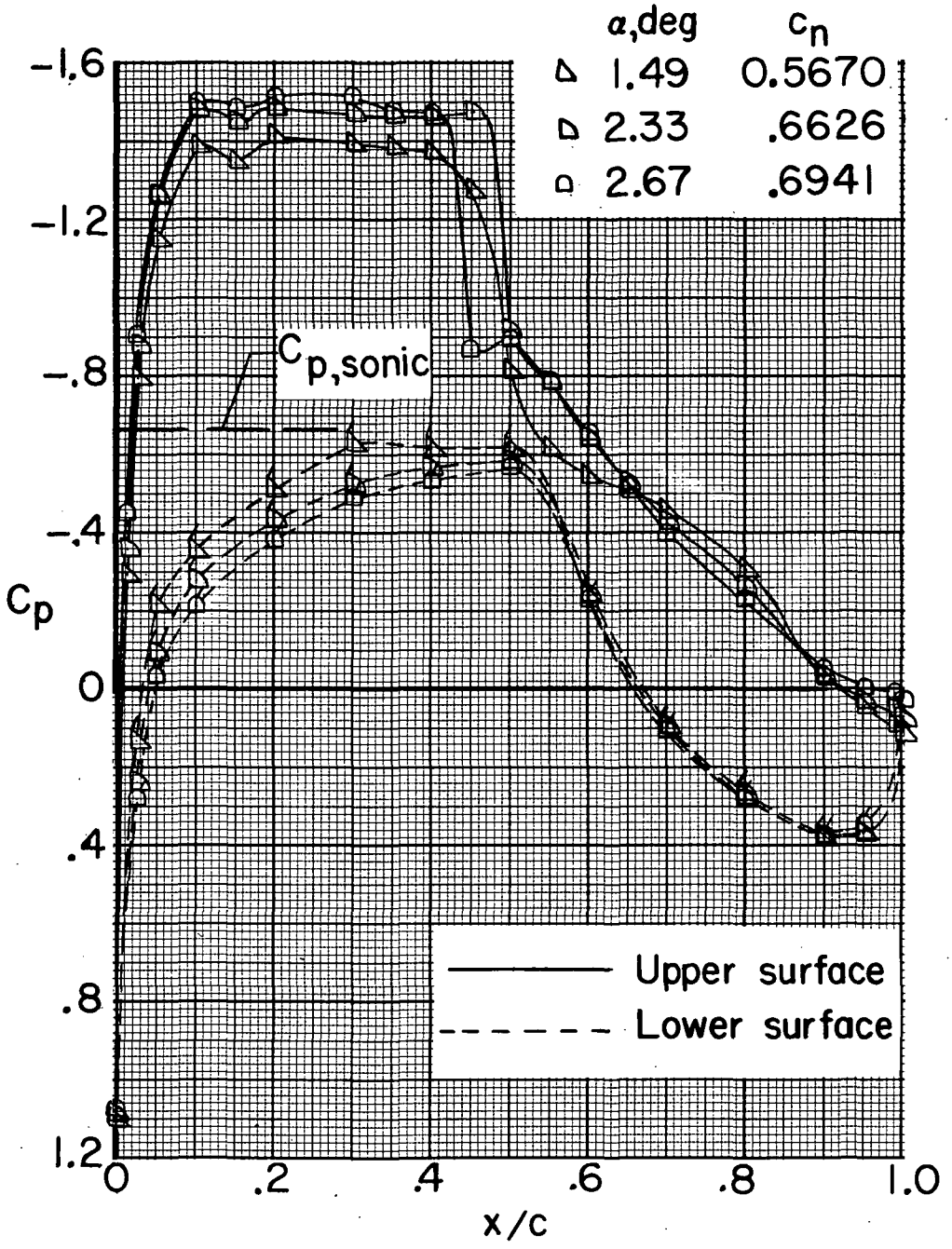
(b) M = 0.73.

Figure 4.- Continued.



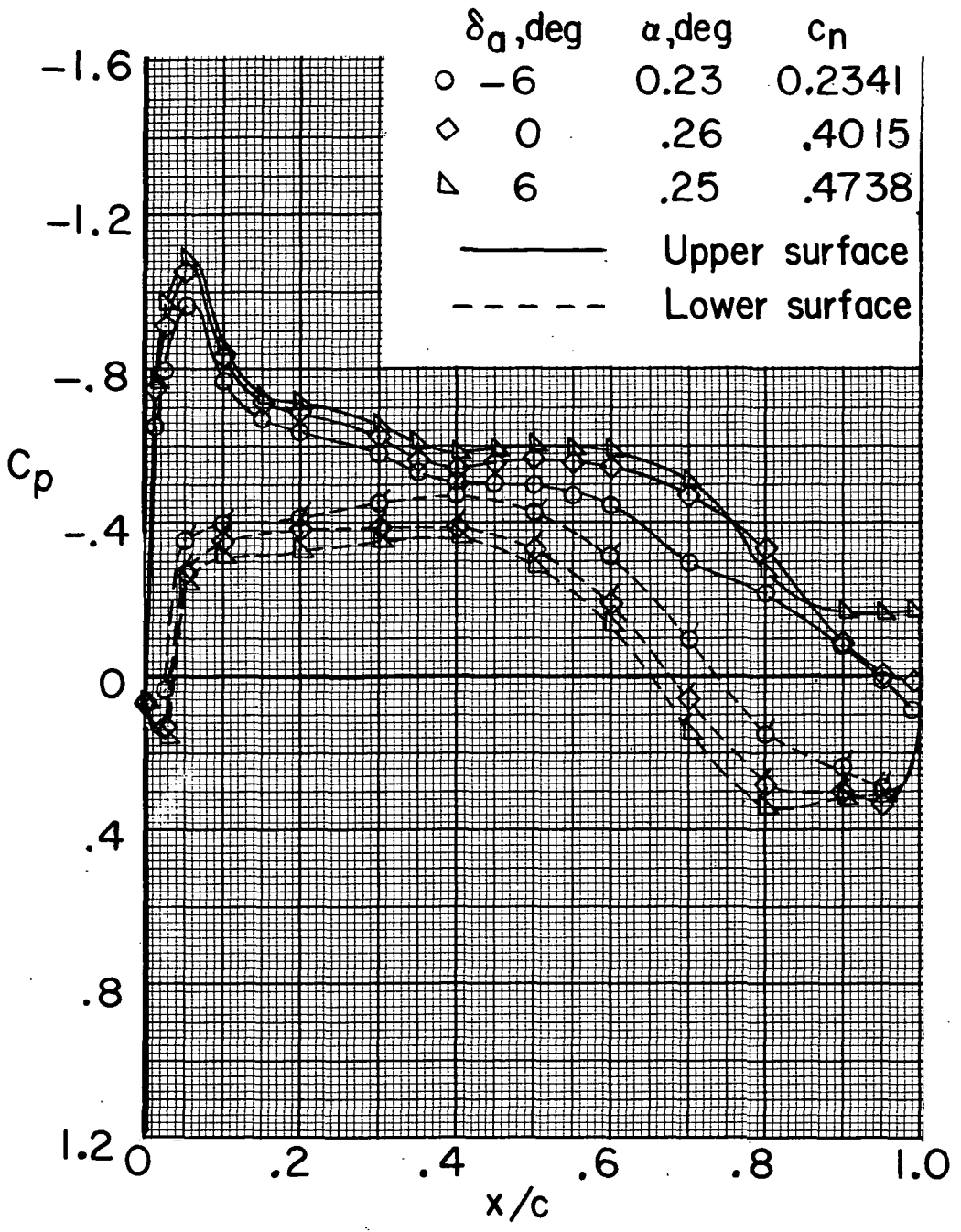
(b) M = 0.73. Continued.

Figure 4.- Continued.



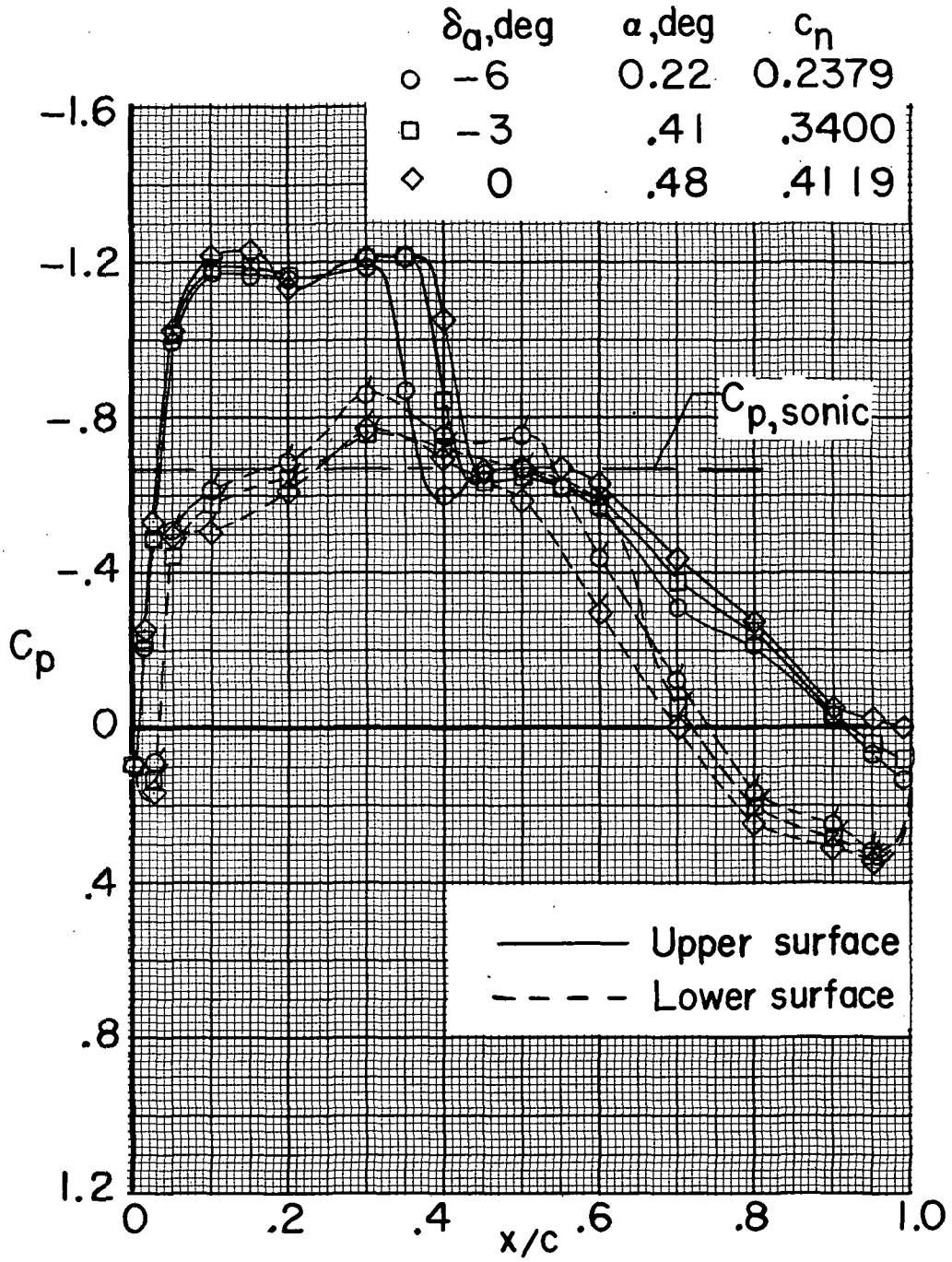
(b) M = 0.73. Concluded.

Figure 4.- Concluded.



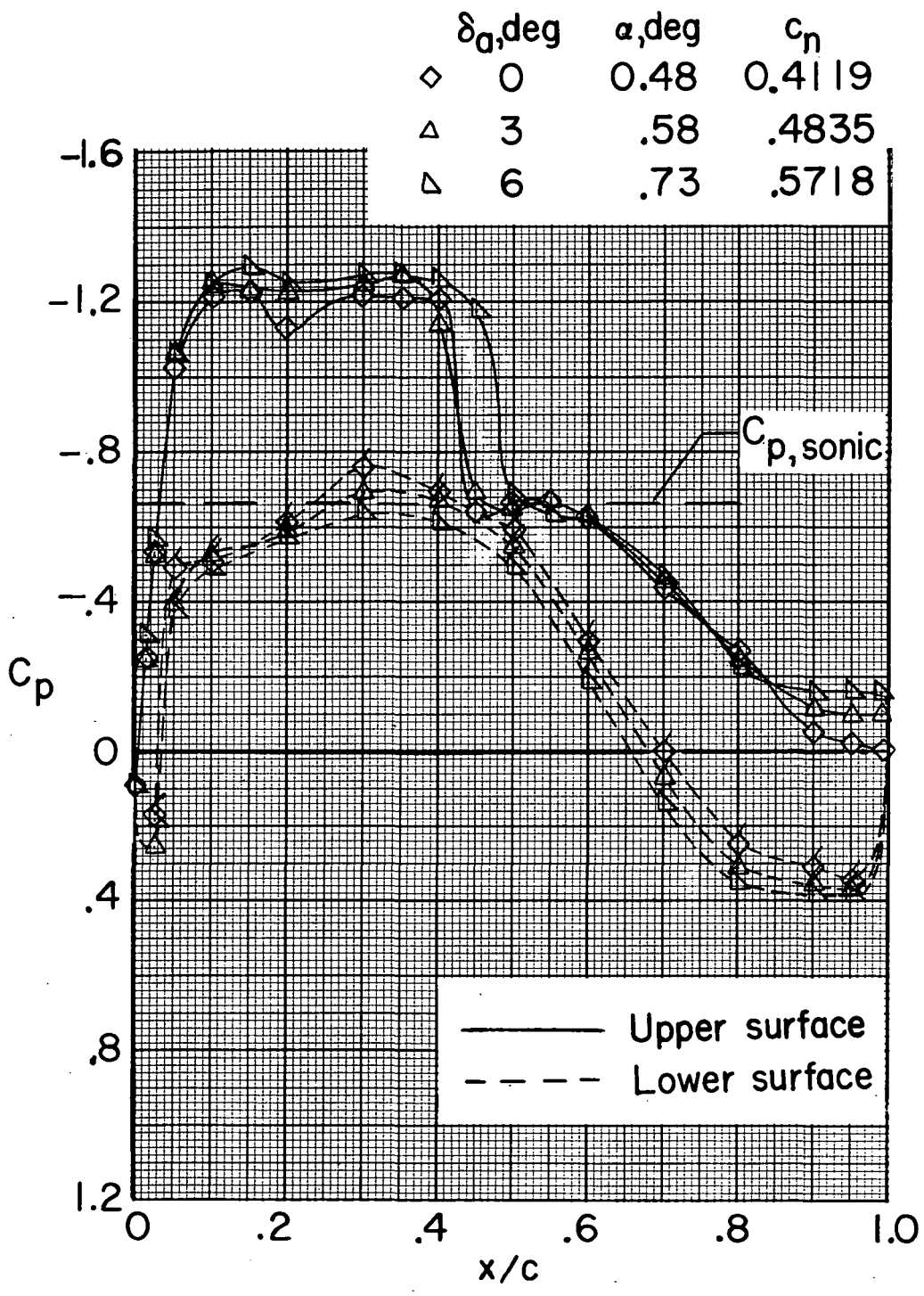
(a) M = 0.30.

Figure 5.- Effect of aileron deflection on the chordwise pressure distribution. $\eta = 0.7325$; $i_h = 0^o$; $\delta_e = 0^o$. Symbols without flags correspond to upper surface; symbols with flags correspond to lower surface.



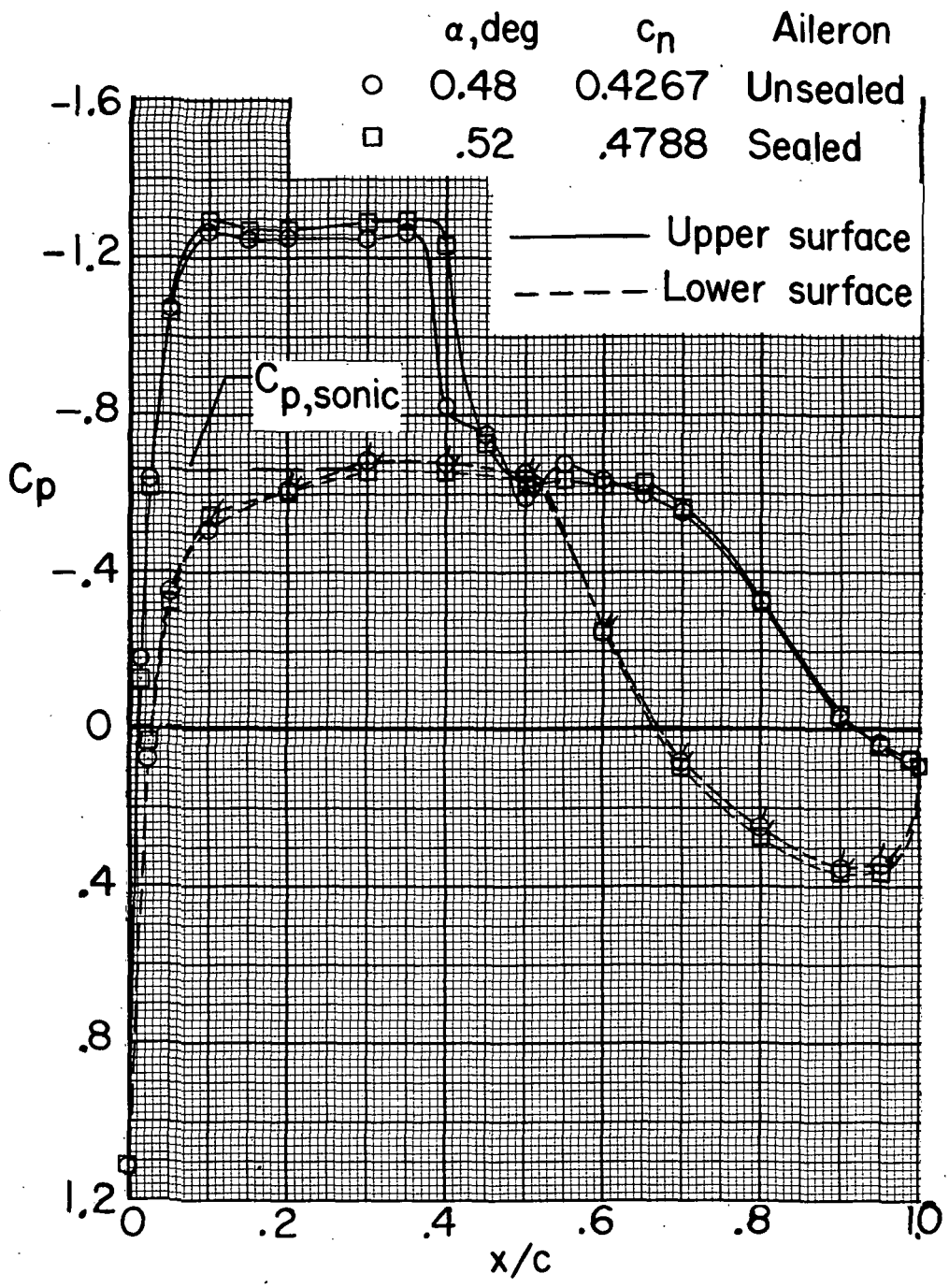
(b) M = 0.73.

Figure 5.- Continued.



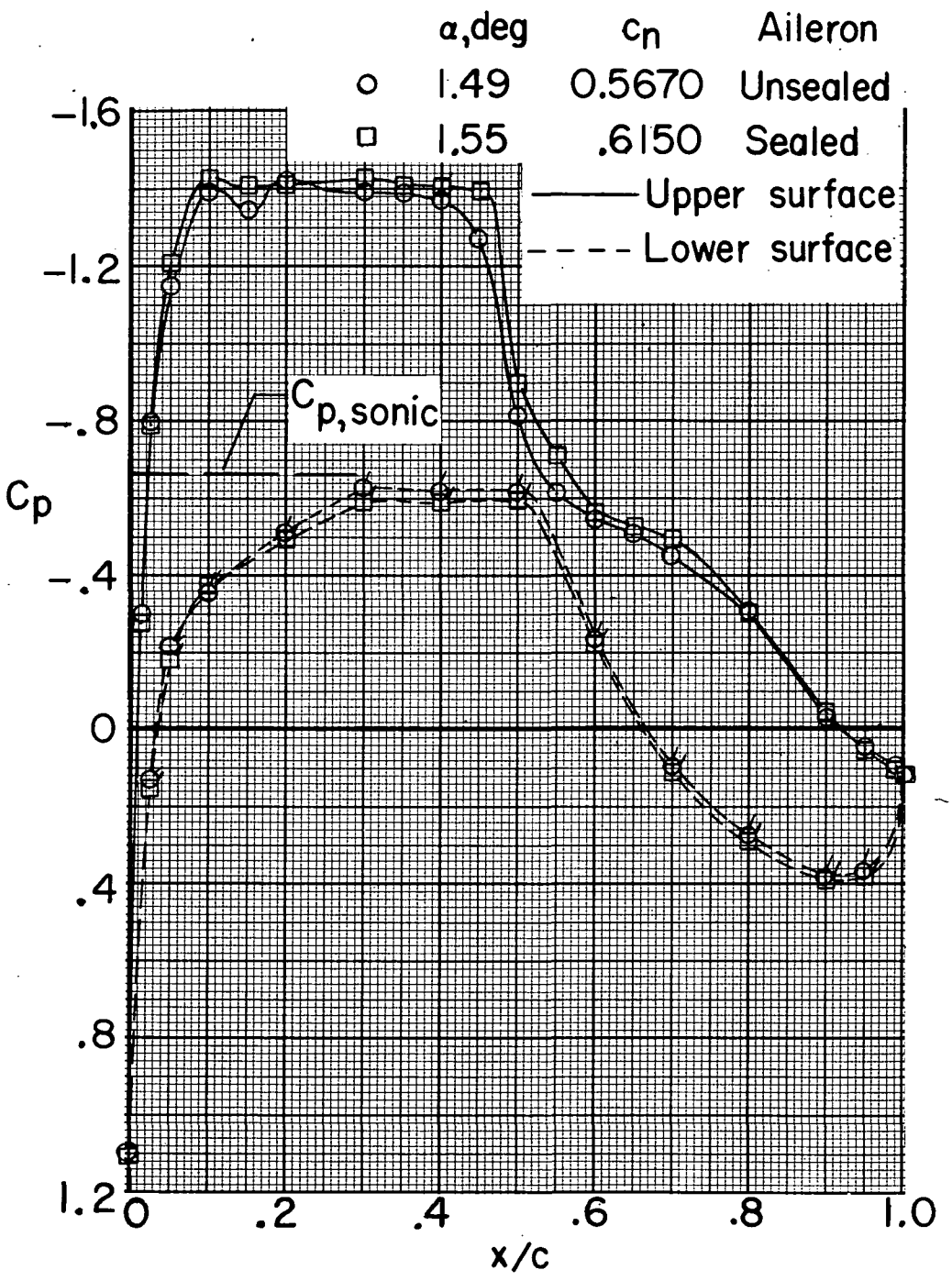
(b) M = 0.73. Concluded.

Figure 5.- Concluded.



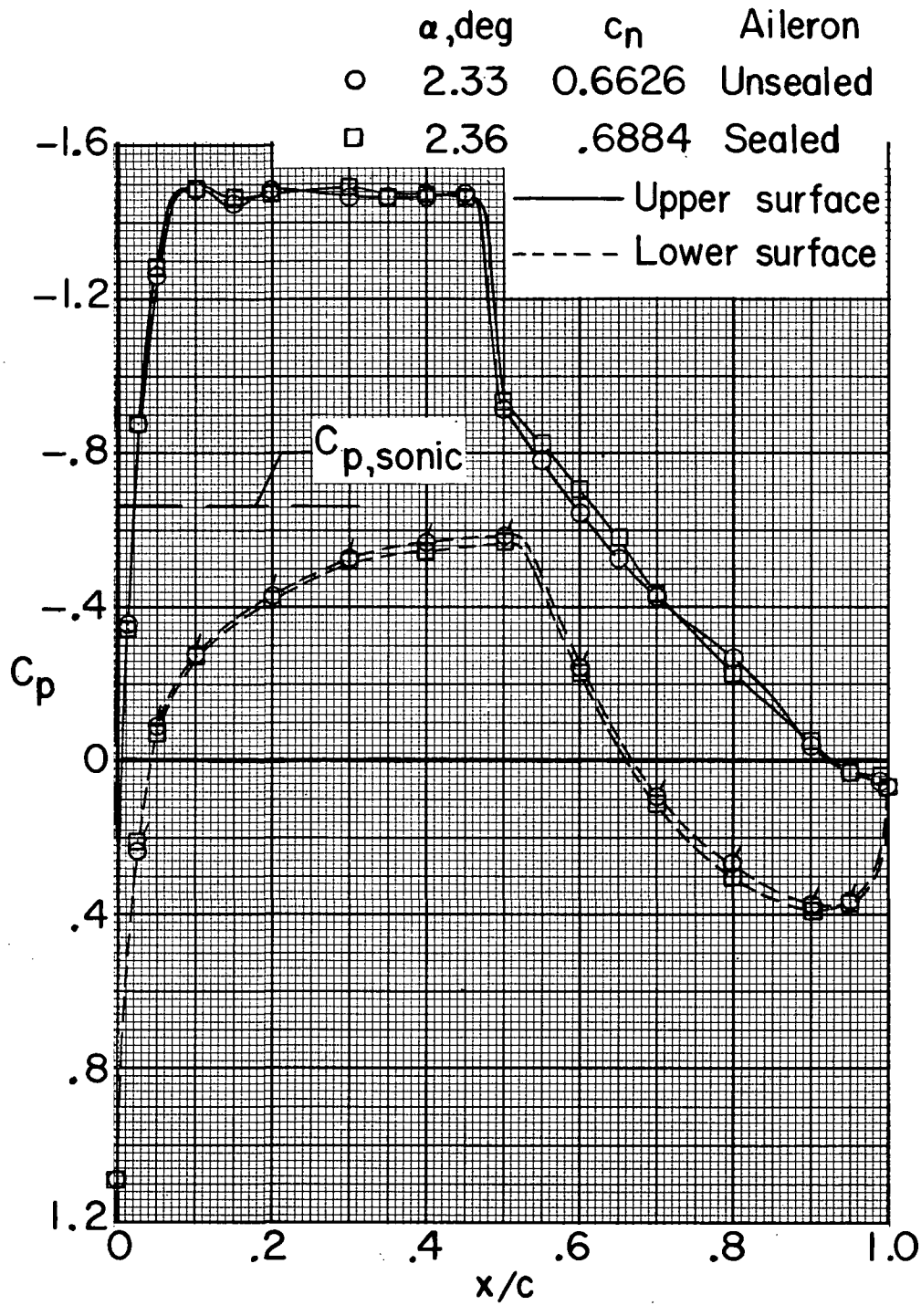
(a) $\eta = 0.4245$.

Figure 6.- Effect of sealed aileron on the chordwise pressure distribution. M = 0.73. Symbols without flags correspond to upper surface; symbols with flags correspond to lower surface.



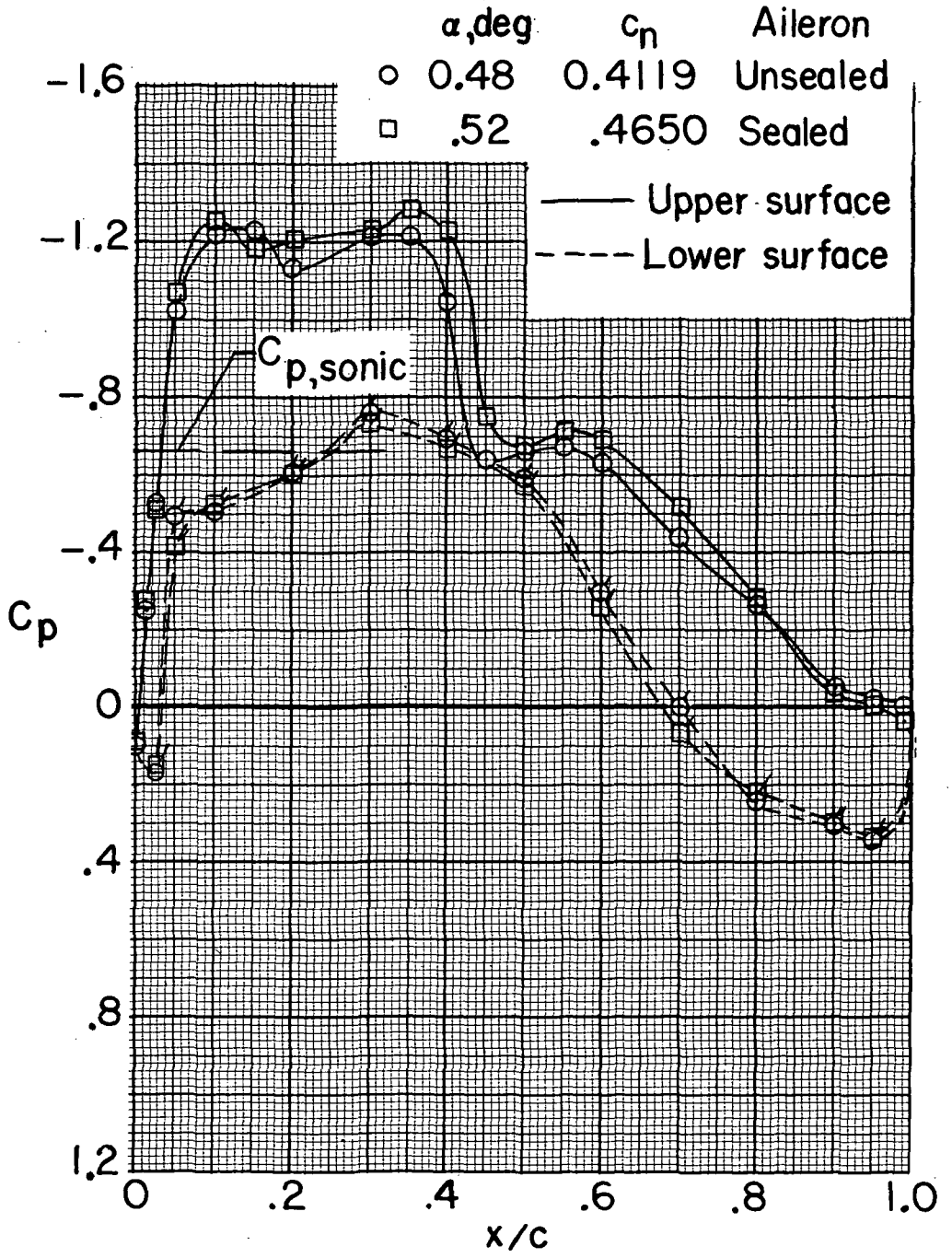
(a) η = 0.4245. Continued.

Figure 6.- Continued.



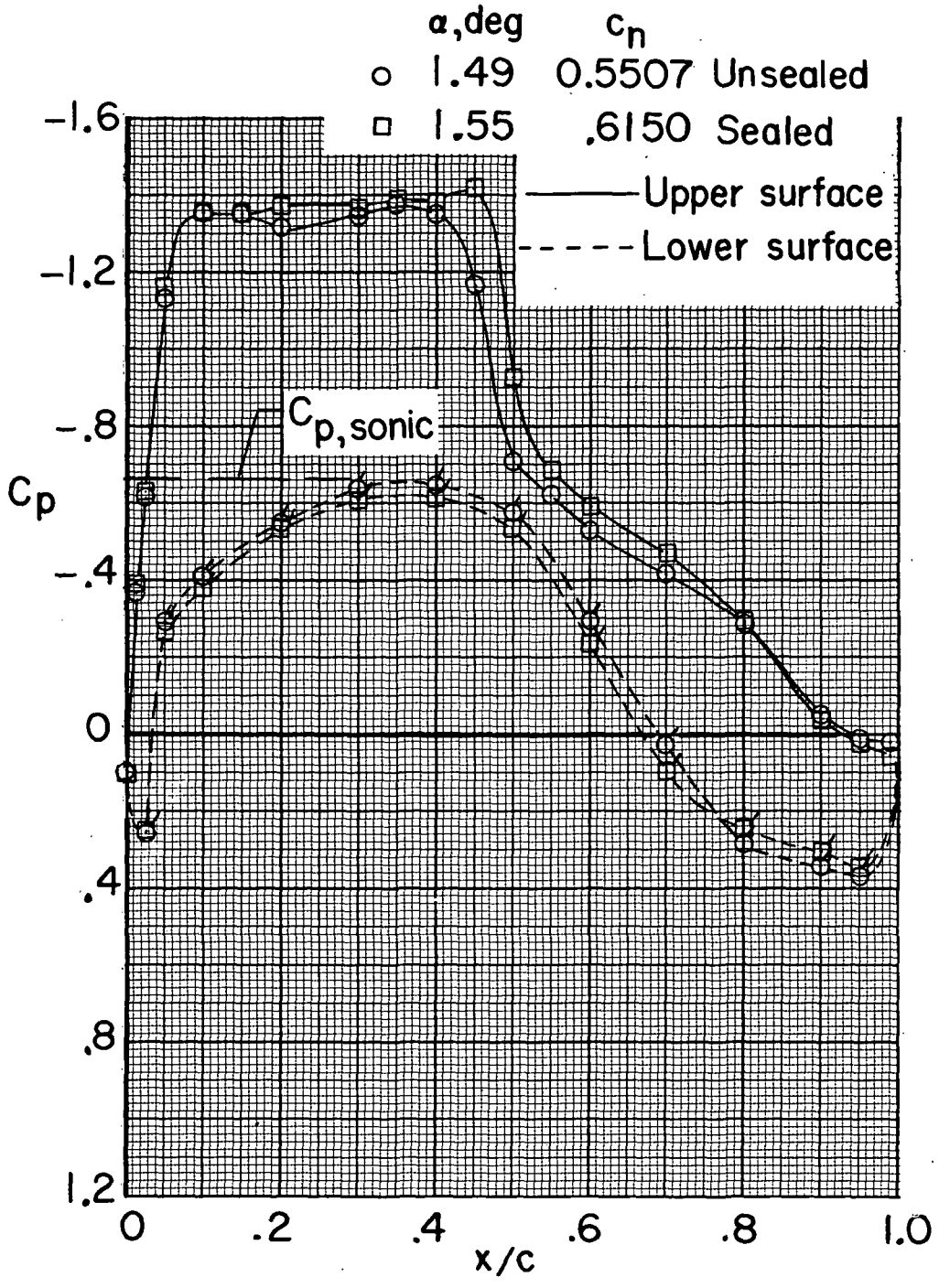
(a) η = 0.4245. Concluded.

Figure 6.- Continued.



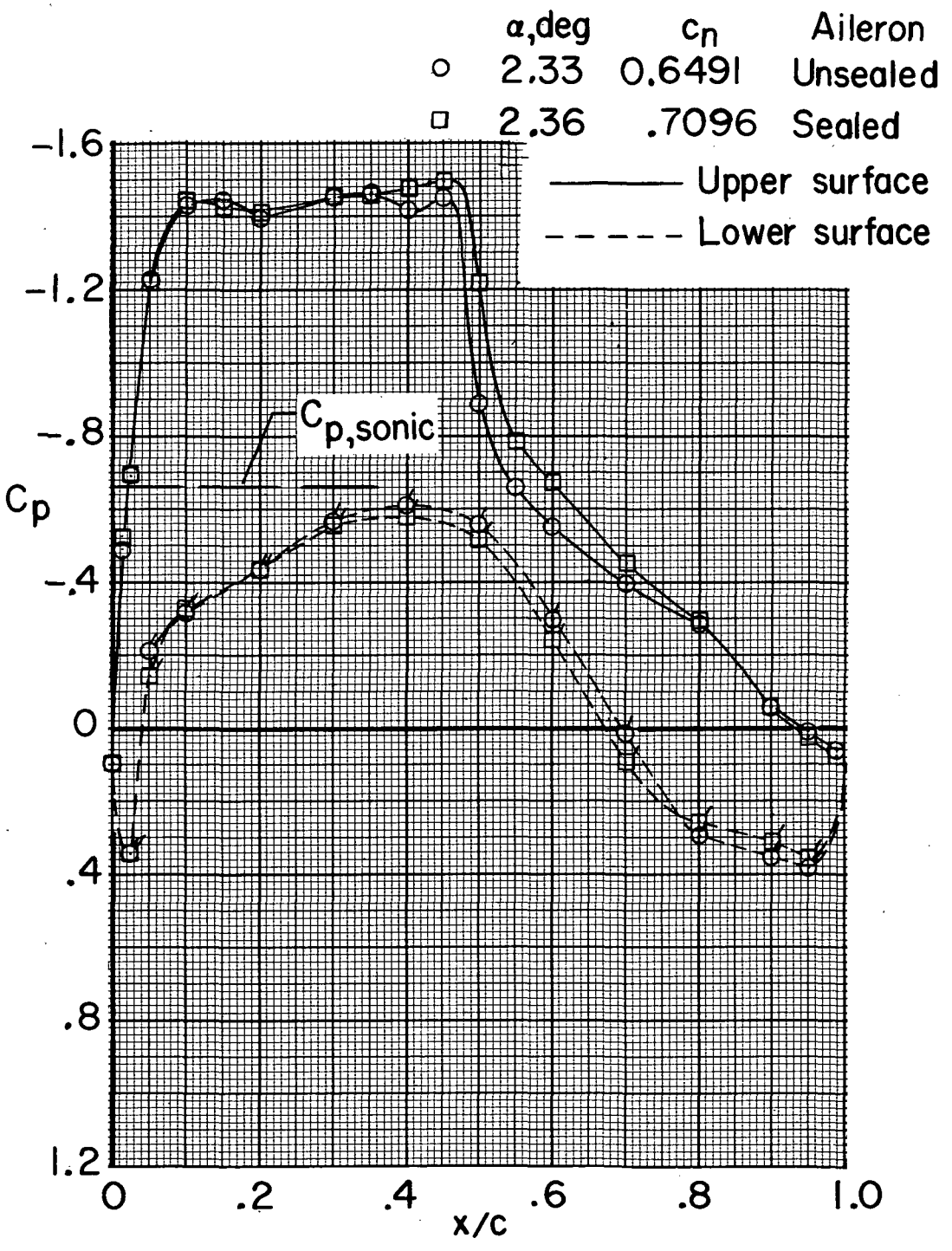
(b) $\eta = 0.7325$.

Figure 6.- Continued.



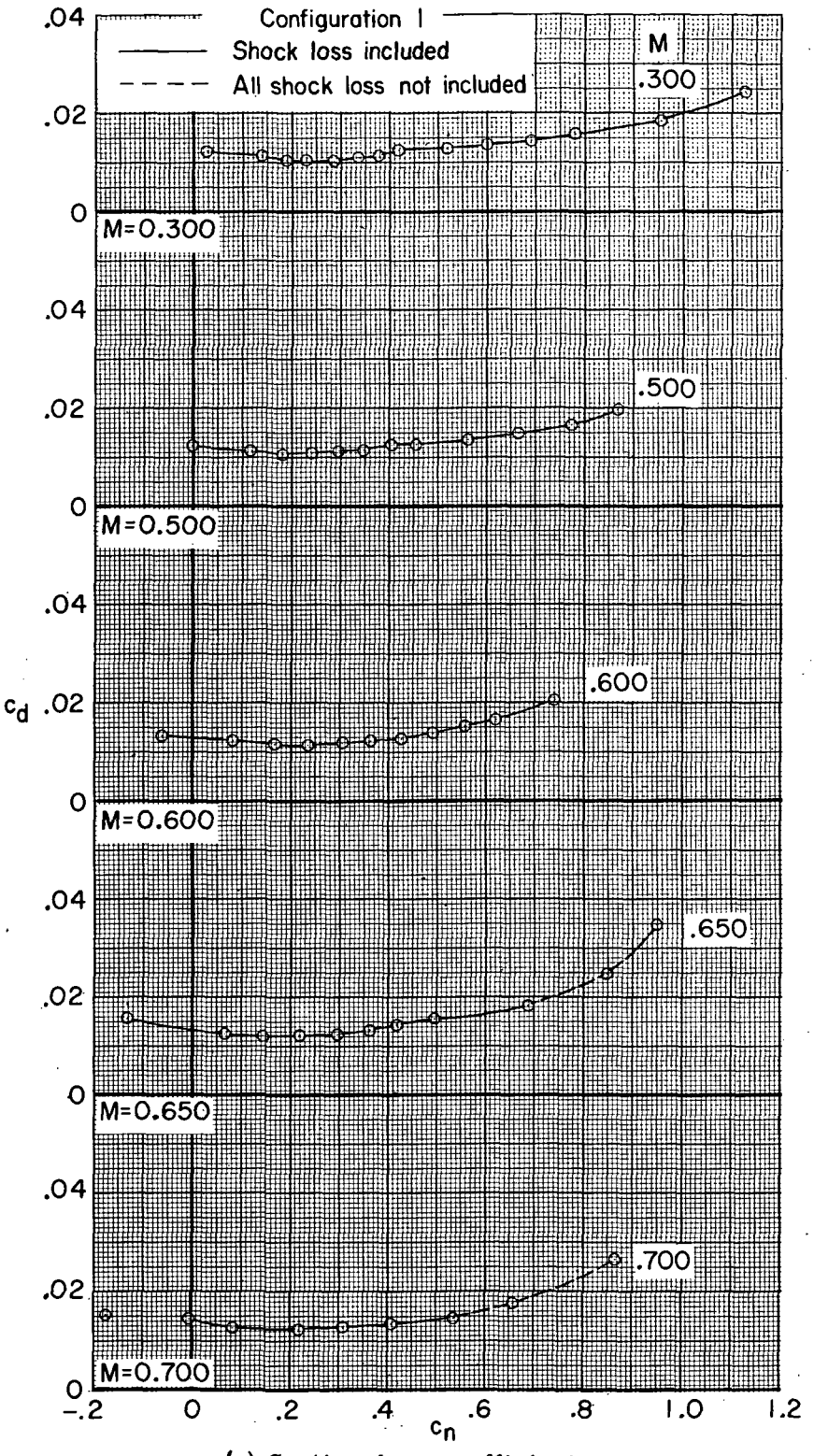
(b) η = 0.7325. Continued.

Figure 6.- Continued.



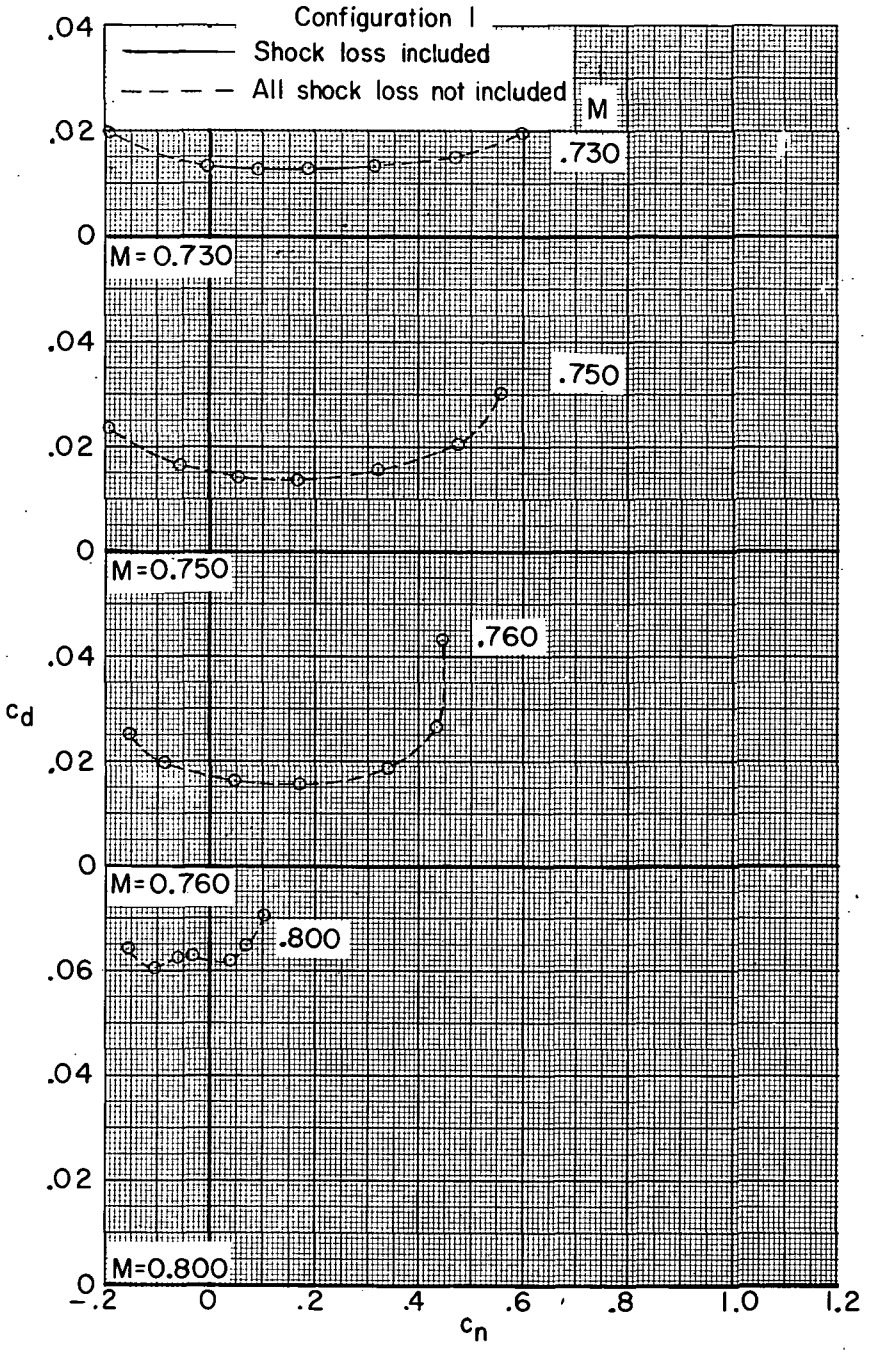
(b) $\eta = 0.7325$. Concluded.

Figure 6.- Concluded.



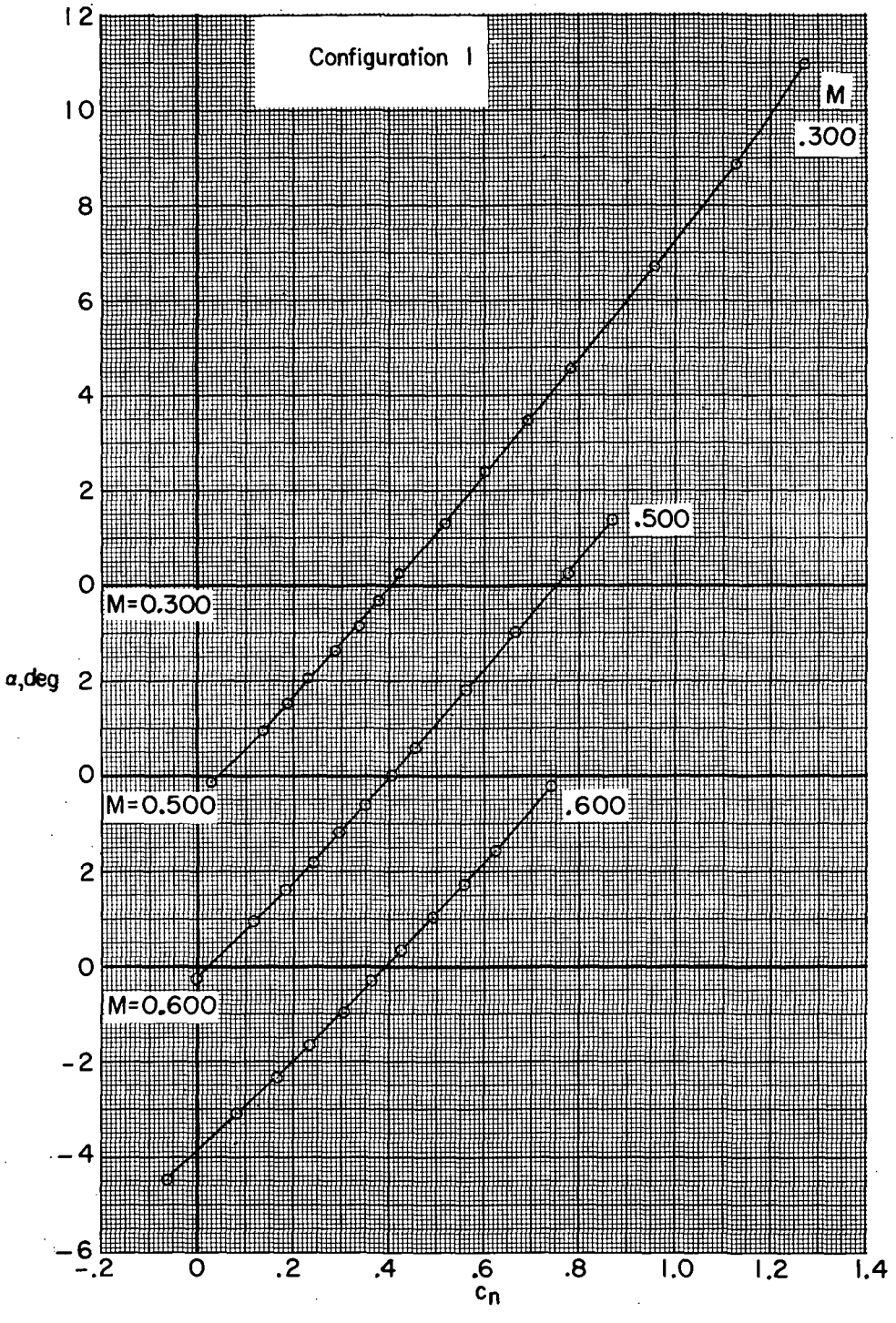
(a) Section drag coefficient.

Figure 7.- Variation of section drag coefficient, angle of attack, and section pitching-moment coefficient with section normal-force coefficient at various Mach numbers for the $\eta = 0.4245$ wing semispan station.



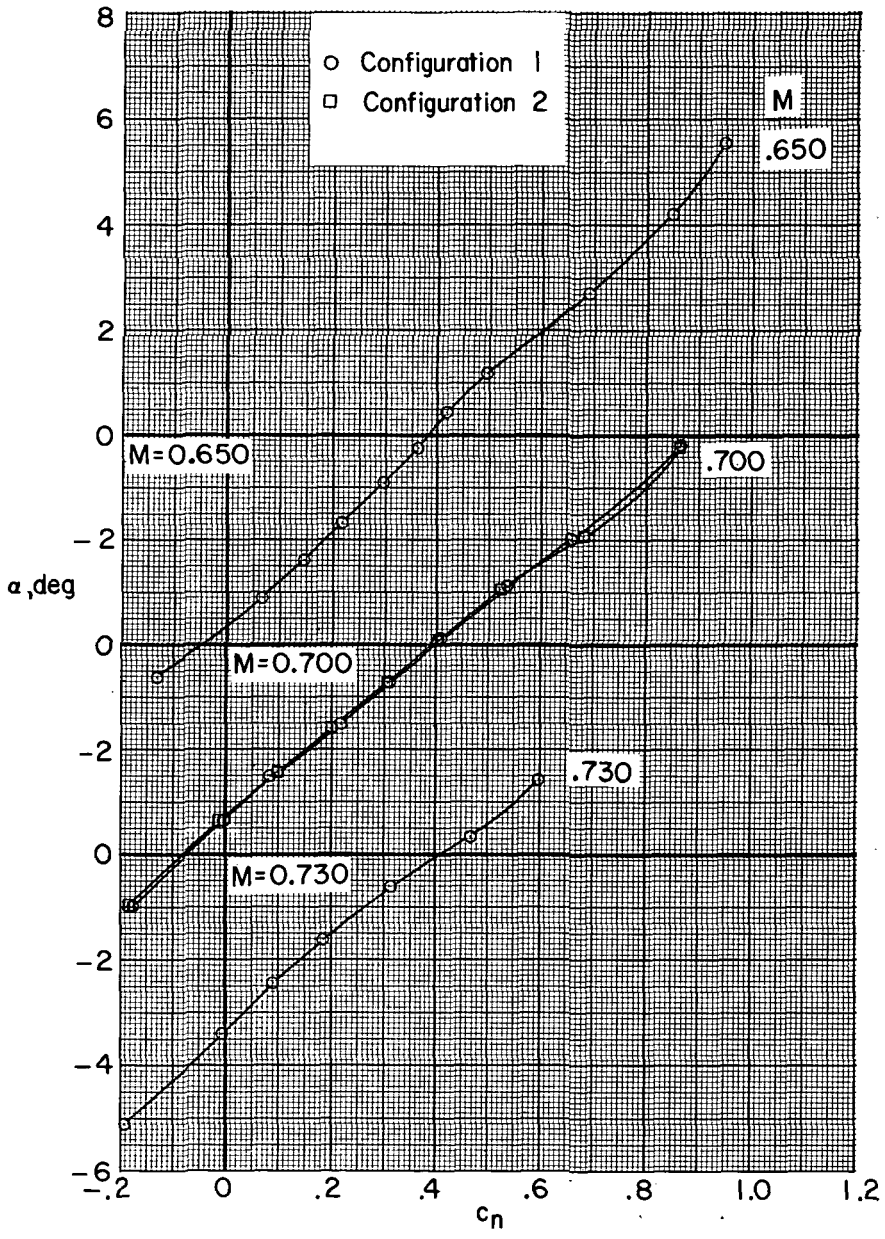
(a) Section drag coefficient. Concluded.

Figure 7.- Continued.



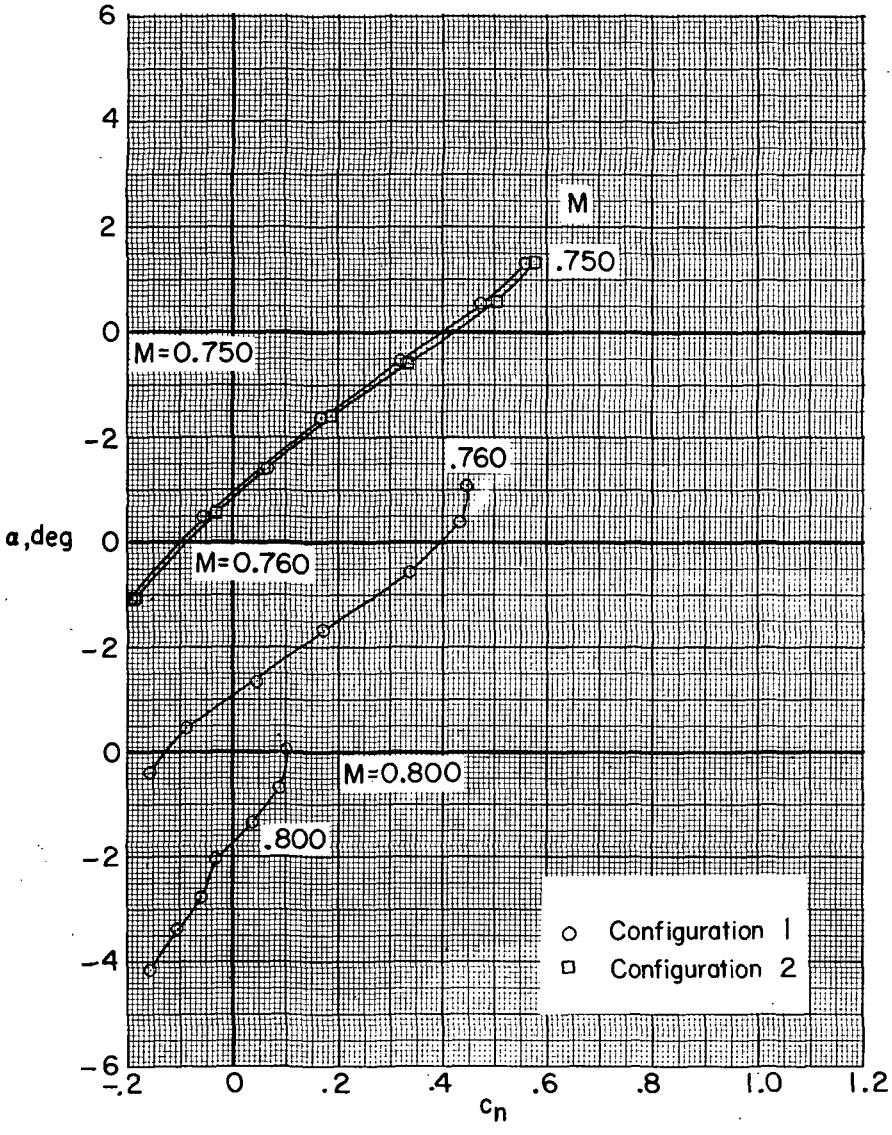
(b) Angle of attack.

Figure 7.- Continued.



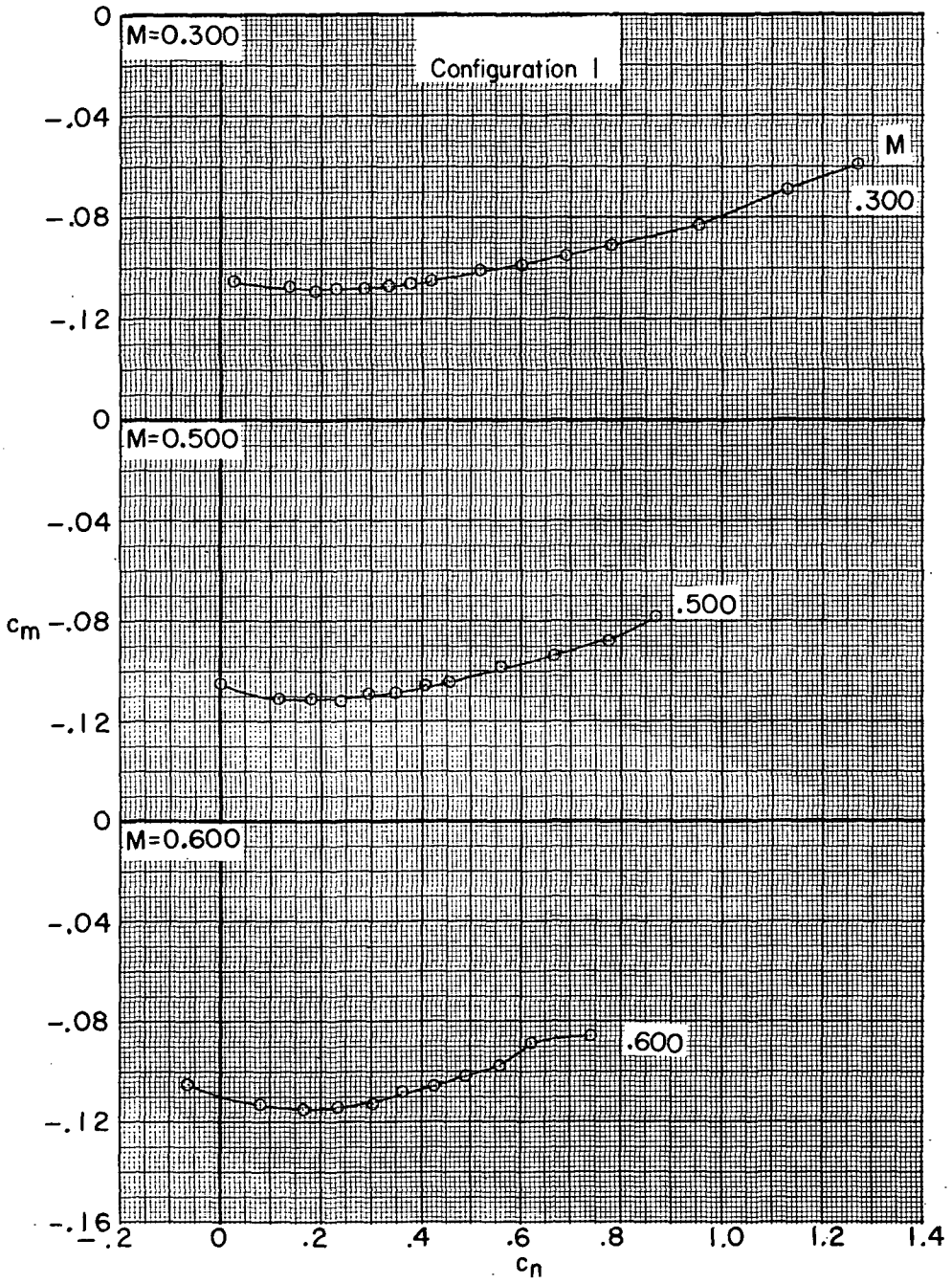
(b) Angle of attack. Continued.

Figure 7.- Continued.



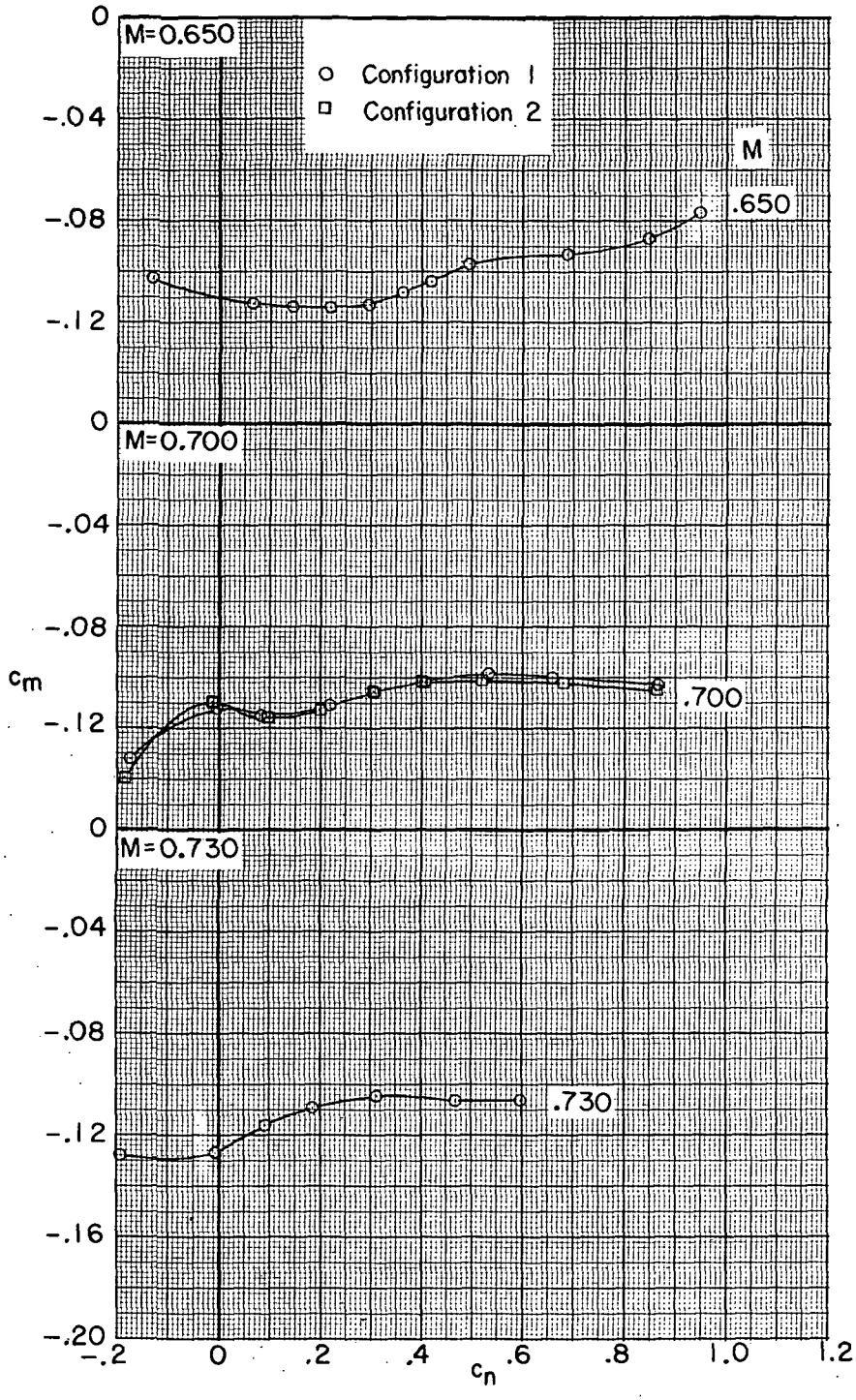
(b) Angle of attack. Concluded.

Figure 7.- Continued.



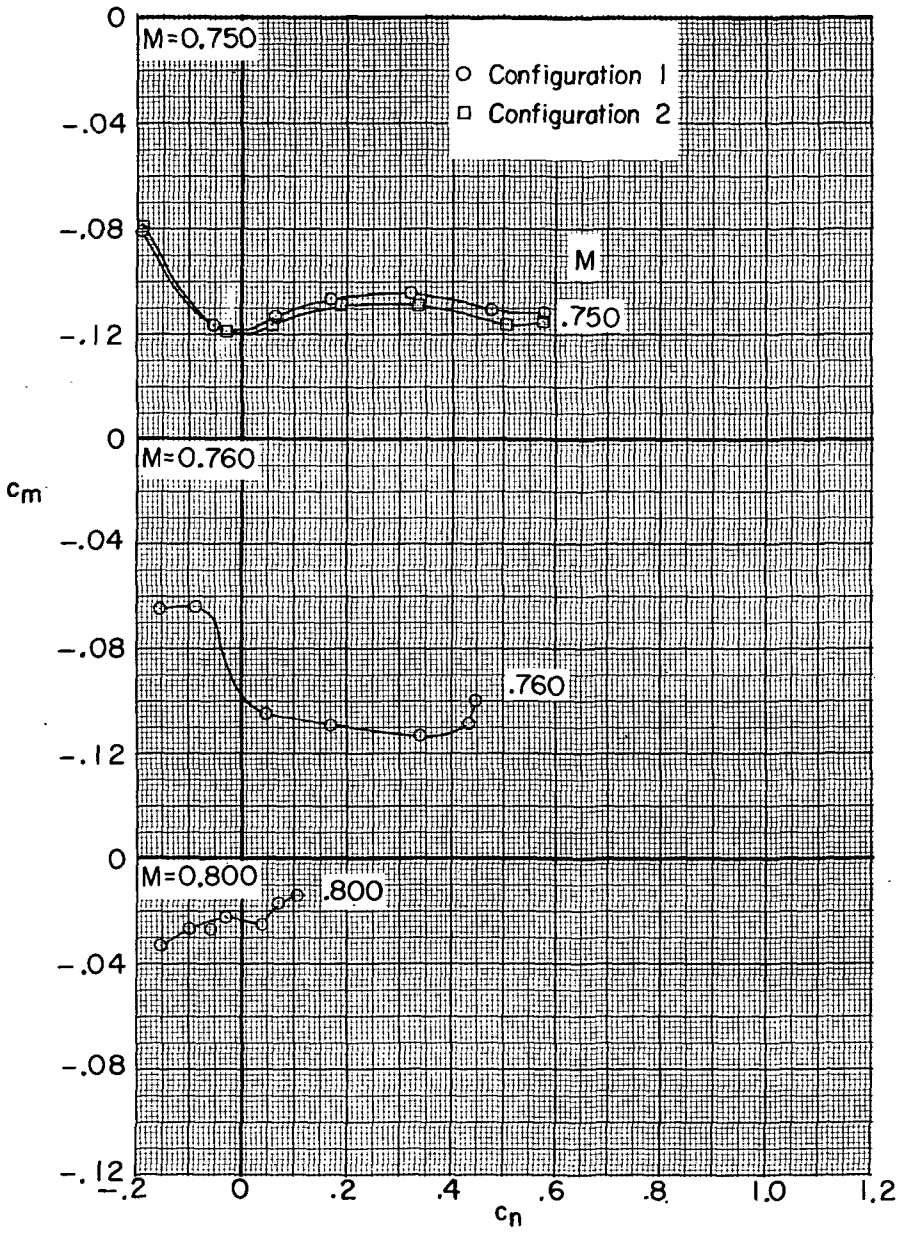
(c) Section pitching-moment coefficient.

Figure 7.- Continued.



(c) Section pitching-moment coefficient. Continued.

Figure 7.- Continued.



(c) Section pitching-moment coefficient. Concluded.

Figure 7.- Concluded.

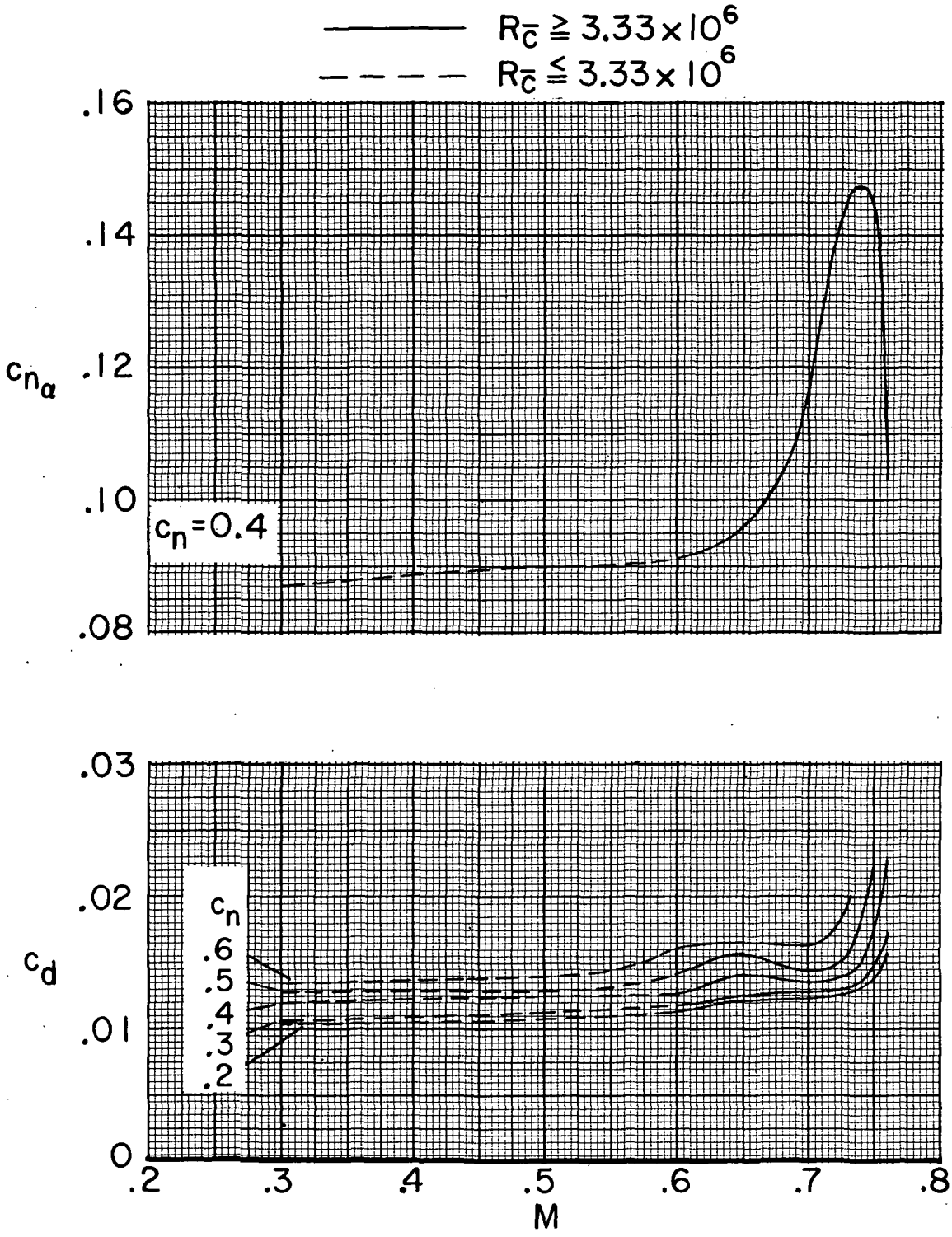


Figure 8.- Variation of c_{n_α}, c_d, $c_{m_{c_n}}$, and $c_{m,o}$ with Mach number for $\eta = 0.4245$ wing semispan station.

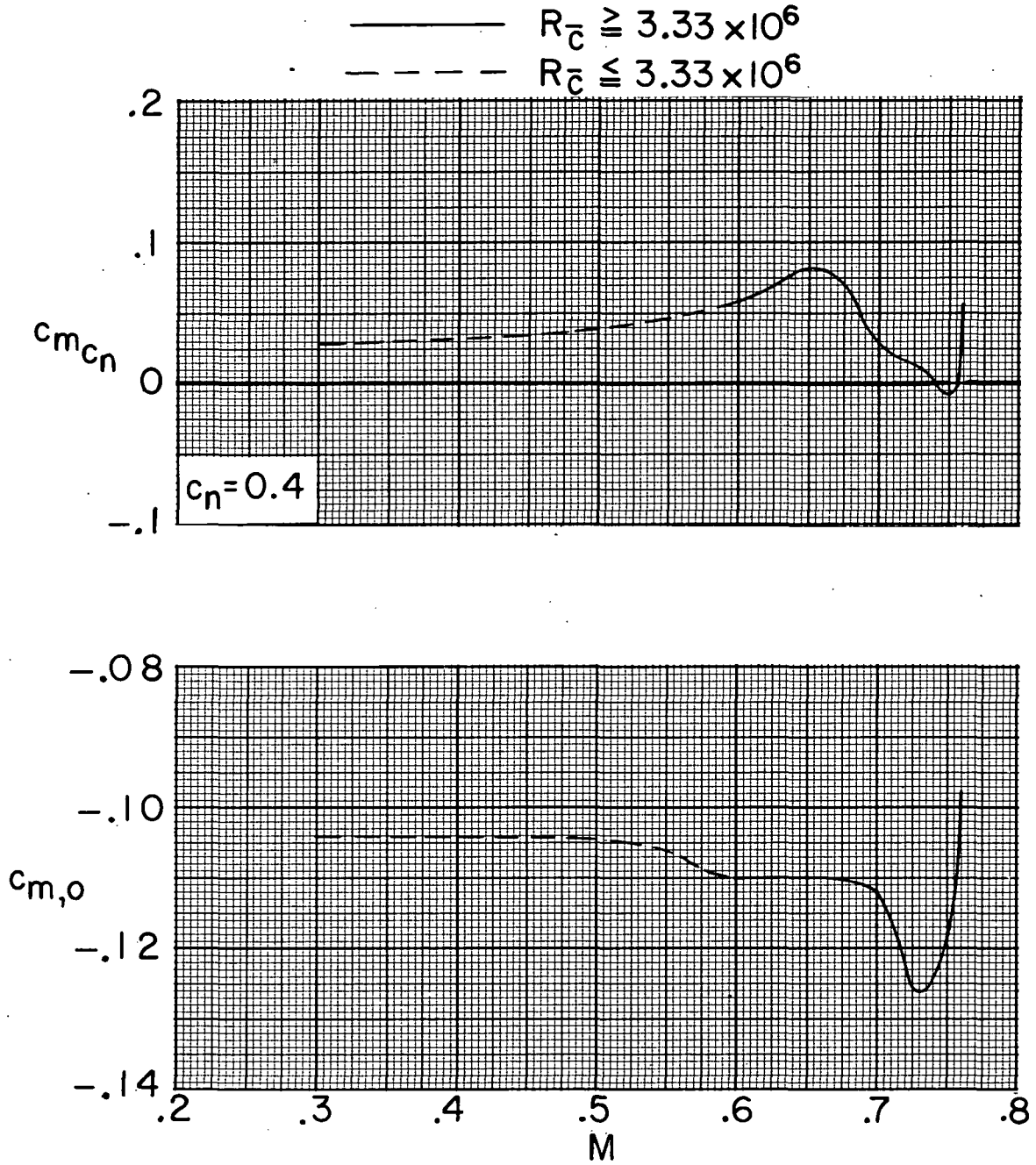


Figure 8.- Concluded.

"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

—NATIONAL AERONAUTICS AND SPACE ACT OF 1958

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